

## C) TEKSTUALNA DOKUMENTACIJA

# 1.TEHNIČKI OPIS

Glavni projekat termotehničkih instalacija za rekonstrukciju i dogradnju objekta ARHITEKTONSKOG FAKULTETA u Podgorici na lokaciji: UP14 DUP „Univerzitetski centar“ u Podgorici urađen je u skladu sa Projektnim zadatkom i Glavnim arhitektonsko građevinskim projektom. Za objekat su predviđene sledeće instalacije:

## **1.Instalacija za grijanje i hlađenje u objektu**

## **2. Instalacija za grijanje i hlađenja amfiteatra i kluba/kafe-a**

## **3. Instalacija ventilacije prostorija**

## **4. Instalacija ventilacije toaleta**

### **1. Instalacija za grijanje i hlađenje u objektu**

Za grijanje/hlađenje objekta predviđeno je sedam nezavisnih VRV sistema, i tri spoljasnje VRV jedinice koje su priključene na dvije klima komore. Za sve sisteme zbog orijentacije objekta predviđen je 3-cijevni VRV sistem. Za suteran je predviđen SISTEM 1, za prizemlje SISTEM 3 i SISTEM 4, za prvi sprat SISTEM 5 i SISTEM 6 i za drugi sprat SISTEM 7 i SISTEM 8. SISTEM 2 je spoljašnja VRV jedinica priključena na klima komoru (KLIMA KOMORA KLUB) koja služi za grijanje/hlađenje kafe kluba u suteranu objekta. SISTEM 9-1 i SISTEM 9-2 su spoljašnje VRV jedinice priključene na klima komoru (K.K. AMFITEATAR) koja služi za grijanje/hlađenje amfiteatra koji se nalazi na drugom spratu. Ovi sistemi rade sa promjenljivom količinom rashladnog fluida. Kao rashladni fluid predviđen je R 410-A, koji nije štetan po ozonski omotač. Kompresorom upravlja inverter koji zavisno od toplotnog opterećenja objekta odabira najpovoljniju brzinu obrtanja kompresora. Rashladni fluid se dovodi do unutrašnjih jedinica sa promjenljivim zapreminskim protokom, dok unutrašnje jedinice imaju elektronski ekspanzioni ventil sa opsegom otvaranja 0-100%.

Ovakvim sistemima se obezbjeđuje istovremeno grijanje i hlađenje pojedinih prostorija – jedna jedinica radi u režimu grijanja dok druga jedinica radi u režimu hlađenja. Ovaj sistem je povoljan u prelaznim periodima (proljeće, jesen) kada jedna grupa prostorija zahtijeva hlađenje a druga istovremeno grijanje.

U narednoj tabeli je prikazan zbirni Izvještaj iz proračuna potrebne količine toplote za grijanje i hlađenje po pojedinim sistemima i navedeno na koji dio objekta se koji sistem odnosi.

SISTEM	$Q_{HL}(W)$	$Q_{GR}(W)$	LOKACIJA
SISTEM 1	35820	30471	SUTERAN
SISTEM 3	24132	17218	PRIZEMLJE
SISTEM 4	47403	45057	PRIZEMLJE
SISTEM 5	33940	22799	PRVI SPRAT
SISTEM 6	41816	36988	PRVI SPRAT
SISTEM 7	40587	31612	DRUGI SPRAT
SISTEM 8	33814	27805	DRUGI SPRAT

Spoljašnje jedinice VRV sistema se smještaju na krovu objekta. Od spoljašnjih do unutrašnjih jedinica vodi se izolovani bakarni cjevovod.



Cjevovod ulazi u objekat sa krova i se spušta vertikalno niz zid koji se oblaže gipsom, i zatim se vodi po plafonu određenih etaža do unutrašnjih jedinica.

Kao unutrašnje jedinice u kancelarijama i kabinetima predviđene su kasetne jedinice sa četvorosmjernim izduvavanjem dimenzija 700x700mm, dok su u holovima, salama, kopirnici, modelarnici i vježbaonicama predviđene kanalske jedinice različitih dimenzija.

Spoljašnje jedinice se sa unutrašnjim jedinicama povezuju bakarnim mekim i polutvrdim cijevima koje se međusobno povezuju tvrdim lemljenjem. Sva odvajanja rashladnog fluida se izvode prefabrikovanim izolovanim račvama. Bakarne cijevi se izoluju samogasivom izolacijom od sintetičke gume, debljine 9-13 mm. Za izolaciju koja se vodi izvan objekta (po krovu) potrebno je izvršiti njenu zaštitu samoljepljivom aluminijskom trakom, izolacijom otpornom na UV zračenje ili aluminijskim limom.

Kondenzat od unutrašnjih jedinica se spaja u zajedničke odvodne cijevi i odvodi izvan objekta u oluke. Horizontalna cijevna mreža za odvod kondenzata se vodi po plafonu. Cijevi za odvod kondenzata su PVC cijevi prečnika Ø32 mm. Priključci unutrašnjih jedinica na kondenz mrežu se izrađuju od PP-R cijevi Ø25mm. Visinu priključka odrediti vodeći računa o visini dizanja pumpi za kondenzat ugrađenih u unutrašnjim jedinicama.

Unutrašnje jedinice imaju sopstvene žičane kontrolere koji se postavljaju na zidu prostorija, sa višejezičkim displejom. Unutrašnje jedinice se sa kontrolerima povezuje dvožilnim LiYCY kablovima 2x0,75 mm<sup>2</sup>. Kontroleri su u izvedbi sa mogućnošću povezivanja na centralni sistem nadzora upravljanja.

Unutrašnje jedinice se povezuju sa spoljašnjim jedinicama dvožilnim kontrolnim LiYCY kablovima 2x0,75 mm<sup>2</sup>, pa svaka od unutrašnjih jedinica ima svoju adresu i zajedno sa spoljašnjim jedinicama čini jedinstveni kontrolni sistem.

Za sistem grijanja i hlađenja predviđena je ugradnja centralnog kontrolera kojim je omogućena centralna kontrola i nadzor nad sistemima koji su predviđeni za objekat.

Centralni kontroler omogućava sledeće kontrolne funkcije: uključivanje/isključivanje, režim rada, podešavanje temperature, brzina ventilatora i pozicija istrujnih lamela, grupno ili individualno upravljanje (uključivanje/isključivanje, režim i podešavanje temperature), regulacija temperature, kalendar, nedjeljni i dnevni programi ograničavanje pristupa individualnim žičanim upravljačima u prostorijama.

Centralni kontroler omogućava sledeće nadzorne funkcije: grafički prikaz na ekranu kontrolera, rad unutrašnjih i spoljašnjih jedinica, signalizacija greške, signalizacija zaprljanosti filztera na unutrašnjim jedinicama, različite nivoe pristupa (korisnički, servisni).

## 2. Instalacija za grijanje i hlađenje amfiteatra i kluba/kafe-a

Za ubacivanje vazduha u prostore, kao i za izvlačenje vazduha, predviđene su dvoetažne klima-komore proizvođača "DIKIN" ili sl, za spoljašnju ugradnju, smještene na ploči - dio krova objekta predviđen za tu namjenu. U sistemima se održava natpritisak. Komore rade sa 100% svježim vazduhom.

Sastav potisnog dijela komora je: priključak za svježi vazduh sa zaštitnom mrežicom i žaluzinama, filter, rekuperator, potisni ventilator, freonski izmjenjivač, izlazni priključak sa fleksi vezom (potis sa čela); a odsisnog dijela: ulazni priključak sa fleksi vezom, filter, rekuperator, odsisni ventilator, žaluzina za otpadni vazduh.

Za grijanje i hlađenje amfiteatra na drugom spratu i kluba/kafe-a u suterenu koriste se klima komore sa rekuperatorima, što povećava efikasnost sistema, jer se vazduh zagrijava/hladi, otpadnim vazduhom iz prostorije, bez miješanja svježeg i otpadnog vazduha. . Grijач i hladnjak su predviđeni kao jedan izmjenjivač.

Klima komora za amfiteatar koristi dva freonska izmjenjivača. Na svaki od izmjenjivača povezana je po jedna spoljašnja VRV jedinica.

Ova klima komora obezbeđuje protok od 6310 m<sup>3</sup>/h pripremljenog svježeg vazduha, i isto toliko otpadnog vazduha izbacuje van objekta. Na izlaznom dijelu kanala za otpadni vazduh, kao i na ulazu u kanal svježeg vazduha, predviđena je ugradnja protivkišnih žaluzina sa zaštitnom mrežom.

Klima komora za klub/kafe koristi jedan freonski izmjenjivač, i obezbeđuje protok od 4400 m<sup>3</sup>/h pripremljenog vazduha. 4400 m<sup>3</sup>/h otpadnog vazduha se odvodi iz prostorije i prolazi kroz rekuperator toplote gdje se energija preko razmjenjivača prenosi na svježi vazduh.

Svježi i otpadni vazduh se do i od klima komore vode kanalima od pocinčanog lima pravougaonog poprečnog presjeka. Kanali se spuštaju kroz vertikalni šaht u objektu, do odredjenih etaža a zatim se vode po plafonu. Od kanala pravougaonog poprečnog presjeka do varijabilnih vrtložnih difuzora vazduh se vodi sporo kanalima. Oblaganje kanala obrađenog vazduha se vrši termičkom izolacijom od mineralne staklene vune, keširane sa Al folijom bez natron papira, tip URSA TF R2/Ah ili sl. debljine 50 mm. Odsisni kanali i kanali otpadnog vazduha su od pocinkovanog lima odgovarajuće debljine izoluju se, na isti način, kao i kanali potisnog vazduha.

### 3. Instalacija ventilacije prostorija

Za prostorije: sala za nastavno osoblje(306), čajna kuhinja i trpezarija(325), arhiv studentskih radova(326) i radna sala(327) koje se nalaze na drugom spratu predviđena je prinudna ventilacija koja se ostvaruje ventilacionim jedinicama sa iskorištenjem otpadne toplote vazduha. Ove jedinice koriste toplotu vazduha iz prostorije koji izbacuje izvan objekta, da bi zagrijale svježi vazduh koji se ubacuje u objekat što i ovaj sistem čini izuzetno energetski efikasnim, tj. ne koristi se toplota, odnosno energija za grijanje odnosno hlađenje spoljašnjeg vazduha za ventilaciju.

Količina vazduha je određena po vazdušnom obroku od  $28\text{m}^3/\text{h}$  po osobi tako da ukupna količina vazduha za salu za nastavno osoblje iznosi  $1000\text{ m}^3/\text{h}$  (36 osoba).

Za ventilaciju sale za nastavno osoblje predviđena je jedna ventilaciona jedinica kapaciteta od  $1000\text{ m}^3/\text{h}$ .

Količina vazduha je određena po vazdušnom obroku od  $37\text{m}^3/\text{h}$  po osobi tako da ukupna količina vazduha za radnu salu iznosi  $450\text{ m}^3/\text{h}$  (12 osoba).

Količina vazduha je određena po vazdušnom obroku od  $50\text{m}^3/\text{h}$  po osobi tako da ukupna količina vazduha za arhiv studentskih radova iznosi  $100\text{ m}^3/\text{h}$  (2 osoba).

Količina vazduha je određena po vazdušnom obroku od  $38\text{m}^3/\text{h}$  po osobi tako da ukupna količina vazduha za čajnu kuhinju I trpezariju  $450\text{ m}^3/\text{h}$  (12 osoba).

Za ventilaciju radne sale, arhiva studentskih radova I čajnu kuhinju I trpezariju predviđena je jedna ventilaciona jedinica kapaciteta od  $1000\text{ m}^3/\text{h}$ .

Ventilacione jedinice se postavljaju na plafonu objekta. Svježi vazduh za ubacivanje u prostore uzimaju se sa fasade preko fiksnih protivkišnih žaluzina. Otpadni vazduh koji se izvlači iz prostora izbacuje se izvan objekta takođe preko fiksnih protivkišnih žaluzina postavljenih na fasadi objekta.

Od ventilacionih jedinica vazduh se neizolovanim spiro kanalima dovodi do elemenata za njegovu distribuciju. Za ubacivanje vazduha u prostore predviđeni su vrtložni difuzori, opremljeni sa priključnom kutijom i regulatorom protoka. Za odsisavanje vazduha predviđeni su takođe vrtložni difuzori – izvedba za izvlačenje vazduha. Difuzori se sa kanalskom mrežom povezuju fleksibilnim crijevima od PVC-a. Kanali i kutije distributivnih elementa se postavljaju vidno na plafonu.

Ventilacionom jedinicom se komanduje kontrolerom koji se sa istom povezuje kablom LIY-CY  $2\times 0.75\text{mm}^2$ .

U svrhu uštede energije za pogon ventilacionih jedinica i kontrolu nivoa  $\text{CO}_2$  u prostoru predviđena je ugradnja  $\text{CO}_2$  senzora, koji usled promjene nivoa  $\text{CO}_2$  u prostoru povećavaju i smanjuju broj obrtaja ventilatora ventilacione jedinice.

#### **4. Instalacija ventilacije toaleta**

U toaletima u suterenu objekta je predviđena ventilacija (odsisavanje vazduha) preko kanalskog ventilatora koji odsisavanje vazduha vrši kroz spiro kanale i ventilacione ventile koji su predviđeni kao odsisni elementi.

Za toalete na prvom i drugom spratu koji nemaju mogućnost prirodnog provjetravanja predviđeni su individualni ventilatori sa nepovratnom klapnom, koji se ugrađuju na vertikalni šaht kroz koji se vrši odvodjenje vazduha.

Na odvodima otpadnog vazduha izvan objekta predviđena je ugradnja fiksnih protivkišnih žaluzina sa zaštitnom mrežom. Ventilatori se uključuju sa paljenjem rasvjete.

Količina vazduha koja se odsisava iz zasebnih sanitarnih prostorija iznosi  $54 \text{ m}^3/\text{h}$ .

ODGOVORNI PROJEKTANT,  
Vuk Janković, dipl.ing.maš.

## 2. OPŠTI POGODBENI I POSEBNI TEHNIČKI USLOVI

### 2.1. POGODBENI USLOVI

#### I OPŠTE ODREDBE

1. Odnosi između naručioca i izvođača radova u poslovima izvođenja na građevinskim objektima uređuju se posebnim uzansama o građenju (Zakon o izgradnji objekata, Službeni list RCG br. 51/08), ako su ugovarači pristali na njihovu primjenu.
2. Poštenje i savjesnost je osnovno načelo kojeg se ugovarači moraju pridržavati.
3. Ugovarači su dužni nastojati da ostvare ciljeve koje su ugovorom postavili.
4. Ugovarači su dužni da svoje obaveze ispunjavaju u predviđenim rokovima. Ako ugovarač ne ispunji svoju obavezu u predviđenom roku, drugi ugovarač mu može odrediti naknadni primjerni rok za ispunjenje odnosne obaveze.
5. Ugovarač je dužan da blagovremeno obavijesti drugog ugovarača o činjenicama čije je nastupanje od uticaja na ispunjenje ugovora, kao što su smetnje u ispunjenju ugovora, promjena okolnosti i sl. Obavješćavanje se vrši u pismenoj formi.
6. Ugovarač ne može tražiti od drugog ugovarača da ispunji obavezu, ako sam nije ispunio ili nije spreman da ispunji svoju obavezu, osim ako ugovorom nije drugačije određeno.

#### II DEFINICIJE SASTAVNIH DJELOVA UGOVORA

7. Sastavni dijelovi ugovora su tehnička dokumentacija sa svim grafičkim, računskim i opisnim prilogima potrebnim za izvođenje radova koji su predmet ugovora, kao i posebni i drugi uslovi naručioca koji su ugovorom određeni.

#### III PROUČAVANJE I IZMJENA TEHNIČKE DOKUMENTACIJE

8. Izvođač je dužan da blagovremeno i detaljno prouči tehničku dokumentaciju na osnovu koje se izvode ugovoreni radovi i da od naručioca blagovremeno zatraži objašnjenje o nedovoljno jasnim detaljima.
9. Izvođač nema pravo da mijenja tehničku dokumentaciju. Ako uoči nedostatke u tehničkoj dokumentaciji ili smatra da tu dokumentaciju treba mijenjati radi njenog poboljšanja ili iz drugih razloga Izvođač je dužan da blagovremeno obavijesti Naručioca.
10. Naručilac ima pravo da mijenja tehničku dokumentaciju na osnovu koje se izvode radovi. Ako se izmijeni tehnička dokumentacija mijenjaju se na odgovarajući način ugovorene cijene, rok za izvođenje radova i drugi dijelovi ugovora na koje utiče izmjena tehničke dokumentacije.
11. Projekat izvedenih radova su crteži i proračuni izvršenih izmjena i dopuna tehničke dokumentacije i stvarno izvedenih na osnovu tih izmjena i dopuna. Projekat izvedenih radova izvođač predaje naručiocu po završetku radova, odnosno po raskidanju ugovora.
12. Izvođač je dužan da izvede ugovorene radove na način i u rokovima koji su određeni ugovorom, propisima i pravilima struke. Ugovorenim radovima se smatraju i viškovi radova.
13. Izvođač je dužan da po pismenom nalogu naručioca izvede nepredviđene radove.
14. Naručilac je dužan da izvođenje nepredviđenih radova ustupi izvođaču, a trećem licu ih može ustupiti ako izvođač odbije da ih izvede ili nije u mogućnosti da ih izvede uopšte ili blagovremeno.
15. Naručilac je dužan da izvođenje naknadnih radova prije ustupanja trećem licu ponudi izvođaču.

#### IV CIJENA

16. Cijena radova određuje se na način utvrđen uslovima naručioca za podnošenje ponuda i ugovaranje predmetnih radova.
17. Svaki ugovarač ima pravo da zahtijeva izmjenu ugovorene cijene u slučaju nastupanja

vanrednih događaja koji utiču na visinu cijene.

18. Ugovarač ne može zahtijevati izmjenu cijene zbog promijenjenih okolnosti koje su nastupile po isteku roka određenog na ispunjenju njegove obaveze, osim ako je za donju kriva druga ugovorna strana.
19. Ako izvođač bez prethodne saglasnosti naručioca upotrijebi materijal boljeg kvaliteta od ugovorenog, ocjena radova se po tom osnovu može izmijeniti uz pristanak naručioca.
20. Naručilac koji je primio izvedene radove ima pravo na srazmjerno smanjenje cijena ako kvalitet upotrijebljenog materijala ili izvedenih radova bude ispod ugovorenog. Iznos smanjenja cijene utvrdiće se sporazumno između naručioca i izvođača.

## V ROKOVI ZA IZVOĐENJE RADOVA

21. Pod rokom za izvođenje radova u smislu ovih uzansi podrazumijevaju se i rokovi za završavanje pojedinih faza radova koji su predviđeni dinamičkim planom radova, ako su ugovarači tako odredili.
22. Ako je naručilac ustupio izvođenje radova dvojici ili većem broju izvođača na istom objektu, dužan je da koordinira rad tih izvođača za izvršenje tih radova.
23. Izvođač ima pravo da zahtijeva produženje roka za izvođenje radova u slučaju u kome je zbog promijenjenih okolnosti ili neispunjavanja obaveza naručioca bio spriječen da izvodi radove.

## VI UVOĐENJE IZVOĐAČA U POSAO

24. Pod uvođenjem izvođača u posao podrazumijeva se ispunjenje ovih obaveza naručioca bez čijeg prethodnog ispunjenja započinjanja radova faktički nije moguće ili pravno nije dozvoljeno.

## VII USTUPANJE RADOVA TREĆEM LICU

25. Izvođač može izvođenje pojedinih radova ustupiti trećem licu.

## VIII UGOVORNA KAZNA

26. Ako je ugovorom predviđena ugovorna kazna, a nije određeno u kojim se slučajevima plaća, smatra se da je kazna ugovorena za slučaj neurednog izmirenja ugovorenih obaveza.
27. Dužnik se oslobađa od plaćanja ugovorne kazne ako je do neispunjenih ili neurednog ispunjenja ugovorenih obaveza došlo zbog uzroka za koji nije odgovoran.

## IX PLAĆANJE

28. Izvedeni radovi plaćaju se na osnovu privremenih situacija i okončane situacije.
29. Privremena situacija i okončana situacija ispostavljaju se na osnovu izvedenih količina ugovorenih radova i ugovorenih cijena. Situacijama se prikazuju radovi na način i po specifikaciji koja je data u tehničkoj dokumentaciji
30. Naručilac ima pravo da zadrži srazmjerni dio cijena za otklanjanje nedostataka utvrđenih prilikom primopredaje radova.

## X PRIVREMENO OBUSTAVLJANJE IZVOĐENJA RADOVA

31. Izvođač ima pravo da privremeno obustavi izvođenje radova, ako je postupcima naručioca spriječen da izvodi radove ili je zbog tih postupaka izvođenje radova znatno otežano.
32. U slučaju obustavljanja radova izvođač je dužan da već izvedene radove zaštititi od propadanja preduzimanjem mjera zaštite koje su nužne.

## XI KVALITET RADOVA I MATERIJALA

33. Izvođač je dužan da saglasno pravilima struke ispita pravilnost tehničkog rješenja u

tehničkoj dokumentaciji i da naručioca upozori na grešku koju primijeti.

34. Izvođač je dužan da pruži dokaze o kvalitetu upotrijebljenog materijala i opremi izvedenih radova i da naručiocu omogući kontrolu.
35. Svi nalazi kontrole izvođača i kontrole naručioca upisuju se u građevinski dnevnik.

## XII GARANCIJA ZA KVALITET IZVEDENIH RADOVA

36. Izvođač garantuje da su izvedeni radovi u vrijeme primopredaje u skladu sa ugovorom, propisima i pravilima struke.
37. Garatni rok na kvalitet izvedenih radova iznosi dvije godine, ako ugovorom ili propisima nije drugačije određeno.
38. Za opremu koju ugrađuje izvođač važi u pogledu sadržine i roka, garancija proizvođača opreme, s tim što je izvođač dužan da svu dokumentaciju o garancijama proizvođača opreme zajedno sa uputstvima za upotrebu, pribavi i preda naručiocu.
39. Izvođač je dužan da o svom trošku otkloni sve nedostatke koji se pokažu u toku garantnog roka, a koji su nastupili usled toga što se izvođač nije držao svojih obaveza u pogledu kvaliteta radova i materijala.

## XIII MATERIJAL I OPREMA KOJI NABAVLJA NARUČILAC

40. Ako je ugovorom između naručioca i izvođača predviđeno da izvođač ugrađuje određenu opremu i materijal koji nabavlja naručilac, izvođač je dužan da materijal i opremu koju primi od naručioca uskladišti, čuva i održava do ugrađivanja.

## XIV OSIGURANJE

41. Izvođač osigurava radove, materijal i opremu za ugrađivanje od uobičajenih rizika do njihove pune vrijednosti.

## XV SNOŠENJE RIZIKA

42. Do primopredaje izvedenih radova, rizik slučajne propasti i oštećenja radova, materijala i opreme snosi izvođač. Naručilac snosi rizik za materijal i opremu, koju je nabavio do njihove predaje izvođaču.

## XVI STRUČNI NADZOR NARUČIOCA

43. Naručilac ima pravo da vrši stručni nadzor nad radovima izvođača radi provjeravanja i obezbjeđenja njihovog kratkog izvođenja, naročito u pogledu vrsta, količina i kvaliteta radova, materijala i opreme i predviđenih rokova.

## XVII ODGOVORNOST IZVOĐAČA ZA STABILNOST I SIGURNOST OBJEKTA

44. Izvođač odgovara za nedostatke objekta u pogledu njegove stabilnosti i sigurnosti, koji bi se pokazali na vrijeme od 10 godina od dana primopredaje radova.

## XVIII MJERE SIGURNOSTI

45. Izvođač je dužan da na gradilištu preduzme mjere radi obezbjeđenja sigurnosti objekta i radova, opreme, uređaja i instalacija, radnika, prolaznika, saobraćaja, susjednih objekata i okoline.

## XIX OBEZBJEĐENJE I ČUVANJE GRADILIŠTA

46. Od početka izvođenja do predaje radova naručiocu, izvođač na pogodan način obezbjeđuje i čuva izvedene radove, opremu i materijal od oštećenja, propadanja, odnošenja ili korišćenja.

## XX PRIMOPREDAJA IZVRŠENIH RADOVA

47. Odmah po završetku radova izvođač obavještava naručioca da su radovi koji čine predmet ugovora završeni.
48. Naručilac i izvođač su dužni da bez odlaganja pristupe primopredaji i konačnom obračunu.
49. Ako je naručilac počeo da koristi objekat prije primopredaje, smatra se da je primopredaja izvršena danom početka korišćenja.

## XXI KONAČAN OBRAČUN

50. Konačnim obračunom se raspravlja o odnosi između ugovarača i utvrđuje izvršenje njihovih međusobnih prava i obaveza iz ugovora.
51. Konačan obračun vrši se po primopredaji izvedenih radova. Rad na konačnom obračunu započinje odmah po izvršenoj primopredaji a završava se u roku od 60 dana od dana primopredaje.
52. Konačnim obračunom obuhvataju se svi radovi, izvedeni na osnovu ugovora, uključujući i nepredviđene i naknadne radove koje je izvođač bio dužan ili ovlašćen da izvede, bez obzira da li su radovi obuhvaćeni privremenim situacijama.

## XXII POSLEDICE RASKIDA UGOVORA

53. Ako dođe do raskida ugovora naručilac je dužan da izvođaču plati izvedene radove i u slučaju u kome je izvođač odgovoran za raskidanje.

## XXIII UREĐENJE GRADILIŠTA

54. Po završenim radovima, odnosno po raskidanju ugovora, izvođač je dužan da sa gradilišta povuče svoje radnike, ukloni preostali materijal, opremu i sredstva za rad, kao i privremene objekte koje je sagradio i očisti objekat i gradilište.

## 2.2. POSEBNI TEHNIČKI USLOVI

### a) Opšti dio

1. Instalacija mora biti izvedena u svemu prema projektu i može se ustupiti samo nom izvođaču koji je u stanju da se obaveže i dokaže da je u mogućnosti da kompletnu instalaciju isporuči, montira, ispita i pusti u pogon.
2. Prije početka radova izvođač je dužan da pregleda projekat i uporedi ga sa objektom i da o eventualnim nedostacima projekta ili bitnim potrebnim promjenama obavijesti investitora i zatraži njegova dalja uputstva.
3. Investitor je dužan da izvođaču obezbijedi zatvoren prostor na gradilištu za uskladištenje i pripremu materijala.
4. Izvođač instalacije može biti samo ono preduzeće koje raspolaže znanjem i mogućnostima koji se zahtijevaju za izradu ove vste instalacije, tj:
  - da može nabaviti, isporučiti i montirati sve elemente instalacije predviđene projektom, i da ima načina da za ovu opremu pribavi kompletnu tehničku dokumentaciju;
  - da raspolaže znanjem i mogućnostima rješavanja svih detalja potrebnih za montažu instalacije centralnog grijanja, na odgovarajući tehnički i estetski način;
  - da respolaže potrebnom kontrolnom, mjernom i regulacionom opremom kako bi izvršio dobru regulaciju svih elemenata izrađene regulacije.
5. Svi elementi predviđeni projektom za ugradnju u jednocijevni sistem moraju imati odgovarajućI sertifikat.
6. Elementi instalacije koji nijesu serijski proizvod, već se izrađuju posebno moraju biti izrađeni



od materijala dobrog kvaliteta i na najbolji način koji se predviđa za tu vrstu radova. Površinska zaštita mora biti izvedena tačno kako je naznačeno u projektu, a na mjestima gdje to nije naznačeno, na način uobičajen za tu vrstu radova i u skladu sa propisima o kvalitetu.

7. Projektant objekta, kao i izvođač građevinskih radova, moraju u dogovoru sa projektantom i izvođačem instalacije predvidjeti u zidovima dovoljno velike otvore i prodore za ugradnju horizontalnih i vertikalnih razvoda.
8. Izvođač instalacije centralnog grijanja mora koordinirati izvođenje svojih instalacija sa izvođačima ostalih instalacija, da ne bi došlo do nesporazuma i do oštećenja instalacije.

## b) Cijevna mreža

1. Sve cijevi horizontalnog i vertikalnog cjevovoda moraju imati atest i odgovarati standardima JUS C.B5.221, DIN 2440, DIN2441, odnosno DIN 2448.
2. Trasa vođenja cijevnih vodova i raspored oslonaca ne smiju se mijenjati bez saglasnosti projektanta.
3. Horizontalnu cijevnu mrežu u objektima sa podrumom treba vješati o plafon podruma ilki oslanjati na zidne konzole. U objektima bez podruma dozvoljava se polaganje cijevne mreže u podne kanale, koji nojanju od 8 do 10m imaju lagane kontrolne poklopce. Prije zatvaranja kanala, treba ga očistiti i cijevnumrežu zaštititi od korozije i na odgovarajući način izolovati.
4. Na prolazu kroz građevinsku konstrukciju cijevi ne smiju biti čvrsto uzidane, već uvijek mora biti dovoljno mjesta za slobodnu dilataciju cijevi usled promjena temperature.
5. Vertikalne cijevne vodove i priključke na grejna tijela treba voditi slobodno uz zid. Na vertikalnim vodovima odmah iza priključaka na horizontalnu cijevnu mrežu, treba ugraditi zasune ili prolazne ventile, a iznad njih slavine za pražnjenje.
6. Na mjestu ukrštanja priključaka za grejno tijelo sa vertikalnim vodom priključak mora da ima odgovarajući zaobilazni luk koji se obavezno izvodi u horizontalnoj ravni.
7. Priključci za grejna tijela ne mogu biti kraći od 30cm.
8. Usponski napojni vod uvijek se postavlja sa lijeve strane i mora biti fiksiran odgovarajućim brojem obujmica.
9. Za izradu cijevne mreže koja se montira u betonski sloj poda upotrijebiće se plastificirana bakarna cijev JUS C.D5.502. Prilikom savijanja cijevi, svijetli otvor se ne smije smanjiti, a za sve spojeve i nastavke moraju se upotrijebiti fitinzi za bakarne cijevi.
10. Odzračivanje instalacije treba rješavati u principu centralno, sa odzračnom mrežom preko odzračnih ili ekspanzionih posuda.
11. Na mjestima prolaska usponskih vodova kroz međuspratnu konstrukciju, cijevi treba obaviti talasastom hartijom, izuzev u mokrim čvorovima gdje se na prolazima postavljaju metalne čaure većeg prečnika radi slobodnog kretanja cijevi. Prostor između cijevi i čaure popuniti zaptivnom masom postojanom na radnoj temperaturi. U podnim prolazima ove čaure treba da budu izdignute 5 cm iznad poda.
12. Za prave cijevne vodove dužine preko 30m, po pravilu moraju se predvidjeti kompenzacione lire.
13. Djelovi cijevi koji nijesu predviđeni za odavanje toplote, a prolaze kroz negrijane prostorije, moraju se izolovati dobrom termičkom izolacijom. Izolaciju postaviti tako da pri širenju cijevi uslijed zagrijavanja ne dođe do njenog oštećenja.
14. Horizontalna mreža u svim djelovima treba da se vodi nagibom od 0.5 do 1% u smjeru odzračnih posuda, odnosno ventila i slavina za pražnjenje.
15. Spajanje cijevi vrši se zavarivanjem ili, ukoliko je potrebno ostvariti razdvojuvu vezu, pomoću prirubnica. Zavarena mjesta moraju biti dobro obrađena, sa dovoljnom debljinom vara, ali tako izvedenim da se presjek cijevi ne smanji. Kvalitet vara mora biti prvoklasan.
16. Pri svakom spajanju zavarivanjem moraju se obaviti sledeći radovi:
  - turpijanje (zakošavanje) rubova na djelkovima cijevi koje se bspajaju. Cijevi sa zidovima debljine manje od 3mm zavaruju se bez zakošenja ivica. Za cijevi sa debljinom zida većom od 3mm, ugao zakošenja ivica mora iznositi 60-70°;
  - čišćenje šavova od rđe i nečistoće;
  - skidanje šljake sa izvedenih varova i njihova antikorozivna zaštita osnovnim

premazom.

17. Cijevi se učvršćuju pokretnim i nepokretnim osloncima, jednodjelnim i dvodjelnim cijevnim obujmicama i konzolama. Maksimalno dozvoljeni razmaci između oslonaca navedeni su u sledećoj tabeli:

Dimenzije cijevi (mm)	Maksimalno rastojanje (m)
Ø17.2x1.8	2.0
Ø21.3x2.0	2.0
Ø26.9x2.3	2.0
Ø33.7x2.6	2.0
Ø42.4x2.6	2.5
Ø48.3x2.6	2.5
Ø57x2.9	2.5
Ø60.3x2.9	2.5
Ø70.0x2.9	3.0
Ø76.1x2.9	3.0
Ø88.9x2.9	3.0
Ø108.0x3.6	3.5

18. Pri izradi prirubničkih spojeva koristiti standardne prirubnice propisanih dimenzija i za odgovarajući radni pritisak. Pri spajanju cjevovoda i armature prirubnicama obavezna je upotreba zaptivnih prstenova od klingerita, minimalne debljine 3mm, ili grafitno-azbestne pletenice četvrtastog presjeka. Pletenice se moraju sjeći pod uglom od 45°, a nikako vertikalno.
19. Konzole i vješaljke na koje se oslanja cjevovod moraju omogućiti njegovo slobodno kretanje usled toplotnih dilatacija, bez mogućnosti stvaranja ugiba. Oslonci i konzole moraju biti ugrađeni u zidove pomoću cementnog maltera, a nikako gipsom.
20. Izrada krivina i fazonskih djelova na cijevnim vodovima može biti izvedena savijanjem cijevi (za prečnike do 26.9mm), ili upotrebom odgovarajućih lukova načinjenih od istog materijala. Armatura i fazonski djelovi ne smiju se postavljati unutar građevinskih elemenata. Na mjestima prodora cijevnih vodova kroz zidove i međuspratnu konstrukciju, a u prostorijama za boravak ljudi, sa obje strane postaviti rozete.
21. Sve cijevi, armatura i ostali metalni djelovi moraju se nakon završene montaže i obavljenih propisanih ispitivanja temeljno očistiti od rđe i zaštititi odgovarajućim temeljnim premazima. Nakon toga cijevi se moraju u zidu omotati talasastim papirom, izolovati ili bojiti uljanim lak-bojamam otpornim na visoke temperature.
22. Ugradnju zasuna, slavina i ventila izvesti tako da se vreteno sa točkom postavi vertikalno na horizontalne vodove. Svoj armaturi mora biti obezbijeđen prilaz radi eventualnih intervencija. Svi radijatorski ventili moraju biti podešeni prema podacima iz projekta.
23. Na svoj ugrađenoj armaturi mora biti strelicama vidno označen smjer kretanja grejnog fluida.
24. Na odgovarajućim mjestima potrebno je obezbijediti prostor za ugradnju ormana za smještaj priključne armature i mjerača utroška toplotne energije za svaki stan ili jednu cjelinu poslovnog prostora.
25. Ormani za smještaj priključne armature moraju biti tipski, sa unificiranom bravom za cijelo naselje. Takođe moraju biti dovoljnih dimenzija da omogućavaju normalnu montažu i demontažu elemenata. Visina razdjelnika i sabirnika smještenih u orman mora iznositi  $h=1.5\text{m}$  od kote poda prostorija u kojima su smještena grejna tijela. Detalj ormana, mjesto i prostor za njegovu ugradnju moraju biti usaglašeni sa arhitektonsko-građevinskim projektom, a potvrda o ovoj usaglašenosti, ovjerena pečatom i potpisima projektanata, treba da bude priložena investiciono-tehničkoj dokumentaciji.

## c) Montaža instalacije

1. Izvođač je dužan da cjelokupnu opremu predviđenu ovim projektom montira na način utvrđen grafičkom dokumentacijom, tehničkim opisom i ovim tehničkim uslovima.
2. Montaža obuhvata cjelokupnu instalaciju za grijanje, povezivanje cijevima sa toplotnom podstanicom, povezivanje sa priključcima vodovoda i kanalizacije koji će biti dovedeni do podstanice od strane izvođača radova na vodovodu i kanalizacije.
3. Svi zidarski radovi potrebni za pričvršćivanje držača, nosača, obujmica za nošenje kanala i drugih elemenata instalacije, spadaju u obavezu izvođača instalacija.
4. Prije svakog štemovanja ili bušenja betona potrebno je tražiti saglasnost nadzornog organa građevinskih radova, odnosno zahtijevati da se građevinski posao izvede i dati uputstvo kako da se izvede. Izvođač je dužan da nakon ugrađivanja elemenata izvrši zatvaranje rupa na način koji odgovara vrsti ugrađenih elemenata.

## 2.3. Tehnički uslovi za instalacije provjetravanja

### 2.3.1. Opšti tehnički uslovi

1. Instalacija mora biti izvedena u svemu prema projektu i može se ustupiti samo onom izvođaču koji je u stanju da se obaveže i dokaže da je u mogućnosti da kompletnu instalaciju isporuči, montira, reguliše, ispita i pusti u pogon, uključujući i automatiku, tačno prema projektu.
2. Svi elementi instalacije moraju biti takvi da u svim detaljima odgovaraju specificiranim karakteristikama i moraju imati takve dimenzije da se mogu uklopiti u gabarite predviđene projektom.
3. Elementi instalacije koji nijesu serijski proizvod, već se izrađuju posebno, moraju biti izrađeni od materijala dobrog kvaliteta i na najbolji način koji se predviđa za tu vrstu radova. Površinska zaštita mora biti izvedena tačno kako je naznačeno u projektu, a na mjestima gdje to nije naznačeno, na način uobičajen za tu vrstu radova i u skladu sa propisima o kvalitetu.
4. Izvođač instalacije izjavljuje da raspolaže znanjem i mogućnostima koji se od izvođača instalacija ove vste zahtijevaju, tj.:
  - a) da može nabaviti, isporučiti, montirati, povezati sa ostalim elementima instalacije predviđene projektom bilo da se radi o domaćoj ili uveznoj opremi, i da ima načina da za ovu opremu dobavi odgovarajuće prospekte, uputstva i objašnjenja koja bi u tu svrhu bila potrebna;
  - b) da raspolaže znanjem i mogućnostima rješavanja svih detalja u okviru montaže instalacije, na odgovarajući tehnički i estetski način, za koje nisu dati detaljni crteži kao što su: vješanje cijevi i kanala za vazduh, izrada čvrstih i kliznih oslonaca, postavljanje sudova za odzračivanje, postavljanje grejnih tijela, postavljanje opreme na plivajuće, elastične ili čvrste fundamente, uklapanje opreme u arhitektonsko-građevnisku cjelinu itd.;
  - c) da raspolaže mogućnostima potrebnim za regulaciju radnih parametara instalacije: brzinom strujanja i protoka, temperaturom vode, i vazduha i vlažnošću vazduha koristeći sve projektom predviđene regulacione elemente.
5. Oprema, materijal i armatura koji budu upotrijebljeni za izradu instalacija moraju biti najnovije fabričke proizvodnje u svemu prema važećim propisima. Armature i mjerni instrumenti moraju biti solidne izrade i u potpunosti odgovarati svojoj namjeni.
6. Izvođač instalacija dužan je da cjelokupnu opremu predviđenu ovim projektom montira na način predviđen crtežima, tehničkim opisom i ovim tehničkim uslovima. Izvođač je dužan da obezbijedi svoju stručnu i pomoćnu radnu snagu, svoj alat, mašine, instrumente i sve ostalo što je potrebno za montažu.
7. Radovi na izradi temelja za opremu koja zahtijeva fundiranje spadaju u dio isporuke instalacije i izvođač instalacije je dužan da ih izvede. Isto tako, svi zidarski radovi potrebni za pričvršćenje držača, nosača, obujmica, zatega i dr. za nošenje elemenata instalacije,

- spadaju u obavezu izvođača ove instalacije.
8. Regulacione krugove, kao i sve ostale elemente koji čine automatsku regulaciju, montirati prema priloženoj dokumentaciji. Izvođač je dužan da se prilikom montaže u potpunosti pridržava uputstava proizvođača opreme za mjerenje i regulaciju i to: detaljnih šema povezivanja, uputstava za montažu i uputstava za regulisanje i rukovanje.
  9. Nakon potpuno završene montaže cjelokupne instalacije, izvođač je obavezan da izvrši kontrolu i fino regulisanje opreme za mjerenje i automatsku regulaciju prema projektovanim parametrima.
  10. Elektroinstalacija je predmet projekta električnih instalacija, međutim, povezivanje svih električnih uređaja u sastavu projektovane mašinske opreme, dužan je da izvrši izvođač mašinskih instalacija, sa svojom radnom snagom, materijalom i alatom.
  11. Sva električna oprema predviđena za ugradnju u projektovanu instalaciju mora biti prilagođena za priključenje na mrežu 3x380V, 50Hz, odnosno 220V i 50Hz za monofazne priključke.
  12. Elektromotori treba da budu isporučeni zajedno sa osiguračima i upuštačima.
  13. Elektro-komandne razvodne table treba da sadrže sve elemente potrebne za upravljanje, kontrolu i osiguranje uređaja (osigurači, upuštači, kontrolne lampe i sl.). Na električnoj komandnoj tabli treba da budu montirani i svi potrebni releji i ostali električni instrumenti koji spadaju u okvir automatike ili su dio opreme koja čini vezu između automatike i elektromotora.
  14. Izvođač instalacije dužan je da obezbijedi sav materijal potreban električno povezivanje svih elektromotora i ostalih električnih uređaja koji ulaze u sastav instalacija, međusobno, kao i sa elektro-komandnom razvodnom tablom.
  15. Izolaciji i bojenju pristupa se po završenoj montaži i nakon uspješnog ispitivanja hermetičnosti instalacije. Prije izolacije i bojenja sve sve metalne djelove instalacije bez fabričke površinske zaštite potrebno je temeljno očistiti čeličnom četkom i dva puta premazati temeljnom bojom. Izolaciju izvesti pravilno u svemu i na način definisan projektom. Bojenje instalacije izvesti bojom po izboru investitora. Boja treba da ima dobra pokrivajuća svojstva i otpornost na maksimalnu predviđenu temperaturu.
  16. Po kompletno završenoj montaži treba pristupiti probnom radu i regulisanju instalacije. Pri probnom radu izvršiti sve pripremne radnje, kao što je ispuštanje vazduha iz cjevovoda, prethodno regulisanje, postavljanje klapni u radni položaj i sl., a zatim instalaciju pustiti u pogon. Po otklanjanju eventualnih nedostataka koji se jave u pogonu instalacije, pristupiti njenom finom regulisanju, koristeći sveprojektom predviđene i ugrađene regulacione i mjerne uređaje i opremu. Regulaciju brzina, protoka i temperatura izvesti tačno i dobro, pridržavajući se u svemu projektom definisanih uslova.

Odgovorni projektant,  
Vuk Janković, dipl.ing.maš.

### **3. PRILOG ZAŠTITE NA RADU**

#### **SADRŽAJ:**

1. Opasnosti i štetnosti koje mogu nastati od termomašinskih instalacija
2. Predviđene mjere za otklanjanje opasnosti i štetnosti
3. Opšte napomene i obaveze
4. Zaključak

#### **1. OPASNOSTI I ŠTETNOSTI**

1. Nepravilno izvršenog dimenzionisanja opreme i cjevovoda kao i nepridržavanja važećih tehničkih propisa i standarda.
2. Nepravilnog izbora opreme, cjevovoda, mjerno regulisanje i sigurnost armature
3. Nepravilnog rasporeda opreme i armature, neispravnog postavljanja cjevovoda i mehaničkog oštećenja istih.
4. Nekvalitetno izvedenih i montiranih cijevi, armature i spojeva.
5. Nesigurnog i nepravilnog rukovanja i održavanja instalacije.
6. Nestručnog rukovanja i održavanja instalacije.
7. Nedovoljne termičke izolacije cjevovoda i opreme.
8. Nemogućnosti regulacije instalacije
9. Nepravilnog rasporeda ventilacionih kanala i mjesta za uzimanje spoljašnjeg vazduha i izbacivanje otpadnog vazduha.
10. Nepravilnog izbora materijala za ventilaciju kanala.
11. Prekomjernog odnosno nedovoljnog odvođenja toplote iz prostorija.
12. Velike brzine strujanja vazduha u prostorijama.
13. Nepravilnog rasporeda mjesta za ubacivanje i izvlačenje vazduha u prostorijama.
14. Pojave nedozvoljene buke u prostorijama, usled rada pojedinih uređaja u instalaciji ventilacije

#### **2. PREDVIĐENE MJERE ZA OTKLANJANJE OPASNOSTI I ŠTETNOSTI**

1. Na bazi izvedenog proračuna izvršeno je pravilno dimenzionisanje pojedinih elemenata instalacije i regulacione armature i uz primjenu važećih tehničkih normativa i standarda.
2. Spajanje instalacije vrši se pertlovanjem i odgovarajućim nastavcima i priključcima. Cijevi se postavljaju iz jednog komada tako da nema zavarenih spojeva.
3. Svi uređaji i oprema na elektro pogon su takve konstrukcije da obezbjeđuju sigurnu zaštitu od električnog napona.
4. Na izolaciji je predviđena odgovarajuća toplotna izolacija i antikoroziorna zaštita, kako ne bi došlo do brzog propadanja instalacije i gubitka toplotne energije.
5. Izvođač radova i proizvođač opreme su dužni da investitoru predaju sve ateste i uputstva za rad sa uređajima i cjelokupnom instalacijom.

6. Materijal i dimenzije kanala i rešetaka za vazduh je izabran prema propisima JUS-a i DIN-a. Sve rešetke su sa mogućnošću regulisanja dometa i količine vazduha.
7. Ventilatori i ostali izvori buke su odabrani i postavljeni tako da u prostorijama izazivaju što manju buku, odnosno buka mora biti u granicama koje određuju odgovarajući propisi.
8. Oprema se postavlja na električne podloge a veza između ventilatora i kanala je sa elastičnim kanalima.
9. Na ventilatore i žaluzine postavljeni su prigušivači buke, tako da je nivo buke u granicama koje određuju odgovarajući propisi.

### 3. OPŠTE NAPOMENE I OBAVEZE

1. Izvođač radova je obavezan da uradi poseban elaborat o uređenju gradilišta i o radu na gradilištu.
2. Proizvođač oruđa za rad na mehanizovani pogon je obavezan da dostavi uputstva za bezbjedan rad i da potvrdi da su na oruđu primijenjene mjere o zaštiti na radu odnosno dostavi uz oruđe za rad atest o primijenjenim propisima zaštite na radu.
3. Radna organizacija je obavezna da prije početka radova na 8 dana obavijesti nadležni organ i inspekciju rada o početku radova.
4. Radna organizacija je obavezna da izradi normativna akta iz oblasti zaštite na radu (Samoupravni sporazum o zaštiti na radu, Program za obučavanje i vaspitanje radnika iz oblasti zaštite, Pravilnik o pregledima, ispitivanjima i održavanju oruđa i alata, Program mjera i unapređenja zaštite na radu i dr.)
5. Radna organizacija je obavezna da izvrši obučavanje radnika iz materije zaštite na radu, opasnostima i zaštitama u vezi sa radom i obavi provjeru sposobnosti radnika za samostalan i bezbjedan rad.
6. Radna organizacija je obavezna da utvrdi radna mjesta sa posebnim uslovima rada ukoliko takva radna mjesta postoje.
7. Investitor je obavezan da rukovanje instalacijom povjeri stručnom čovjeku koji će se starati o ispunjavanju zahtjeva zakona zaštite na radu.
8. Projekat predlaže i navodi sledeće JUS propise i Zakone kojih se mora pridržavati Izvođač radova i korisnik objekta:
  - Zakon o zaštiti i zdravlju na radu
  - Interne propise i mjere o zaštiti na radu

### 4. ZAKLJUČAK

Projektom su predviđene sve potrebne mjere za otklanjanje opasnosti i štetnosti u pogledu zaštite na radu.

Odgovorni projektant,  
Vuk Janković, dipl.ing.maš.

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## 4. PROGRAM KONTROLE I OSIGURANJA KVALITETA

Ovim programom navode se mjere koje Izvođač radova u građenju predmetnog objekta moraju primijeniti kako bi se osigurao kvalitet pojedinih faza radova i objekta kao cjeline.

Program se odnosi na radnje koje slijede nakon završetka glavnog projekta i dobijanja građevinske dozvole, tekstualne i grafičke dokumente obavezne u fazi pripreme građenja. Mašinske termotehničke instalacije izvode se na osnovu projekta čiji je prilog ovaj program kontrole i osiguranja kvaliteta.

Sastavni dio projekta su:

- svi priloženi dokumenti projekta
- kompletni proračuni
- tehnički opis

Za sve promjene i odstupanja od ovog projekta mora se pribaviti pismena saglasnost Nadzornog inženjera, odnosno Projektanta.

Izvođač radova je dužan prije izvođenja proučiti projekat, a takođe provjeriti postojeće stanje. Za sva eventualna odstupanja potrebno je konsultovati Projektanta ili Nadzornog inženjera.

Materijal i oprema ugrađeni u instalaciju moraju biti odgovarajućeg kvaliteta i posjedovati ateste o ispitivanju. Pored materijala i sam rad mora biti kvalitetno izveden, a sve što bi se u toku rada i kasnije pokazalo nekvalitetno Izvođač radova je dužan o svom trošku otkloniti.

Sva oprema, mjerni instrumenti, a naročito sigurnosni uređaji moraju besprijekorno funkcionisati i u djelovanju biti sigurni.

Funkcionalnu probu instalacije grijanja, hlađenja i regulacija vrši se u periodu od 8 sati i trajanju od jednog do više dana što zavisi o složenosti i veličini instalacije te zahtjevu Nadzornog inženjera.

Ispitivanje je potrebno potvrditi zapisnicima i ustanoviti:

- radi li instalacija bez šumova i udaraca
- rade li regulacijski sklopovi (automatika) prema traženim projektnim parametrima
- pokazuju li svi kontrolni instrumenti ispravne podatke
- postoje li oznake na svim osnovnim elementima postrojenja kojima korisnik objekta mora rukovati
- postoje li odgovarajući priručnici za korišćenje i održavanje

Garantni rok za ispravnost uređaja i postrojenja teče od dana tehničkog prijema, odnosno predaje instalacije Investitoru na korišćenje. Garantni rok na kvalitetu izvršenog posla daje Izvođač radova na rok od dvije godine, odnosno prema odredbi Ugovora, a garantni rok na opremu daje Proizvođač prema svojim uslovima.

Instalacije smije izvoditi samo ovlašćeni Izvođač. U protivnom svu nastalu štetu snosi onaj ko je angažovao nestručnog Izvođača.

Tehnička primopredaja instalacija nakon završetka svih radova vrši se u prisustvu Nadzornog inženjera i predstavnika Investitora.

Ukoliko se prilikom predaje instalacije vrši i tehnički pregled u svrhu dobivanja upotrebne dozvole, prisutni su i predstavnici tijela nadležnog za izdavanje upotrebne dozvole.

### **MJERENJA I KONTROLNI PREGLEDI**

Najmanje jedanput godišnje treba izvršiti kontrolu i funkcionalno ispitivanje svih uređaja. Kontrola uređaja i opreme, kao što su filteri, mjerni uređaji i slično vrši se više puta u godini prema potrebi i

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tehničkim uslovima.

Sve uređaje i opremu koja ima posebnu namjenu i posebne tehničke zahtjeve treba kontrolisati i servisirati prema posebnim tehničkim uputstvima koje su date uz navedene uređaje.

Preventivno održavanje, kontrolu i servis mogu vršiti samo osobe koje su za to tehnički osposobljene i ovlaštene od strane odgovorne osobe.

**ATESTI, MJERENJA I ISPITIVANJA KOJE JE POTREBNO PRILOŽITI UZ ZAHTJEV ZA TEHNIČKI PREGLED**

- Elektro ateste na napon i otpor uzemljenja
- Zapisnik o probi na pritisak
- Uvjerjenje o kvalitetu cijevi
- Atesti ugrađene opreme i materijala
- Mjerenje o postignutim parametrima postrojenja: pritisci, temperature
- Atest o obavljenom funkcionalnom ispitivanju

ODGOVORNI INŽENJER,  
Vuk Janković, dipl.ing.maš.



## D) NUMERIČKA DOKUMENTACIJA

## 5. PRORAČUNI

Heat load sum up table

Room name	Fl	Sys -tem	Qty. of rooms	Cooling				Heating				Floor area	Heat load per area	
				Indoor SH	Total	Selected	Time	Total	Selected	Humid.	Time		Cooling	Heating
				[W]			[Hr]	[W]		[kg/h]	[Hr]		[W/m2]	
001 Hol	1	1	1	6410	9412	9883	14	7408	8149	1.35	8	180.2	54.8	45.2
008 Zenski wc	1	10	1	1417	1822	1913	16	1452	1597	0.17	8	25.3	75.6	63.1
010 Muski wc	1	10	1	1298	1706	1791	15	1355	1491	0.17	8	25.4	70.5	58.7
011 Stamp./kopirnica	1	1	1	3295	3925	4121	15	4051	4456	0.61	8	68.8	59.9	64.8
012 Modelarnica	1	1	1	7492	10510	11036	15	7364	8100	1.23	8	143.8	76.7	56.3
013 Visenamjen. sala	1	1	1	7870	10357	10875	14	8878	9766	1.72	8	192.0	56.6	50.9
015 Kafe/klub	1	2	1	10407	18940	19887	15	5948	6543	1.03	8	121.2	164.1	54.0
107 Centralni hol	2	4	1	16013	19598	20578	15	21285	23414	3.40	8	380.8	54.0	61.5
111 Biblioteka	2	4	1	6520	8177	8586	17	8142	8956	1.11	8	124.1	69.2	72.2
112 Student.sluzba 1	2	3	1	2275	2757	2895	18	2282	2510	0.28	8	31.3	92.5	80.2
113 Student.sluzba 2	2	3	1	2072	2555	2683	18	1895	2085	0.29	8	32.1	83.6	64.9
114 Vjezbaonica 1	2	3	1	7202	9626	10107	15	6292	6921	0.86	8	100.7	100.4	68.7
115 Vjezbaonica 2	2	3	1	6202	8632	9064	14	5184	5702	0.86	8	101.4	89.4	56.2
116 Vjezbaonica 3	2	4	1	6202	8632	9064	14	5184	5702	0.86	8	101.4	89.4	56.2
117 Vjezbaonica 4	2	4	1	6986	9416	9887	14	6350	6985	0.86	8	101.4	97.5	68.9
201 Centralni hol	3	6	1	12338	15005	15755	15	16078	17686	2.42	8	270.3	58.3	65.4
202 Diplomaska sala	3	5	1	4785	6208	6518	18	4295	4725	0.59	8	66.3	98.3	71.3
206 Vjezbaonica 5	3	5	1	7252	9676	10160	15	6292	6921	0.86	8	100.7	100.9	68.7
207 Vjezbaonica 6	3	5	1	6202	8632	9064	14	5184	5702	0.86	8	101.4	89.4	56.2
208 Vjezbaonica 7	3	5	1	6015	8438	8860	14	4955	5451	0.83	8	97.0	91.3	56.2
209 Vjezbaonica 8	3	6	1	6178	8607	9037	14	5148	5663	0.86	8	101.1	89.4	56.0
210 Vjezbaonica 9	3	6	1	6973	9403	9873	14	6325	6958	0.86	8	101.4	97.4	68.6
211 Toaleti	3	10	1	1449	1691	1776	17	984	1082	0.11	8	12.6	140.9	85.9
214 Racunovodstvo	3	6	1	1154	1472	1546	18	1056	1162	0.15	8	17.0	90.9	68.3
215 Prodekan 1	3	6	1	1545	1944	2041	18	1495	1645	0.20	8	22.5	90.7	73.1
216 Prodekan 2	3	6	1	1815	2220	2331	17	2067	2274	0.20	8	22.6	103.1	100.6
217 Pravna sluzba	3	6	1	1478	1891	1986	14	1456	1602	0.19	8	22.5	88.2	71.2
301 Hol	4	7	1	12942	15548	16325	14	16810	18491	2.06	18	221.3	73.8	83.6
302 Diplomaska sala	4	7	1	8201	12135	12742	18	5373	5910	0.65	18	69.9	182.3	84.6
306 Sala nast. osob.	4	7	1	3802	7591	7971	15	3540	3894	1.90	18	49.0	162.7	79.5
307 Kabinet dekana	4	7	1	3397	4377	4596	14	3015	3317	0.41	18	46.0	99.9	72.1
308 Amfiteatar	4	9	1	20195	38628	40559	15	21084	23192	8.68	18	215.2	188.5	107.8
309 Hodnik	4	8	1	4324	5195	5455	17	4891	5380	0.94	18	100.7	54.2	53.4
311 Toaleti	4	10	1	1516	1760	1848	17	1102	1212	0.14	18	14.6	126.6	83.0
313 Kabinet 1	4	8	1	1742	2139	2246	18	1333	1466	0.19	18	19.9	112.9	73.7
314 Kabinet 2	4	8	1	1742	2139	2246	18	1333	1466	0.19	18	19.9	112.9	73.7
315 Kabinet 3	4	8	1	1680	2075	2179	18	1247	1372	0.17	18	18.2	119.7	75.4
316 Kabinet 4	4	8	1	2155	2558	2686	17	2347	2582	0.19	18	20.9	128.5	123.5

SH : Sensible heat

Heat load sum up table

Room name	Fl	Sys -tem	Qty. of rooms	Cooling				Heating				Floor area	Heat load per area	
				Indoor SH	Total	Selected	Time	Total	Selected	Humid.	Time		Cooling	Heating
				[W]			[Hr]	[W]		[kg/h]	[Hr]		[W/m2]	
317 Kabinet 5	4	8	1	940	1189	1248	14	958	1054	0.13	18	14.1	88.5	74.7
318 Kabinet 6	4	8	1	1097	1349	1416	14	1140	1254	0.14	18	16.1	88.0	77.9
319 Kabinet 7	4	8	1	1937	2268	2381	14	2076	2284	0.16	18	18.1	131.6	126.2
320 Kabinet 8	4	8	1	1241	1568	1646	14	1119	1231	0.14	18	15.7	104.9	78.4
321 Kabinet 9	4	8	1	1255	1508	1583	14	1195	1315	0.15	18	17.2	92.1	76.4
322 Kabinet 10	4	8	1	1255	1508	1583	14	1195	1315	0.15	18	17.2	92.1	76.4
323 Kabinet 11	4	8	1	1185	1436	1508	14	1119	1231	0.14	18	15.7	96.0	78.4
324 Sekretarica	4	8	1	1301	1556	1634	14	1246	1371	0.16	18	18.2	89.8	75.3
325 Trpezarija	4	8	1	1628	3068	3221	15	1532	1685	0.77	18	23.3	138.3	72.3
326 Arhiv st.radovi	4	8	1	1073	1406	1476	15	1086	1195	0.38	18	23.4	63.1	51.1
327 Radna sala	4	8	1	1549	2987	3136	15	1460	1606	0.75	18	21.4	146.6	75.0
Peak load of building			49	218723	309170	324628	15	224606	247067	42.45	18	3661.3	88.7	67.5

SH : Sensible heat

Table of system heat load

Sys -tem	Cooling							Heating						
	Time	F/A vol	Indoor SH	Indoor	Outside	Total	Selected	Time	F/A vol	Indoor	Outside	Total	Selected	Humid.
	[Hr]	[m3/h]	[W]					[Hr]	[m3/h]	[W]				
1	15	0	24993	34114	0	34114	35820	8	0	27701	0	27701	30471	4.91
2	15	0	10407	18940	0	18940	19887	8	0	5948	0	5948	6543	1.03
3	15	0	17131	22983	0	22983	24132	8	0	15653	0	15653	17218	2.29
4	15	0	35013	45146	0	45146	47403	8	0	40961	0	40961	45057	6.24
5	15	0	23593	32324	0	32324	33940	8	0	20726	0	20726	22799	3.15
6	15	0	30744	39825	0	39825	41816	8	0	33625	0	33625	36988	4.89
7	17	1300	27725	37651	1003	38654	40587	18	1300	27065	1673	28738	31612	5.01
8	14	1150	24252	31045	1159	32204	33814	18	1150	23796	1481	25277	27805	4.74
9	15	6100	20195	32587	6041	38628	40559	18	6100	13233	7851	21084	23192	8.68
10	16	0	5617	6918	0	6918	7264	18	0	4893	0	4893	5382	0.61

F/A : Fresh air  
SH : Sensible heat

## Table of peak heat load detail(Cooling)

[Room name:001 Hol ]		Floor: 1F	Floor area: 180.2m2	Ceiling height: 3.8m	Peak time in cooling:14:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:35.4CDB	, 35.6%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
Shade	333	(35.40-26.00)	2.20	16.1	
	374			(16.1*0.95)	72
Skylight					0.34
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE	104	14.20	0.60	( 3.2*3.8- 0.0)	
SW					
NW	50	6.80	0.60	( 3.2*3.8- 0.0)	
Shade	69	3.60	0.60	(12.7*3.8-16.1)	
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist	949	(35.40-26.00)*0.40	1.40	180.2	
Flat roof					
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer					
Without air layer					
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
425 136.95 (35.40-26.00)					
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
266 136.95 (12.82-10.49)					
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp 2090 1.160 1802 1.00					
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
2016 56 36 1.00					
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
2736 76 36 1.00					
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
9412 6410 3002					
[ 8094] (kcal/h) [ 5513] [ 2582]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
9412 9412 0 0					
[ 8094] (kcal/h) [ 8094] [ 0] [ 0]					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					

## Table of peak heat load detail(Heating)

[Room name:001 Hol ]		Floor: 1F	Floor area: 180.2m2	Ceiling height: 3.8m	Peak time in heating: 8:00
Indoor temperature:18.0CDB		, 50.0%RH	Outdoor temperature:-6.0CDB	, 81.8%RH	
<1> Load of window glass = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
Shade					
Skylight					
	935	1.10	1.00	(18.00+ 6.00)	0.00 2.20 16.1
<2> Load of outer wall = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
Shade					
	184	1.05	1.00	(18.00+ 6.00)	0.00 0.60 ( 3.2*3.8- 0.0)
	193	1.10	1.00	(18.00+ 6.00)	0.00 0.60 ( 3.2*3.8- 0.0)
	509	1.10	1.00	(18.00+ 6.00)	0.00 0.60 (12.7*3.8-16.1)
(!Area of outer wall=length of outer wall*floor height[ceiling height+height of ceiling adv.attic.] -window area)					
<3> Load of roof = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area					
Overhead room exit					
Flat roof					
Inclined roof					
	2422	---	---	(18.00+ 6.00)*0.40	1.40 180.2
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer					
Without air layer					
Pilotis					
	1375	(18.00- 8.47)	0.80	180.2	
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
	1790	225.97	(18.00+ 6.00)		
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
	855	225.97	( 6.40- 1.86)		
(Humidifying vol.)(g/h) = infiltration vol. * abs.humid.diff. * 1.2 * safety factor					
	1354	225.97	( 6.40- 1.86)	1.10	
!Infiltration vol. = No of ventilation * azimuth factor * room capacity					
	225.97	0.30	1.10	684.76	
<8> Load of lighting = -(heat gain/W * lighting consumption vol. * ope.rate * probable rate)					
Fluorescent lamp					
Incandescent lamp					
<9> Load of human body(SH) = -(SH of human body * No of psns * ope.rate * probable rate)					
<10> Load of equipments = -(heat gain from internal equip. * operating rate * probable rate)					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833 * (1 - THEX)					
(Humidifying vol.) = F/A vol. * abs.humid.diff. * 1.2 * safety factor * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
	7408	7408	0		
	[ 6371] (kcal/h)	[ 6371]	[ 0]		
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
	7408	7408	0	0	
	[ 6371] (kcal/h)	[ 6371]	[ 0]	[ 0]	
!Indoor heat load & total heat load are not contained latent heat.					
Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air					
	1354	1354	0		
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					

## Table of peak heat load detail(Cooling)

[Room name:008 Zenski wc ]		Floor: 1F	Floor area: 25.3m2	Ceiling height: 2.9m	Peak time in cooling:16:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:34.4CDB	, 36.8%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW	33	(34.40-26.00)	2.20	1.8	
Shade	191			( 1.8*0.95)	329 0.34
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE	88	10.10	0.60	( 5.0*2.9- 0.0)	
SE					
SW					
NW	44	10.20	0.60	( 3.1*2.9- 1.8)	
Shade	34	5.70	0.60	( 3.4*2.9- 0.0)	
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist	119	(34.40-26.00)*0.40	1.40	25.3	
Flat roof					
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer					
Without air layer					
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
41 14.67 (34.40-26.00)					
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
25 14.67 (12.54-10.49)					
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp 587 1.160 506 1.00					
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
280 56 5 1.00					
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
380 76 5 1.00					
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
1822 1417 405					
[ 1567] (kcal/h) [ 1219] [ 348]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
1822 1822 0 0					
[ 1567] (kcal/h) [ 1567] [ 0] [ 0]					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					



Table of peak heat load detail(Heating)

[Room name:008 Zenski wc ]		Floor: 1F	Floor area: 25.3m2	Ceiling height: 2.9m	Peak time in heating: 8:00
Indoor temperature:20.0CDB		, 50.0%RH	Outdoor temperature:-6.0CDB	, 81.8%RH	
<1> Load of window glass = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW	113	1.10	1.00	(20.00+ 6.00)	0.00 2.20 1.8
Shade					
Skylight					
<2> Load of outer wall = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE	238	1.05	1.00	(20.00+ 6.00)	0.00 0.60 ( 5.0*2.9- 0.0)
SE					
SW					
NW	123	1.10	1.00	(20.00+ 6.00)	0.00 0.60 ( 3.1*2.9- 1.8)
Shade	169	1.10	1.00	(20.00+ 6.00)	0.00 0.60 ( 3.4*2.9- 0.0)
(!Area of outer wall=length of outer wall*floor height[ceiling height+height of ceiling adv.attic.]-window area)					
<3> Load of roof = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area					
Overhead room exit	368	---	---	(20.00+ 6.00)*0.40	1.40 25.3
Flat roof					
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor	233	(20.00- 8.47)	0.80		25.3
With air layer					
Without air layer					
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
	208	24.21	(20.00+ 6.00)		
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
	109	24.21	( 7.26- 1.86)		
(Humidifying vol.)(g/h) = infiltration vol. * abs.humid.diff. * 1.2 * safety factor					
	173	24.21	( 7.26- 1.86)	1.10	
!Infiltration vol. = No of ventilation * azimuth factor * room capacity					
	24.21	0.30	1.10	73.37	
<8> Load of lighting = -(heat gain/W * lighting consumption vol. * ope.rate * probable rate)					
Fluorescent lamp					
Incandescent lamp					
<9> Load of human body(SH) = -(SH of human body * No of psns * ope.rate * probable rate)					
<10> Load of equipments = -(heat gain from internal equip. * operating rate * probable rate)					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833 * (1 - THEX)					
(Humidifying vol.) = F/A vol. * abs.humid.diff. * 1.2 * safety factor * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
	1452	1452	0		
	[ 1249] (kcal/h)	[ 1249]	[ 0]		
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
	1452	1452	0	0	
	[ 1249] (kcal/h)	[ 1249]	[ 0]	[ 0]	
!Indoor heat load & total heat load are not contained latent heat.					
Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air					
	173	173	0		
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					

### Table of peak heat load detail(Cooling)

[Room name:010 Muski wc	]	Floor: 1F	Floor area: 25.4m2	Ceiling height: 2.9m	Peak time in cooling:15:00
Indoor temperature:26.0CDB	,	50.0%RH	Outdoor temperature:35.3CDB	,	35.6%RH

```

Load of window glass
- Material I / with blind-
Upper: heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.
Lower: solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.
Azimuth
N
E
S
W
NE
SE
SW
NW
Shade
Skylight

<2> Load of outer wall = effective temp.diff. * OHTC * area
Azimuth
N
E
S
W
NE 87 10.40 0.60 ( 4.8*2.9= 0.0)
SE 165 14.40 0.60 ( 6.6*2.9= 0.0)
SW
NW
Shade
(!Area of outer wall=length of outer wall
*floor height[ceiling height+height of ceiling adv attic]-window area)

<3> Load of roof = effective temp.diff. * OHTC * area
Overhead room exist 132 (35.30-26.00)*0.40 1.40 25.4
Flat roof
Inclined roof

<4> Load of floor = temp.diff. * OHTC * area
Earth floor
With air layer
Without air layer
Pilotis

<5> Load of inner wall = temp.diff. * OHTC * area
Azimuth
N
E
S
W
NE
SE
SW
NW

<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length
(depth<=2.4m)
Load of underground wall = temp.diff. * OHTC * area

<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33
45 14.73 (35.30-26.00)
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833
28 14.73 (12.75-10.49)

<8> Load of lighting = heat gain/W * lighting consumption vol. * operate
Fluorescent lamp 589 1.160 508 1.00
Incandescent lamp

<9> Load of human body(SH) = SH of human body * No of psns. * operate
280 56 5 1.00
Load of human body(LH) = LH of human body * No of psns. * operate
380 76 5 1.00

<10> Load of equipments = heat gain from internal equip. * operating rate

<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH
1706 1298 408
[ 1467] (kcal/h) [ 1116] [ 351]
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)
1706 1706 0 0
[ 1467] (kcal/h) [ 1467] [ 0] [ 0]

OHTC : Overall heat transfer coefficient
SH : Sensible heat
LH : Latent heat
F/A : Fresh air
THEX : Total heat exchange efficiency

```

## Table of peak heat load detail(Heating)

[Room name:010 Muski wc ] , Floor: 1F Floor area: 25.4m<sup>2</sup> Ceiling height: 2.9m Peak time in heating: 8:00  
 Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 81.8%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE  
 SE  
 SW  
 NW  
 Shade  
 Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE 228 1.05 1.00 (20.00+ 6.00) 0.00 0.60 ( 4.8\*2.9- 0.0)  
 SE 314 1.05 1.00 (20.00+ 6.00) 0.00 0.60 ( 6.6\*2.9- 0.0)  
 SW  
 NW  
 Shade  
 (!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Overhead room exit 370 --- --- (20.00+ 6.00)\*0.40 --- 1.40 25.4  
 Flat roof  
 Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
 Earth floor 234 (20.00- 8.47) 0.80 25.4  
 With air layer  
 Without air layer  
 Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE  
 SE  
 SW  
 NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
 (depth<=2.4m)  
 Load of underground wall = temp.diff. \* OHTC \* area  
 (depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m<sup>3</sup>/h) \* temp.diff. \* 0.33  
 209 24.31 (20.00+ 6.00)  
 Load of infiltration(LH) = infiltration vol.(m<sup>3</sup>/h) \* abs.humid.diff.(g/kg) \* 0.833  
 109 24.31 ( 7.26- 1.86)  
 (Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
 173 24.31 ( 7.26- 1.86) 1.10  
 !Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
 24.31 0.30 1.10 73.66

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
 Fluorescent lamp  
 Incandescent lamp

<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)

<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)

<11> Fresh air load(SH) = F/A vol.(m<sup>3</sup>/h) \* temp.diff. \* 0.33 \* (1 - THEX)

Fresh air load(LH) = F/A vol.(m<sup>3</sup>/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)

(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
 1355 1355 0  
 [ 1165] (kcal/h) [ 1165] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
 1355 1355 0 0  
 [ 1165] (kcal/h) [ 1165] [ 0] [ 0]

!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
 173 173 0

OHTC : Overall heat transfer coefficient  
 SH : Sensible heat  
 LH : Latent heat  
 F/A : Fresh air  
 THEX : Total heat exchange efficiency



## Table of peak heat load detail(Heating)

[Room name:011 Stamp./kopirnica] Floor: 1F Floor area: 68.8m<sup>2</sup> Ceiling height: 3.8m Peak time in heating: 8:00  
 Indoor temperature:20.0CDB, 50.0%RH Outdoor temperature:-6.0CDB, 81.8%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE  
 SE  
 SW  
 NW  
 Shade  
 Skylight  
 805 1.10 1.00 (20.00+ 6.00) 0.00 2.20 12.8

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE  
 SE  
 SW  
 NW  
 Shade  
 417 1.05 1.00 (20.00+ 6.00) 0.00 0.60 ( 6.7\*3.8- 0.0)  
 452 1.10 1.00 (20.00+ 6.00) 0.00 0.60 (10.3\*3.8-12.8)  
 (!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Overhead room exit 1002 --- --- (20.00+ 6.00)\*0.40 --- 1.40 68.8  
 Flat roof  
 Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
 Earth floor 635 (20.00- 8.47) 0.80 68.8  
 With air layer  
 Without air layer  
 Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE  
 SE  
 SW  
 NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
 (depth<=2.4m)  
 Load of underground wall = temp.diff. \* OHTC \* area  
 (depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m<sup>3</sup>/h) \* temp.diff. \* 0.33  
 740 86.28 (20.00+ 6.00)  
 Load of infiltration(LH) = infiltration vol.(m<sup>3</sup>/h) \* abs.humid.diff.(g/kg) \* 0.833  
 388 86.28 ( 7.26- 1.86)  
 (Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
 615 86.28 ( 7.26- 1.86) 1.10  
 !Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
 86.28 0.30 1.10 261.44

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
 Fluorescent lamp  
 Incandescent lamp

<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)

<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)

<11> Fresh air load(SH) = F/A vol.(m<sup>3</sup>/h) \* temp.diff. \* 0.33 \* (1 - THEX)

Fresh air load(LH) = F/A vol.(m<sup>3</sup>/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)

(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
 4051 4051 0  
 [ 3484] (kcal/h) [ 3484] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
 4051 4051 0 0  
 [ 3484] (kcal/h) [ 3484] [ 0] [ 0]  
 !Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
 615 615 0

OHTC : Overall heat transfer coefficient  
 SH : Sensible heat  
 LH : Latent heat  
 F/A : Fresh air  
 THEX : Total heat exchange efficiency

Table of peak heat load detail(Cooling)

Room name:012 Modelarnica		Floor: 1F	Floor area: 143.9m2		Ceiling height: 3.8m	Peak time in cooling:15:00	
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:35.3CDB		, 35.6%RH		
<1> Load of window glass							
-Material I / with blind-							
Upper:heat transfer load = temp.diff. * OHTC * area				(!Area of heat transf. is contained sash area.			
Lower:solar heat load =				area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.			
Azimuth							
N							
E							
S							
W							
NE							
	129	(35.30-26.00)	2.20	6.3			
	165			( 6.3*0.95)	81		0.34
SE							
	129	(35.30-26.00)	2.20	6.3			
	781			( 6.3*0.95)	384		0.34
NW							
Shade							
Skylight							
<2> Load of outer wall = effective temp.diff. * OHTC * area							
Azimuth							
N							
E							
S							
W							
NE							
	198	10.40		0.60	(10.0*3.8- 6.3)		
SE							
	228	12.00		0.60	(10.0*3.8- 6.3)		
SW							
	204	8.70		0.60	(10.3*3.8- 0.0)		
NW							
Shade							
(!Area of outer wall=length of outer wall							
*floor height[ceiling height+height of ceiling adv attic]-window area)							
<3> Load of roof = effective temp.diff. * OHTC * area							
Overhead room exist							
	749	(35.30-26.00)*0.40	1.40		143.8		
Flat roof							
Inclined roof							
<4> Load of floor = temp.diff. * OHTC * area							
Earth floor							
With air layer							
Without air layer							
Pilotis							
<5> Load of inner wall = temp.diff. * OHTC * area							
Azimuth							
N							
E							
S							
W							
NE							
	10510						
SE							
SW							
NW							
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length							
(depth<=2.4m)							
Load of underground wall = temp.diff. * OHTC * area							
(depth>2.4m)							
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33							
	335			109.29		(35.30-26.00)	
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833							
	206			109.29		(12.75-10.49)	
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate							
Fluorescent lamp							
	2502	1.160		2157		1.00	
Incandescent lamp							
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate							
	2072	56		37		1.00	
Load of human body(LH) = LH of human body * No of psns. * ope.rate							
	2812	76		37		1.00	
<10> Load of equipments = heat gain from internal equip. * operating rate							
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)							
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)							
<<Total>> Indoor heat load(W) = SH + LH							
	10510			7492		3018	
	[ 9039]	(kcal/h)		[ 6443]		[ 2595]	
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)							
	10510			10510		0	
	[ 9039]	(kcal/h)		[ 9039]		[ 0]	
						[ 0]	
OHTC : Overall heat transfer coefficient							
SH : Sensible heat							
LH : Latent heat							
F/A : Fresh air							
THEX : Total heat exchange efficiency							

## Table of peak heat load detail(Heating)

[Room name:012 Modelarnica ] Floor: 1F Floor area: 143.8m2 Ceiling height: 3.8m Peak time in heating: 8:00  
 Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 81.8%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE 378 1.05 1.00 (20.00+ 6.00) 0.00 2.20 6.3  
 SE  
 SW 378 1.05 1.00 (20.00+ 6.00) 0.00 2.20 6.3  
 NW  
 Shade  
 Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE 519 1.05 1.00 (20.00+ 6.00) 0.00 0.60 (10.0\*3.8- 6.3)  
 SE 519 1.05 1.00 (20.00+ 6.00) 0.00 0.60 (10.0\*3.8- 6.3)  
 SW 672 1.10 1.00 (20.00+ 6.00) 0.00 0.60 (10.3\*3.8- 0.0)  
 NW  
 Shade  
 (!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Overhead room exit 2094 --- --- (20.00+ 6.00)\*0.40 --- 1.40 143.8  
 Flat roof  
 Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
 Earth floor 1327 (20.00- 8.47) 0.80 143.8  
 With air layer  
 Without air layer  
 Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE  
 SE  
 SW  
 NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
 (depth<=2.4m)  
 Load of underground wall = temp.diff. \* OHTC \* area  
 (depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
 1477 172.13 (20.00+ 6.00)  
 Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
 774 172.13 ( 7.26- 1.86)  
 (Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
 1227 172.13 ( 7.26- 1.86) 1.10  
 !Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
 172.13 0.30 1.05 546.44

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
 Fluorescent lamp  
 Incandescent lamp

<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)

<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)

<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)

Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)

(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
 7364 7364 0  
 [ 6333] (kcal/h) [ 6333] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
 7364 7364 0 0  
 [ 6333] (kcal/h) [ 6333] [ 0] [ 0]  
 !Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
 1227 1227 0

OHTC : Overall heat transfer coefficient  
 SH : Sensible heat  
 LH : Latent heat  
 F/A : Fresh air  
 THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

[Room name:013 Visenamjen. sala]		Floor: 1F	Floor area: 192.0m2	Ceiling height: 3.8m	Peak time in cooling:14:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:35.4CDB	, 35.6%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load		= temp.diff.	* OHTC * area	(!Area of heat transf. is contained sash area.	
Lower:solar heat load		=	area * std.solar heat gain * shading factor	(!Area of solar heat gain is not contained sash area.	
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
Shade	728	(35.40-26.00)	2.20	35.2	
	819			(35.2*0.95)	72
Skylight					0.34
<2> Load of outer wall					
		= effective temp.diff. * OHTC * area			
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
Shade	148	3.60	0.60	(27.3*3.8-35.2)	
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof					
		= effective temp.diff. * OHTC * area			
Overhead room exist	757	(35.40-26.00)*0.40	1.40	143.8	
Flat roof					
Inclined roof					
<4> Load of floor					
		= temp.diff. * OHTC * area			
Earth floor					
With air layer					
Without air layer					
Pilotis					
<5> Load of inner wall					
		= temp.diff. * OHTC * area			
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall					
(depth<=2.4m)		= temp.diff. * OHTC/unit ambient length * ambient length			
Load of underground wall					
(depth>2.4m)		= temp.diff. * OHTC * area			
<7> Load of infiltration(SH)					
		= infiltration vol.(m3/h) * temp.diff. * 0.33			
Azimuth		(35.40-26.00)			
N		453			
E		145.92			
Load of infiltration(LH)					
		= infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833			
N		283			
E		145.92			
S		(12.82-10.49)			
<8> Load of lighting					
		= heat gain/W * lighting consumption vol. * ope.rate			
Fluorescent lamp	3341	1.160	2880	1.00	
Incandescent lamp					
<9> Load of human body(SH)					
		= SH of human body * No of psns. * ope.rate			
N		1624			
E		56			
S		29			
W		1.00			
Load of human body(LH)					
		= LH of human body * No of psns. * ope.rate			
N		2204			
E		76			
S		29			
W		1.00			
<10> Load of equipments					
		= heat gain from internal equip. * operating rate			
<11> Fresh air load(SH)					
		= F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)			
Fresh air load(LH)					
		= F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)			
<<Total>> Indoor heat load(W)					
		= SH + LH			
N		10357			
E		7870			
S		2487			
W		[ 8907] (kcal/h) [ 6768] [ 2139]			
Total heat load(W)					
		= indoor heat load + fresh air load(SH) + fresh air load(LH)			
N		10357			
E		10357			
S		0			
W		0			
NE		[ 8907] (kcal/h) [ 8907] [ 0] [ 0]			
SE					
SW					
NW					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					



## Table of peak heat load detail(Heating)

[Room name:013 Visenamjen. sala] , Floor: 1F Floor area: 192.0m2 Ceiling height: 3.8m Peak time in heating: 8:00  
 Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 81.8%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE  
 SE  
 SW  
 NW  
 Shade 2215 1.10 1.00 (20.00+ 6.00) 0.00 2.20 35.2  
 Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE  
 SE  
 SW  
 NW  
 Shade 1176 1.10 1.00 (20.00+ 6.00) 0.00 0.60 (27.3\*3.8-35.2)  
 (!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Overhead room exit 2094 --- --- (20.00+ 6.00)\*0.40 --- 1.40 143.8  
 Flat roof  
 Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
 Earth floor 1327 (20.00- 8.47) 0.80 143.8  
 With air layer  
 Without air layer  
 Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE  
 SE  
 SW  
 NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
 (depth<=2.4m)  
 Load of underground wall = temp.diff. \* OHTC \* area  
 (depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
 2066 240.77 (20.00+ 6.00)  
 Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
 1083 240.77 ( 7.26- 1.86)  
 (Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
 1716 240.77 ( 7.26- 1.86) 1.10  
 !Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
 240.77 0.30 1.10 729.60

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
 Fluorescent lamp  
 Incandescent lamp

<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)

<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)

<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)

Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)

(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
 8878 8878 0  
 [ 7635] (kcal/h) [ 7635] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
 8878 8878 0 0  
 [ 7635] (kcal/h) [ 7635] [ 0] [ 0]  
 !Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
 1716 1716 0

OHTC : Overall heat transfer coefficient  
 SH : Sensible heat  
 LH : Latent heat  
 F/A : Fresh air  
 THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

[Room name:015 Kafe/klub ]		Floor: 1F	Floor area: 121.2m2	Ceiling height: 3.8m	Peak time in cooling:15:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:35.3CDB	, 35.6%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE	65	(35.30-26.00)	2.20	3.2	
SW	84			( 3.2*0.95)	81 0.34
NW					
Shade					
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE	91	14.40	0.60	( 3.6*3.8- 3.2)	
SE	44	12.00	0.60	( 1.6*3.8- 0.0)	
SW					
NW					
Shade	237	5.00	0.60	(20.8*3.8- 0.0)	
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist	631	(35.30-26.00)*0.40	1.40	121.2	
Flat roof					
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer					
Without air layer					
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
283 92.11 (35.30-26.00)					
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
173 92.11 (12.75-10.49)					
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp 2812 1.160 2424 1.00					
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
6160 56 110 1.00					
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
8360 76 110 1.00					
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
18940 10407 8533					
[ 16288] (kcal/h) [ 8950] [ 7338]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
18940 18940 0 0					
[ 16288] (kcal/h) [ 16288] [ 0] [ 0]					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					

## Table of peak heat load detail(Heating)

[Room name:015 Kafe/klub ] Floor: 1F Floor area: 121.2m2 Ceiling height: 3.8m Peak time in heating: 8:00  
 Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 81.8%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE  
 SE 192 1.05 1.00 (20.00+ 6.00) 0.00 2.20 3.2  
 SW  
 NW  
 Shade  
 Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE  
 SE 172 1.05 1.00 (20.00+ 6.00) 0.00 0.60 ( 3.6\*3.8- 3.2)  
 SW 100 1.05 1.00 (20.00+ 6.00) 0.00 0.60 ( 1.6\*3.8- 0.0)  
 NW  
 Shade 1356 1.10 1.00 (20.00+ 6.00) 0.00 0.60 (20.8\*3.8- 0.0)  
 (!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Overhead room exit 1765 --- --- (20.00+ 6.00)\*0.40 --- 1.40 121.2  
 Flat roof  
 Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
 Earth floor 1118 (20.00- 8.47) 0.80 121.2  
 With air layer  
 Without air layer  
 Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE  
 SE  
 SW  
 NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
 (depth<=2.4m)  
 Load of underground wall = temp.diff. \* OHTC \* area  
 (depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
 1245 145.08 (20.00+ 6.00)  
 Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
 653 145.08 ( 7.26- 1.86)  
 (Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
 1034 145.08 ( 7.26- 1.86) 1.10  
 !Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
 145.08 0.30 1.05 460.56

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
 Fluorescent lamp  
 Incandescent lamp

<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)

<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)

<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)

Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)

(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
 5948 5948 0  
 [ 5115] (kcal/h) [ 5115] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
 5948 5948 0 0  
 [ 5115] (kcal/h) [ 5115] [ 0] [ 0]  
 !Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
 1034 1034 0

OHTC : Overall heat transfer coefficient  
 SH : Sensible heat  
 LH : Latent heat  
 F/A : Fresh air  
 THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

[Room name:107 Centralni hol ]		Floor: 2F	Floor area: 380.9m2	Ceiling height: 3.8m	Peak time in cooling:15:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:35.3CDB	, 35.6%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW	352	(35.30-26.00)	2.20	17.2	
	1389			(17.2*0.95)	250
Shade	1178	(35.30-26.00)	2.20	57.6	
	1191			(57.6*0.95)	64
Skylight					0.34
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
	71	10.40	0.60	( 3.0*3.8- 0.0)	
SE	68	12.00	0.60	( 2.5*3.8- 0.0)	
NW	164	8.70	0.60	(12.8*3.8-17.2)	
Shade	89	5.00	0.60	(23.0*3.8-57.6)	
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist					
	1983	(35.30-26.00)*0.40	1.40	380.8	
Flat roof					
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer					
	1983	(35.30-26.00)*0.40	1.40	380.8	
Without air layer					
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
888 289.41 (35.30-26.00)					
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
545 289.41 (12.75-10.49)					
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp 4417 1.160 3808 1.00					
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
2240 56 40 1.00					
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
3040 76 40 1.00					
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
19598 16013 3585					
[ 16854] (kcal/h) [ 13771] [ 3083]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
19598 19598 0 0					
[ 16854] (kcal/h) [ 16854] [ 0] [ 0]					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					

## Table of peak heat load detail(Heating)

[Room name:107 Centralni hol ] Floor: 2F Floor area: 380.8m2 Ceiling height: 3.8m Peak time in heating: 8:00  
Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 81.8%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW 1082 1.10 1.00 (20.00+ 6.00) 0.00 2.20 17.2  
Shade 3624 1.10 1.00 (20.00+ 6.00) 0.00 2.20 57.6  
Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE 187 1.05 1.00 (20.00+ 6.00) 0.00 0.60 ( 3.0\*3.8- 0.0)  
SE  
SW 156 1.05 1.00 (20.00+ 6.00) 0.00 0.60 ( 2.5\*3.8- 0.0)  
NW 540 1.10 1.00 (20.00+ 6.00) 0.00 0.60 (12.8\*3.8-17.2)  
Shade 511 1.10 1.00 (20.00+ 6.00) 0.00 0.60 (23.0\*3.8-57.6)  
(!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Overhead room exit 5544 --- --- (20.00+ 6.00)\*0.40 --- 1.40 380.8  
Flat roof  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer 5544 (20.00+ 6.00)\*0.40 1.40 380.8  
Without air layer  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
4097 477.52 (20.00+ 6.00)  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
2148 477.52 ( 7.26- 1.86)  
(Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
3404 477.52 ( 7.26- 1.86) 1.10  
!Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
477.52 0.30 1.10 1447.04

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
Fluorescent lamp  
Incandescent lamp

<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)

<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)

<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)

Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)

(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
21285 21285 0  
[ 18305] (kcal/h) [ 18305] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
21285 21285 0 0  
[ 18305] (kcal/h) [ 18305] [ 0] [ 0]  
!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
3404 3404 0

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

Table of peak heat load detail(Cooling)

Room name:111 Biblioteka		Floor: 2F	Floor area: 124.1m2	Ceiling height: 3.8m	Peak time in cooling:17:00	
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:33.3CDB	, 38.2%RH		
<1> Load of window glass						
-Material I / with blind-						
Upper:heat transfer load		= temp.diff.	* OHTC	* area	(!Area of heat transf. is contained sash area.	
Lower:solar heat load		=	area	* std.solar heat gain * shading factor	(!Area of solar heat gain is not contained sash area.	
Azimuth						
N						
E						
S						
W						
NE		198	(33.30-26.00)	2.20	12.3	
SE		187			See <1>>Load detail of window glass with canopy	
SW						
NW		347	(33.30-26.00)	2.20	21.6	
Shade		1554			See <1>>Load detail of window glass with canopy	
Skylight						
<2> Load of outer wall						
		= effective temp.diff.	* OHTC	* area		
Azimuth						
N						
E						
S						
W						
NE		142	9.80	0.60	( 9.6*3.8-12.3)	
SE						
SW						
NW		291	11.90	0.60	(16.4*3.8-21.6)	
Shade						
(!Area of outer wall=length of outer wall						
*floor height[ceiling height+height of ceiling adv attic]-window area)						
<3> Load of roof						
		= effective temp.diff.	* OHTC	* area		
Overhead room exist		507	(33.30-26.00)*0.40	1.40	124.1	
Flat roof						
Inclined roof						
<4> Load of floor						
		= temp.diff.	* OHTC	* area		
Earth floor						
With air layer						
Without air layer		507	(33.30-26.00)*0.40	1.40	124.1	
Pilotis						
<5> Load of inner wall						
		= temp.diff.	* OHTC	* area		
Azimuth						
N						
E						
S						
W						
NE						
SE						
SW						
NW						
<6> Load of underground wall						
(depth<=2.4m)		= temp.diff.	* OHTC/unit ambient length	* ambient length		
Load of underground wall						
(depth>2.4m)		= temp.diff.	* OHTC	* area		
<7> Load of infiltration(SH)						
		= infiltration vol.(m3/h)	* temp.diff.	* 0.33		
		227	94.32		(33.30-26.00)	
Load of infiltration(LH)						
		= infiltration vol.(m3/h)	* abs.humid.diff.(g/kg)	* 0.833		
		137	94.32		(12.23-10.49)	
<8> Load of lighting						
		= heat gain/W	* lighting consumption vol.	* ope.rate		
Fluorescent lamp		1440	1.160	1241	1.00	
Incandescent lamp						
<9> Load of human body(SH)						
		= SH of human body	* No of psns.	* ope.rate		
		1120	56	20	1.00	
Load of human body(LH)						
		= LH of human body	* No of psns.	* ope.rate		
		1520	76	20	1.00	
<10> Load of equipments						
		= heat gain from internal equip.	* operating rate			
<11> Fresh air load(SH)						
		= F/A vol.(m3/h)	* temp.diff.	* 0.33	* (1 - THEX)	
Fresh air load(LH)						
		= F/A vol.(m3/h)	* abs.humid.diff.	* 0.833	* (1 - THEX)	
<<Total>> Indoor heat load(W)						
		=	SH	+	LH	
		8177	6520		1657	
		[ 7032] (kcal/h)	[ 5607]		[ 1425]	
Total heat load(W)						
		= indoor heat load	+	fresh air load(SH)	+	fresh air load(LH)
		8177		0		0
		[ 7032] (kcal/h)	[ 7032]	[ 0]		[ 0]
OHTC : Overall heat transfer coefficient						
SH : Sensible heat						
LH : Latent heat						
F/A : Fresh air						
THEX : Total heat exchange efficiency						

Table of peak heat load detail of window with canopy(Cooling)

<1'> Load detail of window glass with canopy

Upper:solar heat load		=		(S.SHG - S.SHG for shadow) * SG + S.SHG for shadow		* shading factor * area		
Lower:SG		=		( x * y ) / ( Ww * Hw )		<tanF, tanG>		(!Area of heat transf. is contained sash area.
								S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.
Azimuth	911	351	39		0.6	39		0.34 (21.60 * 0.95)
NW	0.6	1.03	1.81	1.4	2.2		< 0.53,	-0.73>
NW	188	351	39		0.5	39	< 0.34	(21.60 * 0.95)
	0.5	0.82	1.81	1.4	2.2		< 0.53,	-0.73>
NW	455	351	39		0.6	39	< 0.34	(21.60 * 0.95)
	0.6	1.03	1.81	1.4	2.2		< 0.53,	-0.73>
NE	47	47	39		1.0	39	< 0.34	(12.30 * 0.95)
	1.0	1.40	2.20	1.4	2.2		< 0.34 0,	0>
NE	94	47	39		1.0	39	< 0.34 0,	(12.30 * 0.95)
	1.0	1.40	2.20	1.4	2.2		< 0.34 0,	0>
NE	47	47	39		1.0	39	< 0.34 0,	(12.30 * 0.95)
	1.0	1.40	2.20	1.4	2.2		< 0.34 0,	0>

## Table of peak heat load detail(Heating)

[Room name:111 Biblioteka ]		Floor: 2F	Floor area: 124.1m2	Ceiling height: 3.8m	Peak time in heating: 8:00
Indoor temperature:20.0CDB		, 50.0%RH	Outdoor temperature:-6.0CDB	, 81.8%RH	
<1> Load of window glass = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE	739	1.05	1.00	(20.00+ 6.00)	0.00 2.20 12.3
SE					
SW					
NW	1359	1.10	1.00	(20.00+ 6.00)	0.00 2.20 21.6
Shade					
Skylight					
<2> Load of outer wall = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE	396	1.05	1.00	(20.00+ 6.00)	0.00 0.60 ( 9.6*3.8-12.3)
SE					
SW					
NW	699	1.10	1.00	(20.00+ 6.00)	0.00 0.60 (16.4*3.8-21.6)
Shade					
(!Area of outer wall=length of outer wall*floor height[ceiling height+height of ceiling adv.attic.]-window area)					
<3> Load of roof = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area					
Overhead room exit	1807	---	---	(20.00+ 6.00)*0.40	1.40 124.1
Flat roof					
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer	1807	(20.00+ 6.00)*0.40	1.40	124.1	
Without air layer					
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
	1335	155.62	(20.00+ 6.00)		
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
	700	155.62	( 7.26- 1.86)		
(Humidifying vol.)(g/h) = infiltration vol. * abs.humid.diff. * 1.2 * safety factor					
	1109	155.62	( 7.26- 1.86)	1.10	
!Infiltration vol. = No of ventilation * azimuth factor * room capacity					
	155.62	0.30	1.10	471.58	
<8> Load of lighting = -(heat gain/W * lighting consumption vol. * ope.rate * probable rate)					
Fluorescent lamp					
Incandescent lamp					
<9> Load of human body(SH) = -(SH of human body * No of psns * ope.rate * probable rate)					
<10> Load of equipments = -(heat gain from internal equip. * operating rate * probable rate)					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833 * (1 - THEX)					
(Humidifying vol.) = F/A vol. * abs.humid.diff. * 1.2 * safety factor * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
	8142	8142	0		
	[ 7002] (kcal/h)	[ 7002]	[ 0]		
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
	8142	8142	0	0	
	[ 7002] (kcal/h)	[ 7002]	[ 0]	[ 0]	
!Indoor heat load & total heat load are not contained latent heat.					
Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air					
	1109	1109	0		
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					



## Table of peak heat load detail(Cooling)

[Room name:112 Student.služba 1]		Floor: 2F	Floor area: 31.3m2	Ceiling height: 3.8m	Peak time in cooling:18:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:31.9CDB	, 39.9%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW	80	(31.90-26.00)	2.20	6.2	
Shade	512				See <1>Load detail of window glass with canopy
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW	263	17.20	0.60	( 6.7*3.8- 0.0)	
NW	106	13.40	0.60	( 5.1*3.8- 6.2)	
Shade					
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist					
Flat roof	103	(31.90-26.00)*0.40	1.40	31.3	
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer					
Without air layer	103	(31.90-26.00)*0.40	1.40	31.3	
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
46 23.79 (31.90-26.00)					
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
26 23.79 (11.80-10.49)					
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp	726	1.160	626	1.00	
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
336 56 6 1.00					
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
456 76 6 1.00					
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
2757 2275 482					
[ 2371] (kcal/h) [ 1957] [ 415]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
2757 2757 0 0					
[ 2371] (kcal/h) [ 2371] [ 0] [ 0]					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					

Table of peak heat load detail of window with canopy(Cooling)

<l'> Load detail of window glass with canopy

Upper:solar heat load

=

(S.SHG - S.SHG for shadow) \* SG + S.SHG for shadow

\* shading factor \* area

Lower:SG

=

( x \* y ) / ( Ww \* Hw )

<tanF, tanG>

(!Area of heat transf. is contained sash area.

S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.

Azimuth

NW

273

332

23

1.4

2.2

23

<

0.34

0.24,

-0.51>

(6.20 \* 0.95)

NW

240

332

23

1.4

0.7

23

<

0.34

0.24,

-0.51>

(6.20 \* 0.95)

0.7

0.99

2.19

1.4

2.2

<

0.24,

-0.51>

## Table of peak heat load detail(Heating)

[Room name:112 Student.sluzba 1] Floor: 2F Floor area: 31.3m<sup>2</sup> Ceiling height: 3.8m Peak time in heating: 8:00  
 Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 81.8%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE  
 SE  
 SW  
 NW 390 1.10 1.00 (20.00+ 6.00) 0.00 2.20 6.2  
 Shade  
 Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE  
 SE  
 SW 417 1.05 1.00 (20.00+ 6.00) 0.00 0.60 ( 6.7\*3.8- 0.0)  
 NW 226 1.10 1.00 (20.00+ 6.00) 0.00 0.60 ( 5.1\*3.8- 6.2)  
 Shade  
 (!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Overhead room exit 456 --- --- (20.00+ 6.00)\*0.40 --- 1.40 31.3  
 Flat roof  
 Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
 Earth floor  
 With air layer 456 (20.00+ 6.00)\*0.40 1.40 31.3  
 Without air layer  
 Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE  
 SE  
 SW  
 NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
 (depth<=2.4m)  
 Load of underground wall = temp.diff. \* OHTC \* area  
 (depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m<sup>3</sup>/h) \* temp.diff. \* 0.33  
 337 39.25 (20.00+ 6.00)  
 Load of infiltration(LH) = infiltration vol.(m<sup>3</sup>/h) \* abs.humid.diff.(g/kg) \* 0.833  
 177 39.25 ( 7.26- 1.86)  
 (Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
 280 39.25 ( 7.26- 1.86) 1.10  
 !Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
 39.25 0.30 1.10 118.94

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
 Fluorescent lamp  
 Incandescent lamp

<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)

<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)

<11> Fresh air load(SH) = F/A vol.(m<sup>3</sup>/h) \* temp.diff. \* 0.33 \* (1 - THEX)

Fresh air load(LH) = F/A vol.(m<sup>3</sup>/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)

(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
 2282 2282 0  
 [ 1963] (kcal/h) [ 1963] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
 2282 2282 0 0  
 [ 1963] (kcal/h) [ 1963] [ 0] [ 0]

!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
 280 280 0

OHTC : Overall heat transfer coefficient  
 SH : Sensible heat  
 LH : Latent heat  
 F/A : Fresh air  
 THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

[Room name:113 Student.sluzba 2]		Floor: 2F	Floor area: 32.1m2	Ceiling height: 3.8m	Peak time in cooling:18:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:31.9CDB	, 39.9%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW	80	(31.90-26.00)	2.20	6.2	
Shade	546				See <1>Load detail of window glass with canopy
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW	106	13.40	0.60	( 5.1*3.8- 6.2)	
Shade					
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist	106	(31.90-26.00)*0.40	1.40	32.1	
Flat roof					
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer					
Without air layer	106	(31.90-26.00)*0.40	1.40	32.1	
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
	47	24.40		(31.90-26.00)	
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
	27	24.40		(11.80-10.49)	
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp	745	1.160		642	1.00
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
	336	56		6	1.00
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
	456	76		6	1.00
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
	2555	2072		483	
	[ 2197]	(kcal/h)	[ 1782]	[ 415]	
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
	2555	2555		0	0
	[ 2197]	(kcal/h)	[ 2197]	[ 0]	[ 0]
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					

Table of peak heat load detail of window with canopy(Cooling)

<l'> Load detail of window glass with canopy

Upper:solar heat load	=	(S.SHG - S.SHG for shadow) * SG + S.SHG for shadow) * shading factor * area									
Lower:SG	=	( x * y ) / ( Ww * Hw ) <tanF, tanG> (!Area of heat transf. is contained sash area.									
S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.											
Azimuth											
NW	273	332	23		0.8	23		0.34	(6.20 * 0.95)		
	0.8	1.15	2.19	1.4	2.2		<	0.24,	-0.51>		
NW	273	332	23		0.8	23		0.34	(6.20 * 0.95)		
	0.8	1.15	2.19	1.4	2.2		<	0.24,	-0.51>		

## Table of peak heat load detail(Heating)

[Room name:113 Student.sluzba 2]		Floor: 2F	Floor area: 32.1m2	Ceiling height: 3.8m	Peak time in heating: 8:00		
Indoor temperature:20.0CDB		, 50.0%RH	Outdoor temperature:-6.0CDB	, 81.8%RH			
<1> Load of window glass = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area							
Azimuth							
N							
E							
S							
W							
NE							
SE							
SW							
NW							
Shade							
Skylight							
390	1.10	1.00	(20.00+ 6.00)	0.00	2.20 6.2		
<2> Load of outer wall = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area							
Azimuth							
N							
E							
S							
W							
NE							
SE							
SW							
NW							
226	1.10	1.00	(20.00+ 6.00)	0.00	0.60 ( 5.1*3.8- 6.2)		
Shade							
(!Area of outer wall=length of outer wall*floor height[ceiling height+height of ceiling adv.attic.]-window area)							
<3> Load of roof = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area							
Overhead room exit							
467	---	---	(20.00+ 6.00)*0.40	---	1.40 32.1		
Flat roof							
Inclined roof							
<4> Load of floor = temp.diff. * OHTC * area							
Earth floor							
With air layer							
467	(20.00+ 6.00)*0.40	1.40	32.1	<8> Load of lighting = -(heat gain/W * lighting consumption vol. * ope.rate * probable rate)			
Without air layer							
Pilotis							
<5> Load of inner wall = temp.diff. * OHTC * area							
Azimuth							
N							
E							
S							
W							
NE							
SE							
SW							
NW							
<6> Load of underground wall = temp.diff. * OHTC * ambient length							
(depth<=2.4m)							
Load of underground wall = temp.diff. * OHTC * area							
(depth>2.4m)							
<<Total>> Indoor heat load(W) = SH + LH							
1895 1895 0							
[ 1630] (kcal/h) [ 1630] [ 0]							
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)							
1895 1895 0							
[ 1630] (kcal/h) [ 1630] [ 0] [ 0]							
!Indoor heat load & total heat load are not contained latent heat.							
Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air							
287 287 0							
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33							
345	40.25	(20.00+ 6.00)	<9> Load of human body(SH) = -(SH of human body * No of psns * ope.rate * probable rate)				
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833							
181	40.25	( 7.26- 1.86)	<10> Load of equipments = -(heat gain from internal equip. * operating rate * probable rate)				
(Humidifying vol.)(g/h) = infiltration vol. * abs.humid.diff. * 1.2 * safety factor							
287	40.25	( 7.26- 1.86)	<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)				
!Infiltration vol. = No of ventilation * azimuth factor * room capacity							
40.25	0.30	1.10	121.98	Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833 * (1 - THEX)			
<<Total>> Indoor heat load(W) = SH + LH							
1895 1895 0							
[ 1630] (kcal/h) [ 1630] [ 0]							
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)							
1895 1895 0							
[ 1630] (kcal/h) [ 1630] [ 0] [ 0]							
!Indoor heat load & total heat load are not contained latent heat.							
Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air							
287 287 0							
OHTC : Overall heat transfer coefficient							
SH : Sensible heat							
LH : Latent heat							
F/A : Fresh air							
THEX : Total heat exchange efficiency							

## Table of peak heat load detail(Cooling)

[Room name:114 Vjezbaonica 1 ]		Floor: 2F	Floor area: 100.7m2	Ceiling height: 3.8m	Peak time in cooling:15:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:35.3CDB	, 35.6%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE					
	252	(35.30-26.00)	2.20	12.3	
322 See <1>Load detail of window glass with canopy					
SW					
	252	(35.30-26.00)	2.20	12.3	
667 See <1>Load detail of window glass with canopy					
NW					
Shade					
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
	222	14.40	0.60	(10.0*3.8-12.3)	
SE					
	188	12.00	0.60	(10.1*3.8-12.3)	
SW					
NW					
Shade					
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist					
	524	(35.30-26.00)*0.40	1.40	100.7	
Flat roof					
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer					
	524	(35.30-26.00)*0.40	1.40	100.7	
Without air layer					
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
	235	76.53		(35.30-26.00)	
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
	144	76.53		(12.75-10.49)	
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp					
	2336	1.160		2014	1.00
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
	1680	56		30	1.00
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
	2280	76		30	1.00
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
	9626		7202	2424	
	[ 8278]	(kcal/h)	[ 6194]	[ 2085]	
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
	9626		9626	0	0
	[ 8278]	(kcal/h)	[ 8278]	[ 0]	[ 0]
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					

Table of peak heat load detail of window with canopy(Cooling)

<l'> Load detail of window glass with canopy

Upper:solar heat load

=

(S.SHG - S.SHG for shadow)

\*

SG + S.SHG for shadow

\*

shading factor

\*

area

Lower:SG

=

( x \* y ) / ( Ww \* Hw )

<tanF, tanG>

(!Area of heat transf. is contained sash area.

S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.

Azimuth	152	384	64		0.3	64		0.34	(12.30 * 0.95)
SW	0.3	0.89	0.97	1.4	2.2		<	1.18,	0.64>
SW	343	384	64		0.3	64		0.34	(12.30 * 0.95)
	0.3	1.08	0.97	1.4	2.2		<	1.18,	0.64>
SW	172	384	64		0.3	64		0.34	(12.30 * 0.95)
	0.3	1.08	0.97	1.4	2.2		<	1.18,	0.64>
SE	81	81	64		1.0	64		0.34	(12.30 * 0.95)
	1.0	1.40	2.20	1.4	2.2		<	0.34	0,
SE	161	81	64		1.0	64		0.34	(12.30 * 0.95)
	1.0	1.40	2.20	1.4	2.2		<	0.34	0,
SE	81	81	64		1.0	64		0.34	(12.30 * 0.95)
	1.0	1.40	2.20	1.4	2.2		<	0,	0>



## Table of peak heat load detail(Heating)

[Room name:114 Vjezbaonica 1 ] Floor: 2F Floor area: 100.7m2 Ceiling height: 3.8m Peak time in heating: 8:00  
Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 81.8%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE 739 1.05 1.00 (20.00+ 6.00) 0.00 2.20 12.3  
SW 739 1.05 1.00 (20.00+ 6.00) 0.00 2.20 12.3  
NW  
Shade  
Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE 421 1.05 1.00 (20.00+ 6.00) 0.00 0.60 (10.0\*3.8-12.3)  
SW 427 1.05 1.00 (20.00+ 6.00) 0.00 0.60 (10.1\*3.8-12.3)  
NW  
Shade  
(!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Overhead room exit 1466 --- --- (20.00+ 6.00)\*0.40 --- 1.40 100.7  
Flat roof  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer  
Without air layer 1466 (20.00+ 6.00)\*0.40 1.40 100.7  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
1034 120.54 (20.00+ 6.00)  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
542 120.54 ( 7.26- 1.86)  
(Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
859 120.54 ( 7.26- 1.86) 1.10  
!Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
120.54 0.30 1.05 382.66

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
Fluorescent lamp  
Incandescent lamp

<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)

<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)

<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)

Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)

(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
6292 6292 0  
[ 5411] (kcal/h) [ 5411] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
6292 6292 0 0  
[ 5411] (kcal/h) [ 5411] [ 0] [ 0]  
!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
859 859 0

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

[Room name:115 Vjezbaonica 2 ]		Floor: 2F	Floor area: 101.4m2	Ceiling height: 3.8m	Peak time in cooling:14:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:35.4CDB	, 35.6%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE					
	254	(35.40-26.00)	2.20	12.3	
SW					
	374				See <1'>Load detail of window glass with canopy
NW					
Shade					
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
	235	14.20	0.60	(10.5*3.8-12.3)	
SE					
SW					
NW					
Shade					
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist					
	534	(35.40-26.00)*0.40	1.40	101.4	
Flat roof					
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer					
	534	(35.40-26.00)*0.40	1.40	101.4	
Without air layer					
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
	239			77.06	(35.40-26.00)
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
	150			77.06	(12.82-10.49)
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp					
	2352	1.160		2028	1.00
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
	1680	56		30	1.00
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
	2280	76		30	1.00
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
	8632			6202	2430
	[ 7424]	(kcal/h)	[ 5334]	[ 2090]	
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
	8632			8632	0
	[ 7424]	(kcal/h)	[ 7424]	[ 0]	[ 0]
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					

Table of peak heat load detail of window with canopy(Cooling)

<l'> Load detail of window glass with canopy

Upper:solar heat load = ((S.SHG - S.SHG for shadow) \* SG + S.SHG for shadow) \* shading factor \* area

Lower:SG = ( x \* y ) / ( Ww \* Hw ) <tanF, tanG> (!Area of heat transf. is contained sash area.

S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.

Azimuth

SE

94

94

72

1.0

72

0.34

(12.30 \* 0.95)

1.0

1.40

2.20

1.4

2.2

<

0.34

0,

0>

SE

187

94

72

1.0

72

<

0.34

0,

0>

1.0

1.40

2.20

1.4

2.2

<

0.34

0,

0>

SE

94

94

72

1.0

72

<

0.34

0,

0>

1.0

1.40

2.20

1.4

2.2

<

0.34

0,

0>

## Table of peak heat load detail(Heating)

[Room name:115 Vjezbaonica 2 ] , Floor: 2F Floor area: 101.4m<sup>2</sup> Ceiling height: 3.8m Peak time in heating: 8:00  
Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 81.8%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE 739 1.05 1.00 (20.00+ 6.00) 0.00 2.20 12.3  
SW  
NW  
Shade  
Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE 452 1.05 1.00 (20.00+ 6.00) 0.00 0.60 (10.5\*3.8-12.3)  
SW  
NW  
Shade  
(!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Overhead room exit 1476 --- --- (20.00+ 6.00)\*0.40 --- 1.40 101.4  
Flat roof  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer 1476 (20.00+ 6.00)\*0.40 1.40 101.4  
Without air layer  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
1041 121.38 (20.00+ 6.00)  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
546 121.38 ( 7.26- 1.86)  
(Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
865 121.38 ( 7.26- 1.86) 1.10  
!Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
121.38 0.30 1.05 385.32

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
Fluorescent lamp  
Incandescent lamp  
<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)  
<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)  
<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)  
Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)  
(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
5184 5184 0  
[ 4458] (kcal/h) [ 4458] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
5184 5184 0 0  
[ 4458] (kcal/h) [ 4458] [ 0] [ 0]  
!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
865 865 0

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

[Room name:116 Vjezbaonica 3 ]		Floor: 2F	Floor area: 101.4m2	Ceiling height: 3.8m	Peak time in cooling:14:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:35.4CDB	, 35.6%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE	254	(35.40-26.00)	2.20	12.3	
SW	374				See <1'>Load detail of window glass with canopy
NW					
Shade					
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE	235	14.20	0.60	(10.5*3.8-12.3)	
SE					
SW					
NW					
Shade					
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist	534	(35.40-26.00)*0.40	1.40	101.4	
Flat roof					
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer					
Without air layer	534	(35.40-26.00)*0.40	1.40	101.4	
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
239 77.06 (35.40-26.00)					
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
150 77.06 (12.82-10.49)					
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp 2352 1.160 2028 1.00					
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
1680 56 30 1.00					
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
2280 76 30 1.00					
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
8632 6202 2430					
[ 7424] (kcal/h) [ 5334] [ 2090]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
8632 8632 0 0					
[ 7424] (kcal/h) [ 7424] [ 0] [ 0]					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					

Table of peak heat load detail of window with canopy(Cooling)

<l'> Load detail of window glass with canopy

Upper:solar heat load

=

(S.SHG - S.SHG for shadow)

\*

SG + S.SHG for shadow

\*

shading factor

\*

area

Lower:SG

=

( x \* y ) / ( Ww \* Hw )

<tanF, tanG>

(!Area of heat transf. is contained sash area.

S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.

Azimuth

SE

1.0

1.40

2.20

1.4

2.2

72

<

0.34

0,

0>

(12.30 \* 0.95)

SE

187

94

72

1.4

1.0

72

<

0.34

0,

0>

(12.30 \* 0.95)

SE

1.0

1.40

2.20

1.4

2.2

72

<

0.34

0,

0>

(12.30 \* 0.95)

SE

94

94

72

1.4

1.0

72

<

0.34

0,

0>

(12.30 \* 0.95)

SE

1.0

1.40

2.20

1.4

2.2

72

<

0.34

0,

0>

(12.30 \* 0.95)

## Table of peak heat load detail(Heating)

[Room name:116 Vjezbaonica 3 ] , Floor: 2F Floor area: 101.4m<sup>2</sup> Ceiling height: 3.8m Peak time in heating: 8:00  
Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 81.8%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE 739 1.05 1.00 (20.00+ 6.00) 0.00 2.20 12.3  
SW  
NW  
Shade  
Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE 452 1.05 1.00 (20.00+ 6.00) 0.00 0.60 (10.5\*3.8-12.3)  
SW  
NW  
Shade  
(!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Overhead room exit 1476 --- --- (20.00+ 6.00)\*0.40 --- 1.40 101.4  
Flat roof  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer 1476 (20.00+ 6.00)\*0.40 1.40 101.4  
Without air layer  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
1041 121.38 (20.00+ 6.00)  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
546 121.38 ( 7.26- 1.86)  
(Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
865 121.38 ( 7.26- 1.86) 1.10  
!Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
121.38 0.30 1.05 385.32

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
Fluorescent lamp  
Incandescent lamp

<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)

<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)

<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)

Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)

(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
5184 5184 0  
[ 4458] (kcal/h) [ 4458] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
5184 5184 0 0  
[ 4458] (kcal/h) [ 4458] [ 0] [ 0]

!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
865 865 0

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

[Room name:117 Vjezbaonica 4 ]		Floor: 2F	Floor area: 101.4m2	Ceiling height: 3.8m	Peak time in cooling:14:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:35.4CDB	, 35.6%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE	254	(35.40-26.00)	2.20	12.3	
SE	254	(35.40-26.00)	2.20	12.3	See <1>Load detail of window glass with canopy
SW	374				See <1>Load detail of window glass with canopy
NW					
Shade					
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE	156	10.00	0.60	(10.1*3.8-12.3)	
SE	235	14.20	0.60	(10.5*3.8-12.3)	
SW					
NW					
Shade					
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist					
Flat roof					
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer					
Without air layer					
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
239 77.06 (35.40-26.00)					
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
150 77.06 (12.82-10.49)					
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp 2352 1.160 2028 1.00					
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
1680 56 30 1.00					
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
2280 76 30 1.00					
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
9416 6986 2430					
[ 8098] (kcal/h) [ 6008] [ 2090]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
9416 9416 0 0					
[ 8098] (kcal/h) [ 8098] [ 0] [ 0]					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					



Table of peak heat load detail of window with canopy(Cooling)

<l'> Load detail of window glass with canopy

Upper:solar heat load

=

(S.SHG - S.SHG for shadow)

\*

SG + S.SHG for shadow

\*

shading factor

\*

area

Lower:SG

=

( x \* y )

/

( Ww \* Hw )

<tanF, tanG>

(!Area of heat transf. is contained sash area.

S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.

Azimuth	94	94	72	1.0	72	0.34	(12.30 * 0.95)
SE	1.0	1.40	2.20	1.4	2.2	< 0, 0>	
SE	187	94	72	1.0	72	0.34	(12.30 * 0.95)
	1.0	1.40	2.20	1.4	2.2	< 0, 0>	
SE	94	94	72	1.0	72	0.34	(12.30 * 0.95)
	1.0	1.40	2.20	1.4	2.2	< 0, 0>	
NE	94	94	72	1.0	72	0.34	(12.30 * 0.95)
	1.0	1.40	2.20	1.4	2.2	< 0, 0>	
NE	187	94	72	1.0	72	0.34	(12.30 * 0.95)
	1.0	1.40	2.20	1.4	2.2	< 0, 0>	
NE	94	94	72	1.0	72	0.34	(12.30 * 0.95)
	1.0	1.40	2.20	1.4	2.2	< 0, 0>	

## Table of peak heat load detail(Heating)

[Room name:117 Vjezbaonica 4 ] Floor: 2F Floor area: 101.4m<sup>2</sup> Ceiling height: 3.8m Peak time in heating: 8:00  
 Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 81.8%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE 739 1.05 1.00 (20.00+ 6.00) 0.00 2.20 12.3  
 SE 739 1.05 1.00 (20.00+ 6.00) 0.00 2.20 12.3  
 SW  
 NW  
 Shade  
 Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE 427 1.05 1.00 (20.00+ 6.00) 0.00 0.60 (10.1\*3.8-12.3)  
 SE 452 1.05 1.00 (20.00+ 6.00) 0.00 0.60 (10.5\*3.8-12.3)  
 SW  
 NW  
 Shade  
 (!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Overhead room exit 1476 --- --- (20.00+ 6.00)\*0.40 --- 1.40 101.4  
 Flat roof  
 Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
 Earth floor  
 With air layer 1476 (20.00+ 6.00)\*0.40 1.40 101.4  
 Without air layer  
 Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE  
 SE  
 SW  
 NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
 (depth<=2.4m)  
 Load of underground wall = temp.diff. \* OHTC \* area  
 (depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m<sup>3</sup>/h) \* temp.diff. \* 0.33  
 1041 121.38 (20.00+ 6.00)  
 Load of infiltration(LH) = infiltration vol.(m<sup>3</sup>/h) \* abs.humid.diff.(g/kg) \* 0.833  
 546 121.38 ( 7.26- 1.86)  
 (Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
 865 121.38 ( 7.26- 1.86) 1.10  
 !Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
 121.38 0.30 1.05 385.32

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
 Fluorescent lamp  
 Incandescent lamp  
 <9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)  
 <10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)  
 <11> Fresh air load(SH) = F/A vol.(m<sup>3</sup>/h) \* temp.diff. \* 0.33 \* (1 - THEX)  
 Fresh air load(LH) = F/A vol.(m<sup>3</sup>/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)  
 (Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
 6350 6350 0  
 [ 5461] (kcal/h) [ 5461] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
 6350 6350 0 0  
 [ 5461] (kcal/h) [ 5461] [ 0] [ 0]  
 !Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
 865 865 0

OHTC : Overall heat transfer coefficient  
 SH : Sensible heat  
 LH : Latent heat  
 F/A : Fresh air  
 THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

Room name:201 Centralni hol ] Floor: 3F Floor area: 270.3m2 Ceiling height: 3.8m Peak time in cooling:15:00  
Indoor temperature:26.0CDB , 50.0%RH Outdoor temperature:35.3CDB , 35.6%RH

<1> Load of window glass  
-Material I / with blind-  
Upper:heat transfer load = temp.diff. \* OHTC \* area (!Area of heat transf. is contained sash area.)  
Lower:solar heat load = area \* std.solar heat gain \* shading factor (!Area of solar heat gain is not contained sash area.)  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW 327 (35.30-26.00) 2.20 16.0  
1292 (16.0\*0.95) 250 0.34  
Shade 1111 (35.30-26.00) 2.20 54.3  
1122 (54.3\*0.95) 64 0.34  
Skylight

<2> Load of outer wall = effective temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW 170 8.70 0.60 (12.8\*3.8-16.0)  
Shade 55 5.00 0.60 (19.1\*3.8-54.3)  
(!Area of outer wall=length of outer wall  
\*floor height[ceiling height+height of ceiling adv attic]-window area)  
<3> Load of roof = effective temp.diff. \* OHTC \* area  
Overhead room exist 1408 (35.30-26.00)\*0.40 1.40 270.3  
Flat roof  
Inclined roof  
<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer  
Without air layer 1408 (35.30-26.00)\*0.40 1.40 270.3  
Pilotis  
<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW  
<6> Load of underground wall = temp.diff. \* OHTC/unit ambient length \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
630 205.43 (35.30-26.00)  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
387 205.43 (12.75-10.49)  
<8> Load of lighting = heat gain/W \* lighting consumption vol. \* ope.rate  
Fluorescent lamp 3135 1.160 2703 1.00  
Incandescent lamp  
<9> Load of human body(SH) = SH of human body \* No of psns. \* ope.rate  
1680 56 30 1.00  
Load of human body(LH) = LH of human body \* No of psns. \* ope.rate  
2280 76 30 1.00  
<10> Load of equipments = heat gain from internal equip. \* operating rate  
<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)  
Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff. \* 0.833 \* (1 - THEX)  
<<Total>> Indoor heat load(W) = SH + LH  
15005 12338 2667  
[ 12904] (kcal/h) [ 10611] [ 2294]  
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
15005 15005 0 0  
[ 12904] (kcal/h) [ 12904] [ 0] [ 0]  
OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

## Table of peak heat load detail(Heating)

[Room name:201 Centralni hol ] , Floor: 3F Floor area: 270.3m<sup>2</sup> Ceiling height: 3.8m Peak time in heating: 8:00  
Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 81.8%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW 1007 1.10 1.00 (20.00+ 6.00) 0.00 2.20 16.0  
Shade 3417 1.10 1.00 (20.00+ 6.00) 0.00 2.20 54.3  
Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW 560 1.10 1.00 (20.00+ 6.00) 0.00 0.60 (12.8\*3.8-16.0)  
NW 314 1.10 1.00 (20.00+ 6.00) 0.00 0.60 (19.1\*3.8-54.3)  
Shade  
(!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Overhead room exit 3936 --- --- (20.00+ 6.00)\*0.40 --- 1.40 270.3  
Flat roof  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer 3936 (20.00+ 6.00)\*0.40 1.40 270.3  
Without air layer  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m<sup>3</sup>/h) \* temp.diff. \* 0.33  
2908 338.96 (20.00+ 6.00)  
Load of infiltration(LH) = infiltration vol.(m<sup>3</sup>/h) \* abs.humid.diff.(g/kg) \* 0.833  
1525 338.96 ( 7.26- 1.86)  
(Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
2416 338.96 ( 7.26- 1.86) 1.10  
!Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
338.96 0.30 1.10 1027.14

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
Fluorescent lamp  
Incandescent lamp

<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)

<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)

<11> Fresh air load(SH) = F/A vol.(m<sup>3</sup>/h) \* temp.diff. \* 0.33 \* (1 - THEX)

Fresh air load(LH) = F/A vol.(m<sup>3</sup>/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)

(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
16078 16078 0  
[ 13827] (kcal/h) [ 13827] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
16078 16078 0 0  
[ 13827] (kcal/h) [ 13827] [ 0] [ 0]  
!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
2416 2416 0

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

[Room name:202 Diplomka sala ]		Floor: 3F	Floor area: 66.3m2	Ceiling height: 3.8m	Peak time in cooling:18:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:31.9CDB	, 39.9%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW	160	(31.90-26.00)	2.20	12.3	
Shade	1064			See <1>	Load detail of window glass with canopy
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
Shade					
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist					
Flat roof					
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer					
Without air layer					
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
98 50.39 (31.90-26.00)					
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
55 50.39 (11.80-10.49)					
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp 1538 1.160 1326 1.00					
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
1008 56 18 1.00					
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
1368 76 18 1.00					
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
6208 4785 1423					
[ 5339] (kcal/h) [ 4115] [ 1224]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
6208 6208 0 0					
[ 5339] (kcal/h) [ 5339] [ 0] [ 0]					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					

Table of peak heat load detail of window with canopy(Cooling)

<l'> Load detail of window glass with canopy

Upper:solar heat load	=	((S.SHG - S.SHG for shadow) * SG + S.SHG for shadow) * shading factor * area									
Lower:SG	=	( x * y ) / ( Ww * Hw ) <tanF, tanG> (!Area of heat transf. is contained sash area.									
S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.											
Azimuth	241	332	23		0.7	23		0.34	(12.30 * 0.95)		
NW	0.7	0.99	2.20	1.4	2.2		<	0.24,	-0.51>		
NW	549	332	23		0.8	23		0.34	(12.30 * 0.95)		
	0.8	1.15	2.20	1.4	2.2		<	0.24,	-0.51>		
NW	274	332	23		0.8	23		0.34	(12.30 * 0.95)		
	0.8	1.15	2.20	1.4	2.2		<	0.24,	-0.51>		

## Table of peak heat load detail(Heating)

[Room name:202 Diplomka sala ] , Floor: 3F Floor area: 66.3m<sup>2</sup> Ceiling height: 3.8m Peak time in heating: 8:00  
 Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 81.8%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE  
 SE  
 SW  
 NW 774 1.10 1.00 (20.00+ 6.00) 0.00 2.20 12.3  
 Shade  
 Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE  
 SE  
 SW 417 1.05 1.00 (20.00+ 6.00) 0.00 0.60 ( 6.7\*3.8- 0.0)  
 NW 461 1.10 1.00 (20.00+ 6.00) 0.00 0.60 (10.3\*3.8-12.3)  
 Shade  
 (!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Overhead room exit 965 --- --- (20.00+ 6.00)\*0.40 --- 1.40 66.3  
 Flat roof  
 Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
 Earth floor  
 With air layer 965 (20.00+ 6.00)\*0.40 1.40 66.3  
 Without air layer  
 Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE  
 SE  
 SW  
 NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
 (depth<=2.4m)  
 Load of underground wall = temp.diff. \* OHTC \* area  
 (depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
 713 83.14 (20.00+ 6.00)  
 Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
 374 83.14 ( 7.26- 1.86)  
 (Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
 593 83.14 ( 7.26- 1.86) 1.10  
 !Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
 83.14 0.30 1.10 251.94

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
 Fluorescent lamp  
 Incandescent lamp

<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)

<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)

<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)

Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)

(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
 4295 4295 0  
 [ 3694] (kcal/h) [ 3694] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
 4295 4295 0 0  
 [ 3694] (kcal/h) [ 3694] [ 0] [ 0]  
 !Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
 593 593 0

OHTC : Overall heat transfer coefficient  
 SH : Sensible heat  
 LH : Latent heat  
 F/A : Fresh air  
 THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

[Room name:206 Vjezbaonica 5 ]		Floor: 3F	Floor area: 100.7m2	Ceiling height: 3.8m	Peak time in cooling:15:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:35.3CDB	, 35.6%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE					
	252	(35.30-26.00)	2.20	12.3	
	322			See <1>Load detail of window glass with canopy	
SW					
	252	(35.30-26.00)	2.20	12.3	
	717			See <1>Load detail of window glass with canopy	
NW					
Shade					
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
	222	14.40	0.60	(10.0*3.8-12.3)	
SE					
	188	12.00	0.60	(10.1*3.8-12.3)	
SW					
NW					
Shade					
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist					
	524	(35.30-26.00)*0.40	1.40	100.7	
Flat roof					
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer					
	524	(35.30-26.00)*0.40	1.40	100.7	
Without air layer					
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
	235	76.53		(35.30-26.00)	
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
	144	76.53		(12.75-10.49)	
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp					
	2336	1.160		2014	1.00
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
	1680	56		30	1.00
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
	2280	76		30	1.00
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
	9676		7252	2424	
	[ 8321]	(kcal/h)	[ 6237]	[ 2085]	
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
	9676		9676	0	0
	[ 8321]	(kcal/h)	[ 8321]	[ 0]	[ 0]
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					



Table of peak heat load detail of window with canopy(Cooling)

<l'> Load detail of window glass with canopy

Upper:solar heat load = ((S.SHG - S.SHG for shadow) \* SG + S.SHG for shadow) \* shading factor \* area  
Lower:SG = ( x \* y ) / ( Ww \* Hw ) <tanF, tanG> (!Area of heat transf. is contained sash area.  
S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.

Azimuth	163	384	64		0.3	64		0.34	(12.30 * 0.95)
SW	0.3	0.89	1.08	1.4	2.2		<	1.18,	0.64>
SW	369	384	64		0.4	64		0.34	(12.30 * 0.95)
	0.4	1.08	1.08	1.4	2.2		<	1.18,	0.64>
SW	185	384	64		0.4	64		0.34	(12.30 * 0.95)
	0.4	1.08	1.08	1.4	2.2		<	1.18,	0.64>
SE	81	81	64		1.0	64		0.34	(12.30 * 0.95)
	1.0	1.40	2.20	1.4	2.2		<	0.34	0,
SE	161	81	64		1.0	64		0.34	(12.30 * 0.95)
	1.0	1.40	2.20	1.4	2.2		<	0.34	0,
SE	81	81	64		1.0	64		0.34	(12.30 * 0.95)
	1.0	1.40	2.20	1.4	2.2		<	0,	0>

## Table of peak heat load detail(Heating)

[Room name:206 Vjezbaonica 5 ] , Floor: 3F Floor area: 100.7m2 Ceiling height: 3.8m Peak time in heating: 8:00  
Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 81.8%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE 739 1.05 1.00 (20.00+ 6.00) 0.00 2.20 12.3  
SW 739 1.05 1.00 (20.00+ 6.00) 0.00 2.20 12.3  
NW  
Shade  
Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE 421 1.05 1.00 (20.00+ 6.00) 0.00 0.60 (10.0\*3.8-12.3)  
SW 427 1.05 1.00 (20.00+ 6.00) 0.00 0.60 (10.1\*3.8-12.3)  
NW  
Shade  
(!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Overhead room exit 1466 --- --- (20.00+ 6.00)\*0.40 --- 1.40 100.7  
Flat roof  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer 1466 (20.00+ 6.00)\*0.40 1.40 100.7  
Without air layer  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
1034 120.54 (20.00+ 6.00)  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
542 120.54 ( 7.26- 1.86)  
(Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
859 120.54 ( 7.26- 1.86) 1.10  
!Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
120.54 0.30 1.05 382.66

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
Fluorescent lamp  
Incandescent lamp  
<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)  
<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)  
<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)  
Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)  
(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
6292 6292 0  
[ 5411] (kcal/h) [ 5411] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
6292 6292 0 0  
[ 5411] (kcal/h) [ 5411] [ 0] [ 0]  
!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
859 859 0

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

[Room name:207 Vjezbaonica 6 ]		Floor: 3F	Floor area: 101.4m2	Ceiling height: 3.8m	Peak time in cooling:14:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:35.4CDB	, 35.6%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE	254	(35.40-26.00)	2.20	12.3	
SW	374				See <1'>Load detail of window glass with canopy
NW					
Shade					
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE	235	14.20	0.60	(10.5*3.8-12.3)	
SE					
SW					
NW					
Shade					
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist	534	(35.40-26.00)*0.40	1.40	101.4	
Flat roof					
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer					
Without air layer	534	(35.40-26.00)*0.40	1.40	101.4	
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
239 77.06 (35.40-26.00)					
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
150 77.06 (12.82-10.49)					
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp 2352 1.160 2028 1.00					
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
1680 56 30 1.00					
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
2280 76 30 1.00					
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
8632 6202 2430					
[ 7424] (kcal/h) [ 5334] [ 2090]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
8632 8632 0 0					
[ 7424] (kcal/h) [ 7424] [ 0] [ 0]					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					

Table of peak heat load detail of window with canopy(Cooling)

<l'> Load detail of window glass with canopy

Upper:solar heat load

=

(S.SHG - S.SHG for shadow)

\*

SG + S.SHG for shadow

\*

shading factor

\*

area

Lower:SG

=

( x \* y ) / ( Ww \* Hw )

<tanF, tanG>

(!Area of heat transf. is contained sash area.

S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.

Azimuth

SE

1.0

1.40

2.20

1.4

2.2

72

<

0.34

0,

0>

(12.30 \* 0.95)

SE

187

94

72

1.4

1.0

72

<

0.34

0,

0>

(12.30 \* 0.95)

SE

1.0

1.40

2.20

1.4

2.2

72

<

0.34

0,

0>

(12.30 \* 0.95)

SE

94

94

72

1.4

1.0

72

<

0.34

0,

0>

(12.30 \* 0.95)

SE

1.0

1.40

2.20

1.4

2.2

72

<

0.34

0,

0>

(12.30 \* 0.95)

## Table of peak heat load detail(Heating)

[Room name:207 Vjezbaonica 6 ] , Floor: 3F Floor area: 101.4m<sup>2</sup> Ceiling height: 3.8m Peak time in heating: 8:00  
Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 81.8%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE 739 1.05 1.00 (20.00+ 6.00) 0.00 2.20 12.3  
SW  
NW  
Shade  
Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE 452 1.05 1.00 (20.00+ 6.00) 0.00 0.60 (10.5\*3.8-12.3)  
SW  
NW  
Shade  
(!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Overhead room exit 1476 --- --- (20.00+ 6.00)\*0.40 --- 1.40 101.4  
Flat roof  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer 1476 (20.00+ 6.00)\*0.40 1.40 101.4  
Without air layer  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
1041 121.38 (20.00+ 6.00)  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
546 121.38 ( 7.26- 1.86)  
(Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
865 121.38 ( 7.26- 1.86) 1.10  
!Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
121.38 0.30 1.05 385.32

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
Fluorescent lamp  
Incandescent lamp  
<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)  
<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)  
<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)  
Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)  
(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
5184 5184 0  
[ 4458] (kcal/h) [ 4458] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
5184 5184 0 0  
[ 4458] (kcal/h) [ 4458] [ 0] [ 0]  
!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
865 865 0

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

[Room name:208 Vjezbaonica 7 ]		Floor: 3F	Floor area: 97.0m2	Ceiling height: 3.8m	Peak time in cooling:14:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:35.4CDB	, 35.6%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE	254	(35.40-26.00)	2.20	12.3	
SW	374				See <1'>Load detail of window glass with canopy
NW					
Shade					
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE	206	14.20	0.60	( 9.6*3.8-12.3)	
SW					
NW					
Shade					
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist					
Flat roof	511	(35.40-26.00)*0.40	1.40	97.0	
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer					
Without air layer	511	(35.40-26.00)*0.40	1.40	97.0	
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
229 73.72 (35.40-26.00)					
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
143 73.72 (12.82-10.49)					
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp 2250 1.160 1940 1.00					
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
1680 56 30 1.00					
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
2280 76 30 1.00					
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
8438 6015 2423					
[ 7257] (kcal/h) [ 5173] [ 2084]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
8438 8438 0 0					
[ 7257] (kcal/h) [ 7257] [ 0] [ 0]					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					

Table of peak heat load detail of window with canopy(Cooling)

<l'> Load detail of window glass with canopy

Upper:solar heat load	=	((S.SHG - S.SHG for shadow) * SG + S.SHG for shadow) * shading factor * area									
Lower:SG	=	( x * y ) / ( Ww * Hw ) <tanF, tanG> (!Area of heat transf. is contained sash area.									
S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.											
Azimuth	94	94	72	1.0	72	0.34	(12.30 * 0.95)				
SE	1.0	1.40	2.20	1.4	2.2	<	0.34	0,	0>		
SE	187	94	72	1.0	72	<	0.34	0,	0>	(12.30 * 0.95)	
	1.0	1.40	2.20	1.4	2.2	<	0.34	0,	0>		
SE	94	94	72	1.0	72	<	0.34	0,	0>	(12.30 * 0.95)	
	1.0	1.40	2.20	1.4	2.2	<	0.34	0,	0>		

## Table of peak heat load detail(Heating)

[Room name:208 Vjezbaonica 7 ] Floor: 3F Floor area: 97.0m2 Ceiling height: 3.8m Peak time in heating: 8:00  
Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 81.8%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE 739 1.05 1.00 (20.00+ 6.00) 0.00 2.20 12.3  
SW  
NW  
Shade  
Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE 396 1.05 1.00 (20.00+ 6.00) 0.00 0.60 ( 9.6\*3.8-12.3)  
SW  
NW  
Shade  
(!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Overhead room exit 1412 --- --- (20.00+ 6.00)\*0.40 --- 1.40 97.0  
Flat roof  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer 1412 (20.00+ 6.00)\*0.40 1.40 97.0  
Without air layer  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
996 116.11 (20.00+ 6.00)  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
522 116.11 ( 7.26- 1.86)  
(Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
828 116.11 ( 7.26- 1.86) 1.10  
!Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
116.11 0.30 1.05 368.60

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
Fluorescent lamp  
Incandescent lamp  
<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)  
<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)  
<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)  
Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)  
(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
4955 4955 0  
[ 4261] (kcal/h) [ 4261] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
4955 4955 0 0  
[ 4261] (kcal/h) [ 4261] [ 0] [ 0]  
!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
828 828 0

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency



Table of peak heat load detail(Cooling)

[Room name:209 Vjezbaonica 8 ]		Floor: 3F	Floor area: 101.1m2	Ceiling height: 3.8m	Peak time in cooling:14:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:35.4CDB	, 35.6%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE	254	(35.40-26.00)	2.20	12.3	
SW	374				See <1'>Load detail of window glass with canopy
NW					
Shade					
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE	222	14.20	0.60	(10.1*3.8-12.3)	
SW					
NW					
Shade					
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist					
Flat roof	532	(35.40-26.00)*0.40	1.40	101.1	
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer					
Without air layer	532	(35.40-26.00)*0.40	1.40	101.1	
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
238 76.84 (35.40-26.00)					
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
149 76.84 (12.82-10.49)					
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp 2346 1.160 2022 1.00					
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
1680 56 30 1.00					
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
2280 76 30 1.00					
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
8607 6178 2429					
[ 7402] (kcal/h) [ 5313] [ 2089]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
8607 8607 0 0					
[ 7402] (kcal/h) [ 7402] [ 0] [ 0]					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					

Table of peak heat load detail of window with canopy(Cooling)

<l'> Load detail of window glass with canopy

Upper:solar heat load

=

(S.SHG - S.SHG for shadow)

\*

SG + S.SHG for shadow

\*

shading factor

\*

area

Lower:SG

=

( x \* y ) / ( Ww \* Hw )

<tanF, tanG>

(!Area of heat transf. is contained sash area.

S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.

Azimuth

SE

1.0

1.40

2.20

1.4

2.2

72

<

0.34

0,

0>

(12.30 \* 0.95)

SE

187

94

72

1.4

1.0

72

<

0.34

0,

0>

(12.30 \* 0.95)

SE

1.0

1.40

2.20

1.4

2.2

72

<

0.34

0,

0>

(12.30 \* 0.95)

SE

94

94

72

1.4

1.0

72

<

0.34

0,

0>

(12.30 \* 0.95)

SE

1.0

1.40

2.20

1.4

2.2

72

<

0.34

0,

0>

(12.30 \* 0.95)

## Table of peak heat load detail(Heating)

[Room name:209 Vjezbaonica 8 ] , Floor: 3F Floor area: 101.1m<sup>2</sup> Ceiling height: 3.8m Peak time in heating: 8:00  
Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 81.8%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE 739 1.05 1.00 (20.00+ 6.00) 0.00 2.20 12.3  
SW  
NW  
Shade  
Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE 427 1.05 1.00 (20.00+ 6.00) 0.00 0.60 (10.1\*3.8-12.3)  
SW  
NW  
Shade  
(!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Overhead room exit 1472 --- --- (20.00+ 6.00)\*0.40 --- 1.40 101.1  
Flat roof  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer 1472 (20.00+ 6.00)\*0.40 1.40 101.1  
Without air layer  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
1038 121.02 (20.00+ 6.00)  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
544 121.02 ( 7.26- 1.86)  
(Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
863 121.02 ( 7.26- 1.86) 1.10  
!Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
121.02 0.30 1.05 384.18

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
Fluorescent lamp  
Incandescent lamp  
<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)  
<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)  
<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)  
Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)  
(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
5148 5148 0  
[ 4427] (kcal/h) [ 4427] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
5148 5148 0 0  
[ 4427] (kcal/h) [ 4427] [ 0] [ 0]  
!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
863 863 0

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

[Room name:210 Vjezbaonica 9 ]		Floor: 3F	Floor area: 101.4m2	Ceiling height: 3.8m	Peak time in cooling:14:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:35.4CDB	, 35.6%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE	254	(35.40-26.00)	2.20	12.3	
SE	374			See <1>Load detail of window glass with canopy	
	254	(35.40-26.00)	2.20	12.3	
	374			See <1>Load detail of window glass with canopy	
SW					
NW					
Shade					
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE	156	10.00	0.60	(10.1*3.8-12.3)	
SE	222	14.20	0.60	(10.1*3.8-12.3)	
SW					
NW					
Shade					
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist					
Flat roof					
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer					
Without air layer					
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE	9403			9403	0
SE	[ 8087]			[ 8087]	[ 0]
SW					[ 0]
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
239 77.06 (35.40-26.00)					
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
150 77.06 (12.82-10.49)					
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp 2352 1.160 2028 1.00					
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
1680 56 30 1.00					
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
2280 76 30 1.00					
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
9403 6973 2430					
[ 8087] (kcal/h) [ 5997] [ 2090]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
9403 9403 0 0					
[ 8087] (kcal/h) [ 8087] [ 0] [ 0]					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					

Table of peak heat load detail of window with canopy(Cooling)

<l'> Load detail of window glass with canopy

Upper:solar heat load = ((S.SHG - S.SHG for shadow) \* SG + S.SHG for shadow) \* shading factor \* area  
Lower:SG = ( x \* y ) / ( Ww \* Hw ) <tanF, tanG> (!Area of heat transf. is contained sash area.  
S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.

Azimuth	94	94	72	1.0	72	0.34	(12.30 * 0.95)
NE	1.0	1.40	2.20	1.4	2.2	< 0, 0>	
NE	187	94	72	1.0	72	0.34	(12.30 * 0.95)
	1.0	1.40	2.20	1.4	2.2	< 0, 0>	
NE	94	94	72	1.0	72	0.34	(12.30 * 0.95)
	1.0	1.40	2.20	1.4	2.2	< 0, 0>	
SE	94	94	72	1.0	72	0.34	(12.30 * 0.95)
	1.0	1.40	2.20	1.4	2.2	< 0, 0>	
SE	187	94	72	1.0	72	0.34	(12.30 * 0.95)
	1.0	1.40	2.20	1.4	2.2	< 0, 0>	
SE	94	94	72	1.0	72	0.34	(12.30 * 0.95)
	1.0	1.40	2.20	1.4	2.2	< 0, 0>	

## Table of peak heat load detail(Heating)

[Room name:210 Vjezbaonica 9 ] Floor: 3F Floor area: 101.4m2 Ceiling height: 3.8m Peak time in heating: 8:00  
Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 81.8%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE 739 1.05 1.00 (20.00+ 6.00) 0.00 2.20 12.3  
SE 739 1.05 1.00 (20.00+ 6.00) 0.00 2.20 12.3  
SW  
NW  
Shade  
Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE 427 1.05 1.00 (20.00+ 6.00) 0.00 0.60 (10.1\*3.8-12.3)  
SE 427 1.05 1.00 (20.00+ 6.00) 0.00 0.60 (10.1\*3.8-12.3)  
SW  
NW  
Shade  
(!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Overhead room exit 1476 --- --- (20.00+ 6.00)\*0.40 --- 1.40 101.4  
Flat roof  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer 1476 (20.00+ 6.00)\*0.40 1.40 101.4  
Without air layer  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
1041 121.38 (20.00+ 6.00)  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
546 121.38 ( 7.26- 1.86)  
(Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
865 121.38 ( 7.26- 1.86) 1.10  
!Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
121.38 0.30 1.05 385.32

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
Fluorescent lamp  
Incandescent lamp  
<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)  
<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)  
<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)  
Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)  
(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
6325 6325 0  
[ 5440] (kcal/h) [ 5440] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
6325 6325 0 0  
[ 5440] (kcal/h) [ 5440] [ 0] [ 0]  
!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
865 865 0

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

[Room name:211 Toaleti ]		Floor: 3F	Floor area: 12.6m2	Ceiling height: 3.8m	Peak time in cooling:17:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:33.3CDB	, 38.2%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW	103	(33.30-26.00)	2.20	6.4	
Shade	726			( 6.4*0.95)	351 0.34
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW	33	11.90	0.60	( 2.9*3.8- 6.4)	
Shade					
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist	52	(33.30-26.00)*0.40	1.40	12.6	
Flat roof					
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer					
Without air layer	52	(33.30-26.00)*0.40	1.40	12.6	
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
23 9.58 (33.30-26.00)					
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
14 9.58 (12.23-10.49)					
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp 292 1.160 252 1.00					
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
168 56 3 1.00					
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
228 76 3 1.00					
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
1691 1449 242					
[ 1454] (kcal/h) [ 1246] [ 208]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
1691 1691 0 0					
[ 1454] (kcal/h) [ 1454] [ 0] [ 0]					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					

## Table of peak heat load detail(Heating)

[Room name:211 Toaleti ] , Floor: 3F Floor area: 12.6m<sup>2</sup> Ceiling height: 3.8m Peak time in heating: 8:00  
 Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 81.8%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE  
 SE  
 SW  
 NW 403 1.10 1.00 (20.00+ 6.00) 0.00 2.20 6.4  
 Shade  
 Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE  
 SE  
 SW 79 1.10 1.00 (20.00+ 6.00) 0.00 0.60 ( 2.9\*3.8- 6.4)  
 NW  
 Shade  
 (!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Overhead room exit 183 --- --- (20.00+ 6.00)\*0.40 --- 1.40 12.6  
 Flat roof  
 Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
 Earth floor  
 With air layer 183 (20.00+ 6.00)\*0.40 1.40 12.6  
 Without air layer  
 Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE  
 SE  
 SW  
 NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
 (depth<=2.4m)  
 Load of underground wall = temp.diff. \* OHTC \* area  
 (depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m<sup>3</sup>/h) \* temp.diff. \* 0.33  
 136 15.80 (20.00+ 6.00)  
 Load of infiltration(LH) = infiltration vol.(m<sup>3</sup>/h) \* abs.humid.diff.(g/kg) \* 0.833  
 71 15.80 ( 7.26- 1.86)  
 (Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
 113 15.80 ( 7.26- 1.86) 1.10  
 !Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
 15.80 0.30 1.10 47.88

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
 Fluorescent lamp  
 Incandescent lamp  
 <9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)  
 <10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)  
 <11> Fresh air load(SH) = F/A vol.(m<sup>3</sup>/h) \* temp.diff. \* 0.33 \* (1 - THEX)  
 Fresh air load(LH) = F/A vol.(m<sup>3</sup>/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)  
 (Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
 984 984 0  
 [ 846] (kcal/h) [ 846] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
 984 984 0 0  
 [ 846] (kcal/h) [ 846] [ 0] [ 0]  
 !Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
 113 113 0

OHTC : Overall heat transfer coefficient  
 SH : Sensible heat  
 LH : Latent heat  
 F/A : Fresh air  
 THEX : Total heat exchange efficiency



## Table of peak heat load detail(Cooling)

Room name:214 Racunovodstvo ]		Floor: 3F	Floor area: 17.0m2	Ceiling height: 3.8m	Peak time in cooling:18:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:31.9CDB	, 39.9%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load		= temp.diff.	* OHTC * area	(!Area of heat transf. is contained sash area.	
Lower:solar heat load		=	area * std.solar heat gain * shading factor	(!Area of solar heat gain is not contained sash area.	
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW	40	(31.90-26.00)	2.20	3.1	
Shade	274				See <1>>Load detail of window glass with canopy
Skylight					
<2> Load of outer wall					
		= effective temp.diff. * OHTC * area			
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW	85	13.40	0.60	( 3.6*3.8- 3.1)	
Shade		(!Area of outer wall=length of outer wall			
		*floor height[ceiling height+height of ceiling adv attic]-window area)			
<3> Load of roof					
		= effective temp.diff. * OHTC * area			
Overhead room exist	56	(31.90-26.00)*0.40	1.40	17.0	
Flat roof					
Inclined roof					
<4> Load of floor					
		= temp.diff. * OHTC * area			
Earth floor					
With air layer					
Without air layer	56	(31.90-26.00)*0.40	1.40	17.0	
Pilotis					
<5> Load of inner wall					
		= temp.diff. * OHTC * area			
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall					
(depth<=2.4m)		= temp.diff. * OHTC/unit ambient length * ambient length			
Load of underground wall		= temp.diff. * OHTC * area			
(depth>2.4m)					
<7> Load of infiltration(SH)					
		= infiltration vol.(m3/h) * temp.diff. * 0.33			
		(31.90-26.00)			
Load of infiltration(LH)					
		= infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833			
		(11.80-10.49)			
<8> Load of lighting					
		= heat gain/W * lighting consumption vol. * ope.rate			
Fluorescent lamp	394	1.160	340	1.00	
Incandescent lamp					
<9> Load of human body(SH)					
		= SH of human body * No of psns. * ope.rate			
		224 56 4 1.00			
Load of human body(LH)					
		= LH of human body * No of psns. * ope.rate			
		304 76 4 1.00			
<10> Load of equipments					
		= heat gain from internal equip. * operating rate			
<11> Fresh air load(SH)					
		= F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)			
Fresh air load(LH)					
		= F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)			
<<Total>> Indoor heat load(W)					
		= SH + LH			
		1472 1154 318			
		[ 1266] (kcal/h) [ 992] [ 273]			
Total heat load(W)					
		= indoor heat load + fresh air load(SH) + fresh air load(LH)			
		1472 1472 0 0			
		[ 1266] (kcal/h) [ 1266] [ 0] [ 0]			
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					



## Table of peak heat load detail(Heating)

[Room name:214 Racunovodstvo ]		Floor: 3F	Floor area: 17.0m2	Ceiling height: 3.8m	Peak time in heating: 8:00		
Indoor temperature:20.0CDB		, 50.0%RH	Outdoor temperature:-6.0CDB	, 81.8%RH			
<1> Load of window glass = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area							
Azimuth							
N							
E							
S							
W							
NE							
SE							
SW							
NW							
Shade							
Skylight							
195	1.10	1.00	(20.00+ 6.00)	0.00	2.20 3.1		
<2> Load of outer wall = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area							
Azimuth							
N							
E							
S							
W							
NE							
SE							
SW							
NW							
Shade							
(!Area of outer wall=length of outer wall*floor height[ceiling height+height of ceiling adv.attic.]-window area)							
<3> Load of roof = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area							
Overhead room exit							
248	---	---	(20.00+ 6.00)*0.40	---	1.40 17.0		
Flat roof							
Inclined roof							
<4> Load of floor = temp.diff. * OHTC * area							
Earth floor							
With air layer							
248	(20.00+ 6.00)*0.40	1.40	17.0	<8> Load of lighting = -(heat gain/W * lighting consumption vol. * ope.rate * probable rate)			
Without air layer							
Pilotis							
<5> Load of inner wall = temp.diff. * OHTC * area							
Azimuth							
N							
E							
S							
W							
NE							
SE							
SW							
NW							
<6> Load of underground wall = temp.diff. * OHTC * ambient length							
(depth<=2.4m)							
Load of underground wall = temp.diff. * OHTC * area							
(depth>2.4m)							
<<Total>> Indoor heat load(W) = SH + LH							
1056 1056 0							
[ 908 ] (kcal/h) [ 908 ] [ 0 ]							
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)							
1056 1056 0 0							
[ 908 ] (kcal/h) [ 908 ] [ 0 ] [ 0 ]							
!Indoor heat load & total heat load are not contained latent heat.							
Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air							
152 152 0							
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33							
183 21.32 (20.00+ 6.00)							
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833							
96 21.32 ( 7.26- 1.86)							
(Humidifying vol.)(g/h) = infiltration vol. * abs.humid.diff. * 1.2 * safety factor							
152 21.32 ( 7.26- 1.86) 1.10							
!Infiltration vol. = No of ventilation * azimuth factor * room capacity							
21.32 0.30 1.10 64.60							
OHTC : Overall heat transfer coefficient							
SH : Sensible heat							
LH : Latent heat							
F/A : Fresh air							
THEX : Total heat exchange efficiency							

## Table of peak heat load detail(Cooling)

[Room name:215 Prodekan 1 ]		Floor: 3F	Floor area: 22.5m2	Ceiling height: 3.8m	Peak time in cooling:18:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:31.9CDB	, 39.9%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW	80	(31.90-26.00)	2.20	6.2	
Shade	515				See <1>>Load detail of window glass with canopy
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW	97	13.40	0.60	( 4.8*3.8- 6.2)	
Shade					
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist	74	(31.90-26.00)*0.40	1.40	22.5	
Flat roof					
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer					
Without air layer	74	(31.90-26.00)*0.40	1.40	22.5	
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
33 17.10 (31.90-26.00)					
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
19 17.10 (11.80-10.49)					
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp 392 1.160 338 1.00					
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
280 56 5 1.00					
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
380 76 5 1.00					
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
1944 1545 399					
[ 1672] (kcal/h) [ 1329] [ 343]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
1944 1944 0 0					
[ 1672] (kcal/h) [ 1672] [ 0] [ 0]					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					

Table of peak heat load detail of window with canopy(Cooling)

<l'> Load detail of window glass with canopy

Upper:solar heat load

=

(S.SHG - S.SHG for shadow) \* SG + S.SHG for shadow

\* shading factor \* area

Lower:SG

=

( x \* y ) / ( Ww \* Hw )

<tanF, tanG>

(!Area of heat transf. is contained sash area.

S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.

Azimuth

NW

274

332

23

0.8

23

0.34

(6.20 \* 0.95)

0.8

1.15

2.20

1.4

2.2

<

0.24,

-0.51>

NW

241

332

23

0.7

23

0.34

(6.20 \* 0.95)

0.7

0.99

2.20

1.4

2.2

<

0.24,

-0.51>

## Table of peak heat load detail(Heating)

[Room name:215 Prodekan 1 ] Floor: 3F Floor area: 22.5m<sup>2</sup> Ceiling height: 3.8m Peak time in heating: 8:00  
Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 81.8%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW  
Shade  
Skylight  
390 1.10 1.00 (20.00+ 6.00) 0.00 2.20 6.2

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW  
Shade  
207 1.10 1.00 (20.00+ 6.00) 0.00 0.60 ( 4.8\*3.8- 6.2)  
(!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Overhead room exit 328 --- --- (20.00+ 6.00)\*0.40 --- 1.40 22.5  
Flat roof  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer 328 (20.00+ 6.00)\*0.40 1.40 22.5  
Without air layer  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
242 28.22 (20.00+ 6.00)  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
127 28.22 ( 7.26- 1.86)  
(Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
201 28.22 ( 7.26- 1.86) 1.10  
!Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
28.22 0.30 1.10 85.50

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
Fluorescent lamp  
Incandescent lamp  
<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)  
<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)  
<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)  
Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)  
(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
1495 1495 0  
[ 1286] (kcal/h) [ 1286] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
1495 1495 0 0  
[ 1286] (kcal/h) [ 1286] [ 0] [ 0]

!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
201 201 0

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

[Room name:216 Prodekan 2 ]		Floor: 3F	Floor area: 22.6m2	Ceiling height: 3.8m	Peak time in cooling:17:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:33.3CDB	, 38.2%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
Shade					
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
Shade					
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist					
Flat roof					
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer					
Without air layer					
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
41 17.18 (33.30-26.00)					
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
25 17.18 (12.23-10.49)					
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp 393 1.160 339 1.00					
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
280 56 5 1.00					
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
380 76 5 1.00					
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
2220 1815 405					
[ 1909] (kcal/h) [ 1561] [ 348]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
2220 2220 0 0					
[ 1909] (kcal/h) [ 1909] [ 0] [ 0]					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					

Table of peak heat load detail of window with canopy(Cooling)

<l'> Load detail of window glass with canopy

Upper:solar heat load

=

(S.SHG - S.SHG for shadow) \* SG + S.SHG for shadow

\* shading factor \* area

Lower:SG

=

( x \* y ) / ( Ww \* Hw )

<tanF, tanG>

(!Area of heat transf. is contained sash area.

S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.

Azimuth	233	351	39	0.6	39	0.34	(6.20 * 0.95)
NW	0.6	1.03	1.86	1.4	2.2	< 0.53,	-0.73>
NW	233	351	39	0.6	39	0.34	(6.20 * 0.95)
	0.6	1.03	1.86	1.4	2.2	< 0.53,	-0.73>
NE	47	47	39	1.0	39	0.34	(6.20 * 0.95)
	1.0	1.40	2.20	1.4	2.2	< 0.34	0,
NE	47	47	39	1.0	39	0.34	(6.20 * 0.95)
	1.0	1.40	2.20	1.4	2.2	< 0.34	0,



## Table of peak heat load detail(Heating)

[Room name:216 Prodekan 2 ] Floor: 3F Floor area: 22.6m<sup>2</sup> Ceiling height: 3.8m Peak time in heating: 8:00  
Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 81.8%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE 372 1.05 1.00 (20.00+ 6.00) 0.00 2.20 6.2  
SE  
SW  
NW 390 1.10 1.00 (20.00+ 6.00) 0.00 2.20 6.2  
Shade  
Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE 197 1.05 1.00 (20.00+ 6.00) 0.00 0.60 ( 4.8\*3.8- 6.2)  
SE  
SW  
NW 207 1.10 1.00 (20.00+ 6.00) 0.00 0.60 ( 4.8\*3.8- 6.2)  
Shade  
(!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Overhead room exit 329 --- --- (20.00+ 6.00)\*0.40 --- 1.40 22.6  
Flat roof  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer 329 (20.00+ 6.00)\*0.40 1.40 22.6  
Without air layer  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
243 28.34 (20.00+ 6.00)  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
127 28.34 ( 7.26- 1.86)  
(Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
202 28.34 ( 7.26- 1.86) 1.10  
!Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
28.34 0.30 1.10 85.88

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
Fluorescent lamp  
Incandescent lamp

<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)

<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)

<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)

Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)

(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
2067 2067 0  
[ 1778] (kcal/h) [ 1778] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
2067 2067 0 0  
[ 1778] (kcal/h) [ 1778] [ 0] [ 0]  
!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
202 202 0

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

[Room name:217 Pravna služba ]		Floor: 3F	Floor area: 22.5m2	Ceiling height: 3.8m	Peak time in cooling:14:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:35.4CDB	, 35.6%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
Shade					
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
Shade					
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist					
Flat roof					
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer					
Without air layer					
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
53 17.10 (35.40-26.00)					
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
33 17.10 (12.82-10.49)					
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp 522 1.160 450 1.00					
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
280 56 5 1.00					
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
380 76 5 1.00					
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
1891 1478 413					
[ 1626] (kcal/h) [ 1271] [ 355]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
1891 1891 0 0					
[ 1626] (kcal/h) [ 1626] [ 0] [ 0]					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					

Table of peak heat load detail of window with canopy(Cooling)

Arhitektonski fakultet 19/June/2018

```
<> Load detail of window glass with canopy
```

Upper:solar heat load	=	(S.SHG - S.SHG for shadow) * SG + S.SHG for shadow) * shading factor * area					
Lower:SG	=	( x * y ) / ( Ww * Hw ) <tanF, tanG> (!Area of heat transf. is contained sash area.					
		S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.					
Azimuth	94	94	72	1.0	72	0.34	(6.20 * 0.95)
NE	1.0	1.40	2.20	1.4	2.2	< 0, 0>	
NE	94	94	72	1.0	72	0.34	(6.20 * 0.95)
	1.0	1.40	2.20	1.4	2.2	< 0, 0>	

## Table of peak heat load detail(Heating)

[Room name:217 Pravna služba ] , Floor: 3F Floor area: 22.5m<sup>2</sup> Ceiling height: 3.8m Peak time in heating: 8:00  
Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 81.8%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE 372 1.05 1.00 (20.00+ 6.00) 0.00 2.20 6.2  
SE  
SW  
NW  
Shade  
Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE 197 1.05 1.00 (20.00+ 6.00) 0.00 0.60 ( 4.8\*3.8- 6.2)  
SE  
SW  
NW  
Shade  
(!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Overhead room exit 328 --- --- (20.00+ 6.00)\*0.40 --- 1.40 22.5  
Flat roof  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer 328 (20.00+ 6.00)\*0.40 1.40 22.5  
Without air layer  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m<sup>3</sup>/h) \* temp.diff. \* 0.33  
231 26.93 (20.00+ 6.00)  
Load of infiltration(LH) = infiltration vol.(m<sup>3</sup>/h) \* abs.humid.diff.(g/kg) \* 0.833  
121 26.93 ( 7.26- 1.86)  
(Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
192 26.93 ( 7.26- 1.86) 1.10  
!Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
26.93 0.30 1.05 85.50

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
Fluorescent lamp  
Incandescent lamp  
<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)  
<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)  
<11> Fresh air load(SH) = F/A vol.(m<sup>3</sup>/h) \* temp.diff. \* 0.33 \* (1 - THEX)  
Fresh air load(LH) = F/A vol.(m<sup>3</sup>/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)  
(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
1456 1456 0  
[ 1252] (kcal/h) [ 1252] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
1456 1456 0 0  
[ 1252] (kcal/h) [ 1252] [ 0] [ 0]  
!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
192 192 0

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

[Room name:301 Hol ]		Floor: 4F	Floor area: 221.3m2	Ceiling height: 3.8m	Peak time in cooling:14:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:35.4CDB	, 35.6%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW	436	(35.40-26.00)	2.20	21.1	
	491			See <1>	Load detail of window glass with canopy
Shade	1855	(35.40-26.00)	2.20	89.7	
	2086			(89.7*0.95)	72 0.34
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW	63	6.80	0.60	( 9.6*3.8-21.1)	
Shade	68	3.60	0.60	(31.9*3.8-89.7)	
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist					
Flat roof	2009	22.70	0.40	221.3	
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer	1165	(35.40-26.00)*0.40	1.40	221.3	
Without air layer					
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
522 168.19 (35.40-26.00)					
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
326 168.19 (12.82-10.49)					
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp 2567 1.160 2213 1.00					
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
1680 56 30 1.00					
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
2280 76 30 1.00					
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
15548 12942 2606					
[ 13371] (kcal/h) [ 11130] [ 2241]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
15548 15548 0 0					
[ 13371] (kcal/h) [ 13371] [ 0] [ 0]					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					



## Table of peak heat load detail(Heating)

[Room name:301 Hol ] , Floor: 4F Floor area: 221.3m2 Ceiling height: 3.8m Peak time in heating:18:00  
Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 72.7%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW 1430 1.10 1.00 (20.00+ 6.00) 2.00 2.20 21.1  
Shade 6078 1.10 1.00 (20.00+ 6.00) 2.00 2.20 89.7  
Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW 284 1.10 1.00 (20.00+ 6.00) 2.00 0.60 ( 9.6\*3.8-21.1)  
Shade 582 1.10 1.00 (20.00+ 6.00) 2.00 0.60 (31.9\*3.8-89.7)  
(!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Overhead room exit  
Flat roof 2833 1.00 1.00 (20.00+ 6.00) 6.00 0.40 221.3  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer 3222 (20.00+ 6.00)\*0.40 1.40 221.3  
Without air layer  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
2381 277.51 (20.00+ 6.00)  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
1297 277.51 ( 7.26- 1.65)  
(Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
2055 277.51 ( 7.26- 1.65) 1.10  
!Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
277.51 0.30 1.10 840.94

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
Fluorescent lamp  
Incandescent lamp

<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)

<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)

<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)

Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)

(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
16810 16810 0  
[ 14457] (kcal/h) [ 14457] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
16810 16810 0 0  
[ 14457] (kcal/h) [ 14457] [ 0] [ 0]  
!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
2055 2055 0

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

[Room name:302 Diplomka sala ]		Floor: 4F	Floor area: 69.9m2	Ceiling height: 3.8m	Peak time in cooling:18:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:31.9CDB	, 39.9%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW	119	(31.90-26.00)	2.20	9.2	
	348			See <1>	Load detail of window glass with canopy
NW	287	(31.90-26.00)	2.20	22.1	
	2050			See <1>	Load detail of window glass with canopy
Shade					
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW	172	17.20	0.60	( 6.8*3.8- 9.2)	
NW	140	13.40	0.60	(10.4*3.8-22.1)	
Shade					
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist					
Flat roof	679	24.30	0.40	69.9	
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer	231	(31.90-26.00)*0.40	1.40	69.9	
Without air layer					
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
103 53.12 (31.90-26.00)					
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
58 53.12 (11.80-10.49)					
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp	1216	1.160	1049	1.00	
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
2856 56 51 1.00					
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
3876 76 51 1.00					
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
12135 8201 3934					
[ 10436] (kcal/h) [ 7053] [ 3383]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
12135 12135 0 0					
[ 10436] (kcal/h) [ 10436] [ 0] [ 0]					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					



Table of peak heat load detail of window with canopy(Cooling)

<l'> Load detail of window glass with canopy

Upper:solar heat load

=

(S.SHG - S.SHG for shadow)

\*

SG + S.SHG for shadow

\*

shading factor

\*

area

Lower:SG

=

( x \* y ) / ( Ww \* Hw )

<tanF, tanG>

(!Area of heat transf. is contained sash area.

S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.

Azimuth

NW

2050

332

23

0.9

2.3

23

<

0.34

(22.10 \* 0.95)

SW

348

164

23

0.7

2.3

23

<

0.34

(9.20 \* 0.95)

0.7

4.00

1.54

4.0

2.3

<

0.48,

1.98>

-79-

117

## Table of peak heat load detail(Heating)

[Room name:302 Diplomka sala ] , Floor: 4F Floor area: 69.9m2 Ceiling height: 3.8m Peak time in heating:18:00  
 Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 72.7%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE  
 SE  
 SW 595 1.05 1.00 (20.00+ 6.00) 2.00 2.20 9.2  
 NW 1497 1.10 1.00 (20.00+ 6.00) 2.00 2.20 22.1  
 Shade  
 Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE  
 SE  
 SW 294 1.05 1.00 (20.00+ 6.00) 2.00 0.60 ( 6.8\*3.8- 9.2)  
 NW 322 1.10 1.00 (20.00+ 6.00) 2.00 0.60 (10.4\*3.8-22.1)  
 Shade  
 (!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Overhead room exit  
 Flat roof 895 1.00 1.00 (20.00+ 6.00) 6.00 0.40 69.9  
 Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
 Earth floor  
 With air layer 1018 (20.00+ 6.00)\*0.40 1.40 69.9  
 Without air layer  
 Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE  
 SE  
 SW  
 NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
 (depth<=2.4m)  
 Load of underground wall = temp.diff. \* OHTC \* area  
 (depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
 752 87.65 (20.00+ 6.00)  
 Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
 410 87.65 ( 7.26- 1.65)  
 (Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
 649 87.65 ( 7.26- 1.65) 1.10  
 !Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
 87.65 0.30 1.10 265.62

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
 Fluorescent lamp  
 Incandescent lamp

<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)

<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)

<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)

Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)

(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
 5373 5373 0  
 [ 4621] (kcal/h) [ 4621] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
 5373 5373 0 0  
 [ 4621] (kcal/h) [ 4621] [ 0] [ 0]  
 !Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
 649 649 0

OHTC : Overall heat transfer coefficient  
 SH : Sensible heat  
 LH : Latent heat  
 F/A : Fresh air  
 THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

Room name:306 Sala nast. osob.] Floor: 4F Floor area: 49.0m2 Ceiling height: 3.8m Peak time in cooling:15:00  
Indoor temperature:26.0CDB , 50.0%RH Outdoor temperature:35.3CDB , 35.6%RH

<1> Load of window glass  
-Material I / with blind-  
Upper:heat transfer load = temp.diff. \* OHTC \* area (!Area of heat transf. is contained sash area.  
Lower:solar heat load = area \* std.solar heat gain \* shading factor (!Area of solar heat gain is not contained sash area.  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW  
Shade  
Skylight

<2> Load of outer wall = effective temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW  
Shade  
(!Area of outer wall=length of outer wall  
\*floor height[ceiling height+height of ceiling adv attic]-window area)

<3> Load of roof = effective temp.diff. \* OHTC \* area  
Overhead room exist  
Flat roof 504 25.70 0.40 49.0  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer  
Without air layer 255 (35.30-26.00)\*0.40 1.40 49.0  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC/unit ambient length \* ambient length  
(depth<=2.4m)  
  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
114 37.24 (35.30-26.00)  
  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
70 37.24 (12.75-10.49)  
  
<8> Load of lighting = heat gain/W \* lighting consumption vol. \* ope.rate  
Fluorescent lamp 1137 1.160 980 1.00  
Incandescent lamp  
  
<9> Load of human body(SH) = SH of human body \* No of psns. \* ope.rate  
1792 56 32 1.00  
  
Load of human body(LH) = LH of human body \* No of psns. \* ope.rate  
2432 76 32 1.00  
  
<10> Load of equipments = heat gain from internal equip. \* operating rate  
  
<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)  
798 1300.0 (35.30-26.00) 0.800  
  
Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff. \* 0.833 \* (1 - THEX)  
489 1300.0 (12.75-10.49) 0.800  
  
<<Total>> Indoor heat load(W) = SH + LH  
6304 3802 2502  
[ 5421] (kcal/h) [ 3270] [ 2152]  
  
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
7591 6304 798 489  
[ 6528] (kcal/h) [ 5421] [ 686] [ 421]

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

## Table of peak heat load detail(Heating)

[Room name:306 Sala nast. osob.] Floor: 4F Floor area: 49.0m<sup>2</sup> Ceiling height: 3.8m Peak time in heating:18:00  
Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 72.7%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW  
Shade  
Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW  
Shade  
(!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Overhead room exit  
Flat roof 627 1.00 1.00 (20.00+ 6.00) 6.00 0.40 49.0  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer 713 (20.00+ 6.00)\*0.40 1.40 49.0  
Without air layer  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m<sup>3</sup>/h) \* temp.diff. \* 0.33  
527 61.45 (20.00+ 6.00)  
Load of infiltration(LH) = infiltration vol.(m<sup>3</sup>/h) \* abs.humid.diff.(g/kg) \* 0.833  
287 61.45 ( 7.26- 1.65)  
(Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
455 61.45 ( 7.26- 1.65) 1.10  
!Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
61.45 0.30 1.10 186.20

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
Fluorescent lamp  
Incandescent lamp

<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)

<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)

<11> Fresh air load(SH) = F/A vol.(m<sup>3</sup>/h) \* temp.diff. \* 0.33 \* (1 - THEX)  
1673 1300.0 (20.00+ 6.00) 0.850

Fresh air load(LH) = F/A vol.(m<sup>3</sup>/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)  
911 1300.0 ( 7.26- 1.65) 0.850

(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)  
1444 1300.0 ( 7.26- 1.65) 1.10 0.850

<<Total>> Indoor heat load(W) = SH + LH  
1867 1867 0  
[ 1606] (kcal/h) [ 1606] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
3540 1867 1673 0  
[ 3044] (kcal/h) [ 1606] [ 1439] [ 0]  
!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
1899 455 1444

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

Room name:307 Kabinet dekana | Floor: 4F Floor area: 46.0m2 Ceiling height: 3.8m Peak time in cooling:14:00  
Indoor temperature:26.0CDB , 50.0%RH Outdoor temperature:35.4CDB , 35.6%RH

<1> Load of window glass  
-Material I / with blind-  
Upper:heat transfer load = temp.diff. \* OHTC \* area (!Area of heat transf. is contained sash area.  
Lower:solar heat load = area \* std.solar heat gain \* shading factor (!Area of solar heat gain is not contained sash area.  
Azimuth  
N  
E  
S  
W  
NE  
SE 281 (35.40-26.00) 2.20 13.6  
SW 414 See <1'>Load detail of window glass with canopy  
NW  
Shade  
Skylight

<2> Load of outer wall = effective temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE 195 14.20 0.60 ( 9.6\*3.8-13.6)  
SW  
NW  
Shade  
(!Area of outer wall=length of outer wall  
\*floor height[ceiling height+height of ceiling adv attic]-window area)

<3> Load of roof = effective temp.diff. \* OHTC \* area  
Overhead room exist  
Flat roof 418 22.70 0.40 46.0  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer  
Without air layer 242 (35.40-26.00)\*0.40 1.40 46.0  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC/unit ambient length \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
108 34.96 (35.40-26.00)  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
68 34.96 (12.82-10.49)  
<8> Load of lighting = heat gain/W \* lighting consumption vol. \* ope.rate  
Fluorescent lamp 1067 1.160 920 1.00  
Incandescent lamp  
<9> Load of human body(SH) = SH of human body \* No of psns. \* ope.rate  
672 56 12 1.00  
Load of human body(LH) = LH of human body \* No of psns. \* ope.rate  
912 76 12 1.00  
<10> Load of equipments = heat gain from internal equip. \* operating rate  
<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)  
Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff. \* 0.833 \* (1 - THEX)  
<<Total>> Indoor heat load(W) = SH + LH  
4377 3397 980  
[ 3764] (kcal/h) [ 2921] [ 843]  
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
4377 4377 0 0  
[ 3764] (kcal/h) [ 3764] [ 0] [ 0]

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

Table of peak heat load detail of window with canopy(Cooling)

Arhitektonski fakultet 19/June/2018

<1'> Load detail of window glass with canopy

Upper:solar heat load	=	(S.SHG - S.SHG for shadow) * SG + S.SHG for shadow) * shading factor * area									
Lower:SG	=	( x * y ) / ( Ww * Hw )	<tanF, tanG>		(!Area of heat transf. is contained sash area.						
S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.											
Azimuth	414	94	72		1.0	72		0.34		(13.60 * 0.95)	
SE	1.0	6.20	2.20		6.2	2.2		<	0,	0>	

## Table of peak heat load detail(Heating)

[Room name:307 Kabinet dekana ] Floor: 4F Floor area: 46.0m2 Ceiling height: 3.8m Peak time in heating:18:00  
Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 72.7%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE 880 1.05 1.00 (20.00+ 6.00) 2.00 2.20 13.6  
SW  
NW  
Shade  
Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE 404 1.05 1.00 (20.00+ 6.00) 2.00 0.60 ( 9.6\*3.8-13.6)  
SW  
NW  
Shade  
(!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Overhead room exit  
Flat roof 589 1.00 1.00 (20.00+ 6.00) 6.00 0.40 46.0  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer 670 (20.00+ 6.00)\*0.40 1.40 46.0  
Without air layer  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
472 55.06 (20.00+ 6.00)  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
257 55.06 ( 7.26- 1.65)  
(Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
408 55.06 ( 7.26- 1.65) 1.10  
!Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
55.06 0.30 1.05 174.80

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
Fluorescent lamp  
Incandescent lamp  
<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)  
<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)  
<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)  
Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)  
(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
3015 3015 0  
[ 2593] (kcal/h) [ 2593] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
3015 3015 0 0  
[ 2593] (kcal/h) [ 2593] [ 0] [ 0]  
!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
408 408 0

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

[Room name:308 Amfiteatar ]		Floor: 4F	Floor area: 215.2m2	Ceiling height: 3.8m	Peak time in cooling:15:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:35.3CDB	, 35.6%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE					
1140					
SW					
432					
810					
NW					
Shade					
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
303					
SE					
135					
NW					
Shade					
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist					
Flat roof					
2212					
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer					
1121					
Without air layer					
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
502					
163.55					
(35.30-26.00)					
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
308					
163.55					
(12.75-10.49)					
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp					
3744					
1.160					
3228					
1.00					
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
8904					
56					
159					
1.00					
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
12084					
76					
159					
1.00					
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
3744					
6100.0					
(35.30-26.00)					
0.800					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
2297					
6100.0					
(12.75-10.49)					
0.800					
<<Total>> Indoor heat load(W) = SH + LH					
32587					
20195					
12392					
[ 28025] (kcal/h) [ 17368] [ 10657]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
38628					
32587					
3744					
2297					
[ 33220] (kcal/h) [ 28025] [ 3220] [ 1975]					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					



Table of peak heat load detail of window with canopy(Cooling)

Arhitektonski fakultet 19/June/2018

```
<'> Load detail of window glass with canopy
```

Upper:solar heat load	=	((S.SHG - S.SHG for shadow) * SG + S.SHG for shadow) * shading factor * area						
Lower:SG	=	( x * y ) / ( Ww * Hw ) <tanF, tanG> (!Area of heat transf. is contained sash area.						
		S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.						
Azimuth								
SW	810	384	64		0.2	64	0.34	(21.10 * 0.95)
	0.2	9.60	0.38	9.6	2.2		< 1.18,	0.64>
SE	1140	81	64		1.0	64	0.34	(43.60 * 0.95)
	1.0	19.80	2.20	19.8	2.2		< 0,	0>

## Table of peak heat load detail(Heating)

[Room name:308 Amfiteatar ] Floor: 4F Floor area: 215.2m<sup>2</sup> Ceiling height: 3.8m Peak time in heating:18:00  
Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 72.7%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE 2820 1.05 1.00 (20.00+ 6.00) 2.00 2.20 43.6  
SW 1365 1.05 1.00 (20.00+ 6.00) 2.00 2.20 21.1  
NW  
Shade  
Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE 618 1.05 1.00 (20.00+ 6.00) 2.00 0.60 (20.7\*3.8-43.6)  
SW 332 1.05 1.00 (20.00+ 6.00) 2.00 0.60 (10.5\*3.8-21.1)  
NW  
Shade  
(!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Overhead room exit  
Flat roof 2755 1.00 1.00 (20.00+ 6.00) 6.00 0.40 215.2  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer 3133 (20.00+ 6.00)\*0.40 1.40 215.2  
Without air layer  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
2210 257.59 (20.00+ 6.00)  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
1204 257.59 ( 7.26- 1.65)  
(Humidifying vol.) (g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
1908 257.59 ( 7.26- 1.65) 1.10  
!Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
257.59 0.30 1.05 817.76

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
Fluorescent lamp  
Incandescent lamp

<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)

<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)

<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)  
7851 6100.0 (20.00+ 6.00) 0.850

Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)  
4276 6100.0 ( 7.26- 1.65) 0.850

(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)  
6776 6100.0 ( 7.26- 1.65) 1.10 0.850

<<Total>> Indoor heat load(W) = SH + LH  
13233 13233 0  
[ 11380] (kcal/h) [ 11380] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
21084 13233 7851 0  
[ 18132] (kcal/h) [ 11380] [ 6752] [ 0]  
!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
8684 1908 6776

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

[Room name:309 Hodnik ]		Floor: 4F	Floor area: 100.7m2	Ceiling height: 3.8m	Peak time in cooling:17:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:33.3CDB	, 38.2%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
Shade					
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
Shade					
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist					
Flat roof					
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer					
Without air layer					
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
184 76.53 (33.30-26.00)					
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
111 76.53 (12.23-10.49)					
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp 1168 1.160 1007 1.00					
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
560 56 10 1.00					
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
760 76 10 1.00					
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
5195 4324 871					
[ 4468] (kcal/h) [ 3719] [ 749]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
5195 5195 0 0					
[ 4468] (kcal/h) [ 4468] [ 0] [ 0]					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					

Table of peak heat load detail of window with canopy(Cooling)

<l'> Load detail of window glass with canopy

Upper:solar heat load	=	((S.SHG - S.SHG for shadow) * SG + S.SHG for shadow) * shading factor * area									
Lower:SG	=	( x * y ) / ( Ww * Hw )									
		S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.									
Azimuth											
NE	94	47	39		1.0	39		0.34		(6.20 * 0.95)	
	1.0	1.40	2.20	1.4	2.2		<	0, 0>			
NW	569	351	39		0.7	39		0.34		(6.80 * 0.95)	
	0.7	3.10	1.55	3.1	2.2		<	0.53, -0.73>			

## Table of peak heat load detail(Heating)

[Room name:309 Hodnik ] , Floor: 4F Floor area: 100.7m2 Ceiling height: 3.8m Peak time in heating:18:00  
Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 72.7%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE 401 1.05 1.00 (20.00+ 6.00) 2.00 2.20 6.2  
SE  
SW  
NW 461 1.10 1.00 (20.00+ 6.00) 2.00 2.20 6.8  
Shade  
Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE 92 1.05 1.00 (20.00+ 6.00) 2.00 0.60 ( 3.0\*3.8- 6.2)  
SE  
SW  
NW 99 1.10 1.00 (20.00+ 6.00) 2.00 0.60 ( 3.2\*3.8- 6.8)  
Shade  
(!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Overhead room exit  
Flat roof 1289 1.00 1.00 (20.00+ 6.00) 6.00 0.40 100.7  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer 1466 (20.00+ 6.00)\*0.40 1.40 100.7  
Without air layer  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
1083 126.28 (20.00+ 6.00)  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
590 126.28 ( 7.26- 1.65)  
(Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
935 126.28 ( 7.26- 1.65) 1.10  
!Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
126.28 0.30 1.10 382.66

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
Fluorescent lamp  
Incandescent lamp

<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)

<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)

<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)

Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)

(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
4891 4891 0  
[ 4206] (kcal/h) [ 4206] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
4891 4891 0 0  
[ 4206] (kcal/h) [ 4206] [ 0] [ 0]  
!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
935 935 0

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

[Room name:311 Toaleti ] Floor: 4F Floor area: 14.6m2 Ceiling height: 3.8m Peak time in cooling:17:00  
 Indoor temperature:26.0CDB , 50.0%RH Outdoor temperature:33.3CDB , 38.2%RH

<1> Load of window glass

-Material I / with blind-

Upper:heat transfer load = temp.diff. \* OHTC \* area (!Area of heat transf. is contained sash area.  
 Lower:solar heat load = area \* std.solar heat gain \* shading factor (!Area of solar heat gain is not contained sash area.

Azimuth  
 N

E

S

W

NE

SE

SW

NW 103 (33.30-26.00) 2.20 6.4  
 726 ( 6.4\*0.95) 351 0.34

Shade

Skylight

<2> Load of outer wall = effective temp.diff. \* OHTC \* area

Azimuth

N

E

S

W

NE

SE

SW

NW 33 11.90 0.60 ( 2.9\*3.8- 6.4)  
 Shade (!Area of outer wall=length of outer wall  
 \*floor height[ceiling height+height of ceiling adv attic]-window area)

<3> Load of roof = effective temp.diff. \* OHTC \* area  
 Overhead room exist 60 (33.30-26.00)\*0.40 1.40 14.6  
 Flat roof  
 Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
 Earth floor  
 With air layer  
 Without air layer 60 (33.30-26.00)\*0.40 1.40 14.6  
 Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area

Azimuth

N

E

S

W

NE

SE

SW

NW

<6> Load of underground wall = temp.diff. \* OHTC/unit ambient length \* ambient length  
 (depth<=2.4m)

Load of underground wall = temp.diff. \* OHTC \* area  
 (depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
 27 11.10 (33.30-26.00)

Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
 16 11.10 (12.23-10.49)

<8> Load of lighting = heat gain/W \* lighting consumption vol. \* ope.rate  
 Fluorescent lamp 339 1.160 292 1.00  
 Incandescent lamp

<9> Load of human body(SH) = SH of human body \* No of psns. \* ope.rate  
 168 56 3 1.00

Load of human body(LH) = LH of human body \* No of psns. \* ope.rate  
 228 76 3 1.00

<10> Load of equipments = heat gain from internal equip. \* operating rate

<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)

Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff. \* 0.833 \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
 1760 1516 244  
 [ 1514] (kcal/h) [ 1304] [ 210]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
 1760 1760 0 0  
 [ 1514] (kcal/h) [ 1514] [ 0] [ 0]

OHTC : Overall heat transfer coefficient  
 SH : Sensible heat  
 LH : Latent heat  
 F/A : Fresh air  
 THEX : Total heat exchange efficiency

## Table of peak heat load detail(Heating)

[Room name:311 Toaleti ] , Floor: 4F Floor area: 14.6m<sup>2</sup> Ceiling height: 3.8m Peak time in heating:18:00  
Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 72.7%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW 434 1.10 1.00 (20.00+ 6.00) 2.00 2.20 6.4  
Shade  
Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW 85 1.10 1.00 (20.00+ 6.00) 2.00 0.60 ( 2.9\*3.8- 6.4)  
Shade  
(!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Overhead room exit 213 --- --- (20.00+ 6.00)\*0.40 --- 1.40 14.6  
Flat roof  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer 213 (20.00+ 6.00)\*0.40 1.40 14.6  
Without air layer  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
157 18.31 (20.00+ 6.00)  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
86 18.31 ( 7.26- 1.65)  
(Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
136 18.31 ( 7.26- 1.65) 1.10  
!Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
18.31 0.30 1.10 55.48

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
Fluorescent lamp  
Incandescent lamp

<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)

<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)

<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)

Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)

(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
1102 1102 0  
[ 948] (kcal/h) [ 948] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
1102 1102 0 0  
[ 948] (kcal/h) [ 948] [ 0] [ 0]  
!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
136 136 0

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

Table of peak heat load detail(Cooling)

[Room name:313 Kabinet 1 ] Floor: 4F Floor area: 19.9m2 Ceiling height: 3.8m Peak time in cooling:18:00									
Indoor temperature:26.0CDB , 50.0%RH Outdoor temperature:31.9CDB , 39.9%RH									
<1> Load of window glass									
-Material I / with blind-									
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.									
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.									
Azimuth									
N									
E									
S									
W									
NE									
SE									
SW									
NW									
88 (31.90-26.00) 2.20 6.8									
691 See <1>>Load detail of window glass with canopy									
Shade									
Skylight									
<2> Load of outer wall = effective temp.diff. * OHTC * area									
Azimuth									
N									
E									
S									
W									
NE									
SE									
SW									
NW									
49 13.40 0.60 ( 3.4*3.8- 6.8)									
Shade									
(!Area of outer wall=length of outer wall									
*floor height[ceiling height+height of ceiling adv attic]-window area)									
<3> Load of roof = effective temp.diff. * OHTC * area									
Overhead room exist									
Flat roof									
193 24.30 0.40 19.9									
Inclined roof									
<4> Load of floor = temp.diff. * OHTC * area									
Earth floor									
With air layer									
Without air layer									
66 (31.90-26.00)*0.40 1.40 19.9									
Pilotis									
<5> Load of inner wall = temp.diff. * OHTC * area									
Azimuth									
N									
E									
S									
W									
NE									
SE									
SW									
NW									
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length									
(depth<=2.4m)									
Load of underground wall = temp.diff. * OHTC * area									
(depth>2.4m)									
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33									
29 15.12 (31.90-26.00)									
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833									
17 15.12 (11.80-10.49)									
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate									
Fluorescent lamp									
346 1.160 299 1.00									
Incandescent lamp									
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate									
280 56 5 1.00									
Load of human body(LH) = LH of human body * No of psns. * ope.rate									
380 76 5 1.00									
<10> Load of equipments = heat gain from internal equip. * operating rate									
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)									
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)									
<<Total>> Indoor heat load(W) = SH + LH									
2139 1742 397									
[ 1840] (kcal/h) [ 1498] [ 341]									
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)									
2139 2139 0 0									
[ 1840] (kcal/h) [ 1840] [ 0] [ 0]									
OHTC : Overall heat transfer coefficient									
SH : Sensible heat									
LH : Latent heat									
F/A : Fresh air									
THEX : Total heat exchange efficiency									



Table of peak heat load detail of window with canopy(Cooling)

Arhitektonski fakultet 19/June/2018

<1'> Load detail of window glass with canopy

Upper:solar heat load	=	(S.SHG - S.SHG for shadow) * SG + S.SHG for shadow) * shading factor * area									
Lower:SG	=	( x * y ) / ( Ww * Hw ) <tanF, tanG> (!Area of heat transf. is contained sash area.									
S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.											
Azimuth	691	332	23	0.9	23	0.34	(6.80 * 0.95)				
NW	0.9	3.10	2.07	3.1	2.2	<	0.24,	-0.51>			

## Table of peak heat load detail(Heating)

[Room name:313 Kabinet 1 ] Floor: 4F Floor area: 19.9m2 Ceiling height: 3.8m Peak time in heating:18:00  
Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 72.7%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW 461 1.10 1.00 (20.00+ 6.00) 2.00 2.20 6.8  
Shade  
Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW 113 1.10 1.00 (20.00+ 6.00) 2.00 0.60 ( 3.4\*3.8- 6.8)  
NW  
Shade  
(!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Overhead room exit  
Flat roof 255 1.00 1.00 (20.00+ 6.00) 6.00 0.40 19.9  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer 290 (20.00+ 6.00)\*0.40 1.40 19.9  
Without air layer  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
214 24.95 (20.00+ 6.00)  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
117 24.95 ( 7.26- 1.65)  
(Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
185 24.95 ( 7.26- 1.65) 1.10  
!Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
24.95 0.30 1.10 75.62

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
Fluorescent lamp  
Incandescent lamp  
<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)  
<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)  
<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)  
Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)  
(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
1333 1333 0  
[ 1146] (kcal/h) [ 1146] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
1333 1333 0 0  
[ 1146] (kcal/h) [ 1146] [ 0] [ 0]  
!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
185 185 0

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

[Room name:314 Kabinet 2 ]		Floor: 4F	Floor area: 19.9m2	Ceiling height: 3.8m	Peak time in cooling:18:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:31.9CDB	, 39.9%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW	88	(31.90-26.00)	2.20	6.8	
Shade	691			See <1>	Load detail of window glass with canopy
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW	49	13.40	0.60	(3.4*3.8-6.8)	
Shade					
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist					
Flat roof	193	24.30	0.40	19.9	
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer	66	(31.90-26.00)*0.40	1.40	19.9	
Without air layer					
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
29 15.12 (31.90-26.00)					
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
17 15.12 (11.80-10.49)					
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp 346 1.160 299 1.00					
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
280 56 5 1.00					
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
380 76 5 1.00					
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
2139 1742 397					
[ 1840] (kcal/h) [ 1498] [ 341]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
2139 2139 0 0					
[ 1840] (kcal/h) [ 1840] [ 0] [ 0]					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					

Table of peak heat load detail of window with canopy(Cooling)

Arhitektonski fakultet 19/June/2018

<1'> Load detail of window glass with canopy

Upper:solar heat load	=	(S.SHG - S.SHG for shadow) * SG + S.SHG for shadow) * shading factor * area									
Lower:SG	=	( x * y ) / ( Ww * Hw ) <tanF, tanG> (!Area of heat transf. is contained sash area.									
S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.											
Azimuth	691	332	23		0.9	23		0.34	(6.80 * 0.95)		
NW	0.9	3.10	2.07		3.1	2.2		<	0.24,	-0.51>	

## Table of peak heat load detail(Heating)

[Room name:314 Kabinet 2 ] , Floor: 4F Floor area: 19.9m2 Ceiling height: 3.8m Peak time in heating:18:00  
Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 72.7%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW 461 1.10 1.00 (20.00+ 6.00) 2.00 2.20 6.8  
Shade  
Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW 113 1.10 1.00 (20.00+ 6.00) 2.00 0.60 ( 3.4\*3.8- 6.8)  
NW  
Shade  
(!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Overhead room exit  
Flat roof 255 1.00 1.00 (20.00+ 6.00) 6.00 0.40 19.9  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer 290 (20.00+ 6.00)\*0.40 1.40 19.9  
Without air layer  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
214 24.95 (20.00+ 6.00)  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
117 24.95 ( 7.26- 1.65)  
(Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
185 24.95 ( 7.26- 1.65) 1.10  
!Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
24.95 0.30 1.10 75.62

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
Fluorescent lamp  
Incandescent lamp  
<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)  
<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)  
<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)  
Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)  
(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
1333 1333 0  
[ 1146] (kcal/h) [ 1146] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
1333 1333 0 0  
[ 1146] (kcal/h) [ 1146] [ 0] [ 0]  
!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
185 185 0

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

[Room name:315 Kabinet 3 ]		Floor: 4F	Floor area: 18.2m2	Ceiling height: 3.8m	Peak time in cooling:18:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:31.9CDB	, 39.9%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW	88	(31.90-26.00)	2.20	6.8	
Shade	691				See <1>>Load detail of window glass with canopy
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW	40	13.40	0.60	( 3.1*3.8- 6.8)	
Shade					
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist					
Flat roof	177	24.30	0.40	18.2	
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer	60	(31.90-26.00)*0.40	1.40	18.2	
Without air layer					
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
27 13.83 (31.90-26.00)					
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
15 13.83 (11.80-10.49)					
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp 317 1.160 273 1.00					
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
280 56 5 1.00					
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
380 76 5 1.00					
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
2075 1680 395					
[ 1785] (kcal/h) [ 1445] [ 340]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
2075 2075 0 0					
[ 1785] (kcal/h) [ 1785] [ 0] [ 0]					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					

Table of peak heat load detail of window with canopy(Cooling)

Arhitektonski fakultet 19/June/2018

```
<1> Load detail of window glass with canopy
```

Upper:solar heat load	=	((S.SHG - S.SHG for shadow) * SG + S.SHG for shadow) * shading factor * area									
Lower:SG	=	( x * y ) / ( Ww * Hw ) <tanF, tanG> (!Area of heat transf. is contained sash area.									
		S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.									
Azimuth	691	332	23	0.9	23	0.34	(6.80 * 0.95)				
NW	0.9	3.10	2.07	3.1	2.2	<	0.24,	-0.51>			

## Table of peak heat load detail(Heating)

[Room name:315 Kabinet 3 ] Floor: 4F Floor area: 18.2m2 Ceiling height: 3.8m Peak time in heating:18:00  
Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 72.7%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW 461 1.10 1.00 (20.00+ 6.00) 2.00 2.20 6.8  
Shade  
Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW 92 1.10 1.00 (20.00+ 6.00) 2.00 0.60 ( 3.1\*3.8- 6.8)  
Shade  
(!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Overhead room exit  
Flat roof 233 1.00 1.00 (20.00+ 6.00) 6.00 0.40 18.2  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer 265 (20.00+ 6.00)\*0.40 1.40 18.2  
Without air layer  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
196 22.82 (20.00+ 6.00)  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
107 22.82 ( 7.26- 1.65)  
(Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
169 22.82 ( 7.26- 1.65) 1.10  
!Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
22.82 0.30 1.10 69.16

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
Fluorescent lamp  
Incandescent lamp

<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)

<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)

<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)

Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)

(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
1247 1247 0  
[ 1072] (kcal/h) [ 1072] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
1247 1247 0 0  
[ 1072] (kcal/h) [ 1072] [ 0] [ 0]  
!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
169 169 0

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency



## Table of peak heat load detail(Cooling)

[Room name:316 Kabinet 4 ]		Floor: 4F	Floor area: 20.9m2	Ceiling height: 3.8m	Peak time in cooling:17:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:33.3CDB	, 38.2%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
Shade					
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
Shade					
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist					
Flat roof					
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer					
Without air layer					
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
38 15.88 (33.30-26.00)					
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
23 15.88 (12.23-10.49)					
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp 364 1.160 314 1.00					
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
280 56 5 1.00					
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
380 76 5 1.00					
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
2558 2155 403					
[ 2200] (kcal/h) [ 1853] [ 347]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
2558 2558 0 0					
[ 2200] (kcal/h) [ 2200] [ 0] [ 0]					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					

Table of peak heat load detail of window with canopy(Cooling)

<l'> Load detail of window glass with canopy

Upper:solar heat load

=

(S.SHG - S.SHG for shadow)

\*

SG + S.SHG for shadow

\*

shading factor

\*

area

Lower:SG

=

( x \* y )

/

( Ww \* Hw )

<tanF, tanG>

(!Area of heat transf. is contained sash area.

S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.

Azimuth

NW

569

351

39

0.7

39

0.34

(6.80 \* 0.95)

NE

184

47

39

1.0

2.2

0.34

(12.10 \* 0.95)

1.0

5.50

2.20

5.5

2.2

0,

0>

## Table of peak heat load detail(Heating)

[Room name:316 Kabinet 4 ] , Floor: 4F Floor area: 20.9m2 Ceiling height: 3.8m Peak time in heating:18:00  
Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 72.7%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE 783 1.05 1.00 (20.00+ 6.00) 2.00 2.20 12.1  
SE  
SW  
NW 461 1.10 1.00 (20.00+ 6.00) 2.00 2.20 6.8  
Shade  
Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE 189 1.05 1.00 (20.00+ 6.00) 2.00 0.60 ( 6.0\*3.8-12.1)  
SE  
SW  
NW 127 1.10 1.00 (20.00+ 6.00) 2.00 0.60 ( 3.6\*3.8- 6.8)  
Shade  
(!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Overhead room exit  
Flat roof 268 1.00 1.00 (20.00+ 6.00) 6.00 0.40 20.9  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer 304 (20.00+ 6.00)\*0.40 1.40 20.9  
Without air layer  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
215 25.02 (20.00+ 6.00)  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
117 25.02 ( 7.26- 1.65)  
(Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
185 25.02 ( 7.26- 1.65) 1.10  
!Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
25.02 0.30 1.05 79.42

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
Fluorescent lamp  
Incandescent lamp

<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)

<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)

<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)

Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)

(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
2347 2347 0  
[ 2018] (kcal/h) [ 2018] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
2347 2347 0 0  
[ 2018] (kcal/h) [ 2018] [ 0] [ 0]  
!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
185 185 0

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

[Room name:317 Kabinet 5 ]		Floor: 4F	Floor area: 14.1m2	Ceiling height: 3.8m	Peak time in cooling:14:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:35.4CDB	, 35.6%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
Shade					
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
Shade					
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist					
Flat roof					
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer					
Without air layer					
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
33 10.72 (35.40-26.00)					
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
21 10.72 (12.82-10.49)					
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp 245 1.160 212 1.00					
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
168 56 3 1.00					
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
228 76 3 1.00					
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
1189 940 249					
[ 1023] (kcal/h) [ 808] [ 214]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
1189 1189 0 0					
[ 1023] (kcal/h) [ 1023] [ 0] [ 0]					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					

Table of peak heat load detail of window with canopy(Cooling)

Arhitektonski fakultet 19/June/2018

<1'> Load detail of window glass with canopy

Upper:solar heat load = ((S.SHG - S.SHG for shadow) \* SG + S.SHG for shadow) \* shading factor \* area

Lower:SG = ( x \* y ) / ( Ww \* Hw ) <tanF, tanG> (!Area of heat transf. is contained sash area.

S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.

Azimuth

NE15494721.0720.34(5.10 \* 0.95)

1.02.302.202.32.2<0,0>

## Table of peak heat load detail(Heating)

[Room name:317 Kabinet 5 ] , Floor: 4F Floor area: 14.1m<sup>2</sup> Ceiling height: 3.8m Peak time in heating:18:00  
Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 72.7%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE 330 1.05 1.00 (20.00+ 6.00) 2.00 2.20 5.1  
SE  
SW  
NW  
Shade  
Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE 98 1.05 1.00 (20.00+ 6.00) 2.00 0.60 ( 2.8\*3.8- 5.1)  
SE  
SW  
NW  
Shade  
(!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Overhead room exit  
Flat roof 180 1.00 1.00 (20.00+ 6.00) 6.00 0.40 14.1  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer 205 (20.00+ 6.00)\*0.40 1.40 14.1  
Without air layer  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m<sup>3</sup>/h) \* temp.diff. \* 0.33  
145 16.88 (20.00+ 6.00)  
Load of infiltration(LH) = infiltration vol.(m<sup>3</sup>/h) \* abs.humid.diff.(g/kg) \* 0.833  
79 16.88 ( 7.26- 1.65)  
(Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
125 16.88 ( 7.26- 1.65) 1.10  
!Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
16.88 0.30 1.05 53.58

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
Fluorescent lamp  
Incandescent lamp  
<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)  
<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)  
<11> Fresh air load(SH) = F/A vol.(m<sup>3</sup>/h) \* temp.diff. \* 0.33 \* (1 - THEX)  
Fresh air load(LH) = F/A vol.(m<sup>3</sup>/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)  
(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
958 958 0  
[ 824] (kcal/h) [ 824] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
958 958 0 0  
[ 824] (kcal/h) [ 824] [ 0] [ 0]  
!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
125 125 0

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

[Room name:318 Kabinet 6 ]		Floor: 4F	Floor area: 16.1m2	Ceiling height: 3.8m	Peak time in cooling:14:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:35.4CDB	, 35.6%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
Shade					
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
Shade					
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist					
Flat roof					
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer					
Without air layer					
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
38 12.24 (35.40-26.00)					
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
24 12.24 (12.82-10.49)					
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp 280 1.160 242 1.00					
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
168 56 3 1.00					
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
228 76 3 1.00					
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
1349 1097 252					
[ 1160] (kcal/h) [ 943] [ 217]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
1349 1349 0 0					
[ 1160] (kcal/h) [ 1160] [ 0] [ 0]					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					

Table of peak heat load detail of window with canopy(Cooling)

Arhitektonski fakultet 19/June/2018

<1'> Load detail of window glass with canopy

Upper:solar heat load	=	((S.SHG - S.SHG for shadow) * SG + S.SHG for shadow) * shading factor * area									
Lower:SG	=	( x * y ) / ( Ww * Hw ) <tanF, tanG> (!Area of heat transf. is contained sash area.									
S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.											
Azimuth	207	94	72		1.0	72		0.34		(6.80 * 0.95)	
NE	1.0	3.10	2.20	3.1	2.2		<	0,		0>	



## Table of peak heat load detail(Heating)

[Room name:318 Kabinet 6 ] , Floor: 4F Floor area: 16.1m2 Ceiling height: 3.8m Peak time in heating:18:00  
Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 72.7%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE 440 1.05 1.00 (20.00+ 6.00) 2.00 2.20 6.8  
SE  
SW  
NW  
Shade  
Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE 95 1.05 1.00 (20.00+ 6.00) 2.00 0.60 ( 3.2\*3.8- 6.8)  
SE  
SW  
NW  
Shade  
(!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Overhead room exit  
Flat roof 206 1.00 1.00 (20.00+ 6.00) 6.00 0.40 16.1  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer 234 (20.00+ 6.00)\*0.40 1.40 16.1  
Without air layer  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
165 19.27 (20.00+ 6.00)  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
90 19.27 ( 7.26- 1.65)  
(Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
143 19.27 ( 7.26- 1.65) 1.10  
!Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
19.27 0.30 1.05 61.18

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
Fluorescent lamp  
Incandescent lamp  
<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)  
<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)  
<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)  
Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)  
(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
1140 1140 0  
[ 980] (kcal/h) [ 980] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
1140 1140 0 0  
[ 980] (kcal/h) [ 980] [ 0] [ 0]

!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
143 143 0

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

Table of peak heat load detail(Cooling)

Room name:319 Kabinet 7  
Indoor temperature:26.0CDB

Floor: 4F  
50.0%RH

Floor area: 18.1m2  
Outdoor temperature:35.4CDB

Ceiling height: 3.8m  
35.6%RH

Peak time in cooling:14:00

<1> Load of window glass

-Material I / with blind-

Upper:heat transfer load = temp.diff. \* OHTC \* area

Lower:solar heat load = area \* std.solar heat gain \* shading factor

Area of heat transf. is contained sash area.

Area of solar heat gain is not contained sash area.

Azimuth

N

E

S

W

NE

213 (35.40-26.00) 2.20 10.3

314 See <1>Load detail of window glass with canopy

SE

141 (35.40-26.00) 2.20 6.8

207 See <1>Load detail of window glass with canopy

SW

NW

Shade

Skylight

<2> Load of outer wall = effective temp.diff. \* OHTC \* area

Azimuth

N

E

S

W

NE

57 10.00 0.60 ( 5.2\*3.8-10.3)

SE

59 14.20 0.60 ( 3.6\*3.8- 6.8)

SW

NW

Shade

(!Area of outer wall=length of outer wall

\*floor height[ceiling height+height of ceiling adv attic]-window area)

<3> Load of roof = effective temp.diff. \* OHTC \* area

Overhead room exist

Flat roof

164 22.70 0.40 18.1

Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area

Earth floor

With air layer

Without air layer

95 (35.40-26.00)\*0.40 1.40 18.1

Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area

Azimuth

N

E

S

W

NE

SE

SW

NW

<6> Load of underground wall = temp.diff. \* OHTC/unit ambient length \* ambient length

(depth<=2.4m)

Load of underground wall = temp.diff. \* OHTC \* area

(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33

43 13.76 (35.40-26.00)

Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833

27 13.76 (12.82-10.49)

<8> Load of lighting = heat gain/W \* lighting consumption vol. \* ope.rate

Fluorescent lamp

420 1.160 362 1.00

Incandescent lamp

<9> Load of human body(SH) = SH of human body \* No of psns. \* ope.rate

224 56 4 1.00

Load of human body(LH) = LH of human body \* No of psns. \* ope.rate

304 76 4 1.00

<10> Load of equipments = heat gain from internal equip. \* operating rate

<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)

Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff. \* 0.833 \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH

2268 1937 331

[ 1950] (kcal/h) [ 1666] [ 285]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)

2268 2268 0 0

[ 1950] (kcal/h) [ 1950] [ 0] [ 0]

OHTC : Overall heat transfer coefficient

SH : Sensible heat

LH : Latent heat

F/A : Fresh air

THEX : Total heat exchange efficiency

Table of peak heat load detail of window with canopy(Cooling)

Arhitektonski fakultet 19/June/2018

<> Load detail of window glass with canopy

Upper:solar heat load = ((S.SHG - S.SHG for shadow) \* SG + S.SHG for shadow) \* shading factor \* area

Lower:SG = ( x \* y ) / ( Ww \* Hw ) <tanF, tanG> (!Area of heat transf. is contained sash area.

S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.

Azimuth

NE

314

94

72

1.0

72

0.34

(10.30 \* 0.95)

1.0

4.70

2.20

4.7

2.2

<

0.34

0,

0>

SE

207

94

72

1.0

72

0.34

(6.80 \* 0.95)

1.0

3.10

2.20

3.1

2.2

<

0,

0>

## Table of peak heat load detail(Heating)

[Room name:319 Kabinet 7 ] Floor: 4F Floor area: 18.1m<sup>2</sup> Ceiling height: 3.8m Peak time in heating:18:00  
 Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 72.7%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE 666 1.05 1.00 (20.00+ 6.00) 2.00 2.20 10.3  
 SE 440 1.05 1.00 (20.00+ 6.00) 2.00 2.20 6.8  
 SW  
 NW  
 Shade  
 Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE 167 1.05 1.00 (20.00+ 6.00) 2.00 0.60 ( 5.2\*3.8-10.3)  
 SE 121 1.05 1.00 (20.00+ 6.00) 2.00 0.60 ( 3.6\*3.8- 6.8)  
 SW  
 NW  
 Shade  
 (!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
 Overhead room exit  
 Flat roof 232 1.00 1.00 (20.00+ 6.00) 6.00 0.40 18.1  
 Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
 Earth floor  
 With air layer 264 (20.00+ 6.00)\*0.40 1.40 18.1  
 Without air layer  
 Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
 Azimuth  
 N  
 E  
 S  
 W  
 NE  
 SE  
 SW  
 NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
 (depth<=2.4m)  
 Load of underground wall = temp.diff. \* OHTC \* area  
 (depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m<sup>3</sup>/h) \* temp.diff. \* 0.33  
 186 21.67 (20.00+ 6.00)  
 Load of infiltration(LH) = infiltration vol.(m<sup>3</sup>/h) \* abs.humid.diff.(g/kg) \* 0.833  
 101 21.67 ( 7.26- 1.65)  
 (Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
 160 21.67 ( 7.26- 1.65) 1.10  
 !Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
 21.67 0.30 1.05 68.78

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
 Fluorescent lamp  
 Incandescent lamp  
 <9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)  
 <10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)  
 <11> Fresh air load(SH) = F/A vol.(m<sup>3</sup>/h) \* temp.diff. \* 0.33 \* (1 - THEX)  
 Fresh air load(LH) = F/A vol.(m<sup>3</sup>/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)  
 (Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
 2076 2076 0  
 [ 1785] (kcal/h) [ 1785] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
 2076 2076 0 0  
 [ 1785] (kcal/h) [ 1785] [ 0] [ 0]  
 !Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
 160 160 0

OHTC : Overall heat transfer coefficient  
 SH : Sensible heat  
 LH : Latent heat  
 F/A : Fresh air  
 THEX : Total heat exchange efficiency

Table of peak heat load detail(Cooling)

Room name:320 Kabinet 8  
Indoor temperature:26.0CDB

Floor: 4F  
50.0%RH

Floor area: 15.7m2  
Outdoor temperature:35.4CDB

Ceiling height: 3.8m  
35.6%RH

Peak time in cooling:14:00

<1> Load of window glass

-Material I / with blind-

Upper:heat transfer load = temp.diff. \* OHTC \* area (!Area of heat transf. is contained sash area.

Lower:solar heat load = area \* std.solar heat gain \* shading factor (!Area of solar heat gain is not contained sash area.

Azimuth

N

E

S

W

NE

SE 141 (35.40-26.00) 2.20 6.8

SW 207 See <1>Load detail of window glass with canopy

NW

Shade

Skylight

<2> Load of outer wall = effective temp.diff. \* OHTC \* area

Azimuth

N

E

S

W

NE

SE 42 14.20 0.60 ( 3.1\*3.8- 6.8)

SW

NW

Shade

(!Area of outer wall=length of outer wall

\*floor height[ceiling height+height of ceiling adv attic]-window area)

<3> Load of roof = effective temp.diff. \* OHTC \* area

Overhead room exist

Flat roof 143 22.70 0.40 15.7

Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area

Earth floor

With air layer

Without air layer

Pilotis 83 (35.40-26.00)\*0.40 1.40 15.7

<5> Load of inner wall = temp.diff. \* OHTC \* area

Azimuth

N

E

S

W

NE

SE

SW

NW

<6> Load of underground wall = temp.diff. \* OHTC/unit ambient length \* ambient length

(depth<=2.4m)

Load of underground wall = temp.diff. \* OHTC \* area

(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33

37 11.93 (35.40-26.00)

Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833

23 11.93 (12.82-10.49)

<8> Load of lighting = heat gain/W \* lighting consumption vol. \* ope.rate

Fluorescent lamp 364 1.160 314 1.00

Incandescent lamp

<9> Load of human body(SH) = SH of human body \* No of psns. \* ope.rate

224 56 4 1.00

Load of human body(LH) = LH of human body \* No of psns. \* ope.rate

304 76 4 1.00

<10> Load of equipments = heat gain from internal equip. \* operating rate

<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)

Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff. \* 0.833 \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH

1568 1241 327

[ 1348] (kcal/h) [ 1067] [ 281]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)

1568 1568 0 0

[ 1348] (kcal/h) [ 1348] [ 0] [ 0]

OHTC : Overall heat transfer coefficient

SH : Sensible heat

LH : Latent heat

F/A : Fresh air

THEX : Total heat exchange efficiency

Table of peak heat load detail of window with canopy(Cooling)

Arhitektonski fakultet 19/June/2018

<1'> Load detail of window glass with canopy

Upper:solar heat load = ((S.SHG - S.SHG for shadow) \* SG + S.SHG for shadow) \* shading factor \* area

Lower:SG = ( x \* y ) / ( Ww \* Hw ) <tanF, tanG> (!Area of heat transf. is contained sash area.

S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.

Azimuth

SE

207

94

72

1.0

72

0.34

(6.80 \* 0.95)

1.0

3.10

2.20

3.1

2.2

<

0,

0>

## Table of peak heat load detail(Heating)

[Room name:320 Kabinet 8 ] Floor: 4F Floor area: 15.7m2 Ceiling height: 3.8m Peak time in heating:18:00  
Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 72.7%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE 440 1.05 1.00 (20.00+ 6.00) 2.00 2.20 6.8  
SW  
NW  
Shade  
Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE 88 1.05 1.00 (20.00+ 6.00) 2.00 0.60 ( 3.1\*3.8- 6.8)  
SW  
NW  
Shade  
(!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Overhead room exit  
Flat roof 201 1.00 1.00 (20.00+ 6.00) 6.00 0.40 15.7  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer 229 (20.00+ 6.00)\*0.40 1.40 15.7  
Without air layer  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
161 18.79 (20.00+ 6.00)  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
88 18.79 ( 7.26- 1.65)  
(Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
139 18.79 ( 7.26- 1.65) 1.10  
!Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
18.79 0.30 1.05 59.66

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
Fluorescent lamp  
Incandescent lamp  
<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)  
<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)  
<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)  
Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)  
(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
1119 1119 0  
[ 962] (kcal/h) [ 962] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
1119 1119 0 0  
[ 962] (kcal/h) [ 962] [ 0] [ 0]  
!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
139 139 0

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

Room name:321 Kabinet 9  
Indoor temperature:26.0CDB , 50.0%RH  
Floor: 4F  
Floor area: 17.2m2  
Ceiling height: 3.8m  
Peak time in cooling:14:00  
Outdoor temperature:35.4CDB , 35.6%RH

<1> Load of window glass  
-Material I / with blind-  
Upper:heat transfer load = temp.diff. \* OHTC \* area (!Area of heat transf. is contained sash area.  
Lower:solar heat load = area \* std.solar heat gain \* shading factor (!Area of solar heat gain is not contained sash area.  
Azimuth  
N  
E  
S  
W  
NE  
SE 141 (35.40-26.00) 2.20 6.8  
207 See <1'>Load detail of window glass with canopy  
SW  
NW  
Shade  
Skylight

<2> Load of outer wall = effective temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE 52 14.20 0.60 ( 3.4\*3.8- 6.8)  
SE  
SW  
NW  
Shade  
(!Area of outer wall=length of outer wall  
\*floor height[ceiling height+height of ceiling adv attic]-window area)  
<3> Load of roof = effective temp.diff. \* OHTC \* area  
Overhead room exist  
Flat roof 156 22.70 0.40 17.2  
Inclined roof  
<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer  
Without air layer  
Pilotis 91 (35.40-26.00)\*0.40 1.40 17.2  
<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW  
<6> Load of underground wall = temp.diff. \* OHTC/unit ambient length \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
41 13.07 (35.40-26.00)  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
25 13.07 (12.82-10.49)  
<8> Load of lighting = heat gain/W \* lighting consumption vol. \* ope.rate  
Fluorescent lamp 399 1.160 344 1.00  
Incandescent lamp  
<9> Load of human body(SH) = SH of human body \* No of psns. \* ope.rate  
168 56 3 1.00  
Load of human body(LH) = LH of human body \* No of psns. \* ope.rate  
228 76 3 1.00  
<10> Load of equipments = heat gain from internal equip. \* operating rate  
<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)  
Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff. \* 0.833 \* (1 - THEX)  
<<Total>> Indoor heat load(W) = SH + LH  
1508 1255 253  
[ 1297] (kcal/h) [ 1079] [ 218]  
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
1508 1508 0 0  
[ 1297] (kcal/h) [ 1297] [ 0] [ 0]  
OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency



Table of peak heat load detail of window with canopy(Cooling)

Arhitektonski fakultet 19/June/2018

<1'> Load detail of window glass with canopy

Upper:solar heat load = ((S.SHG - S.SHG for shadow) \* SG + S.SHG for shadow) \* shading factor \* area

Lower:SG = ( x \* y ) / ( Ww \* Hw ) <tanF, tanG> (!Area of heat transf. is contained sash area.

S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.

Azimuth

SE

207

94

72

1.0

72

0.34

(6.80 \* 0.95)

1.0

3.10

2.20

3.1

2.2

<

0,

0>

## Table of peak heat load detail(Heating)

[Room name:321 Kabinet 9 ] Floor: 4F Floor area: 17.2m<sup>2</sup> Ceiling height: 3.8m Peak time in heating:18:00  
Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 72.7%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE 440 1.05 1.00 (20.00+ 6.00) 2.00 2.20 6.8  
SW  
NW  
Shade  
Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE 108 1.05 1.00 (20.00+ 6.00) 2.00 0.60 ( 3.4\*3.8- 6.8)  
SW  
NW  
Shade  
(!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Overhead room exit  
Flat roof 220 1.00 1.00 (20.00+ 6.00) 6.00 0.40 17.2  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer 250 (20.00+ 6.00)\*0.40 1.40 17.2  
Without air layer  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
177 20.59 (20.00+ 6.00)  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
96 20.59 ( 7.26- 1.65)  
(Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
152 20.59 ( 7.26- 1.65) 1.10  
!Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
20.59 0.30 1.05 65.36

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
Fluorescent lamp  
Incandescent lamp  
<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)  
<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)  
<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)  
Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)  
(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
1195 1195 0  
[ 1028] (kcal/h) [ 1028] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
1195 1195 0 0  
[ 1028] (kcal/h) [ 1028] [ 0] [ 0]  
!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
152 152 0

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

[Room name:322 Kabinet 10 ]		Floor: 4F	Floor area: 17.2m2	Ceiling height: 3.8m	Peak time in cooling:14:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:35.4CDB	, 35.6%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE	141	(35.40-26.00)	2.20	6.8	
SW	207				See <1'>Load detail of window glass with canopy
NW					
Shade					
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE	52	14.20	0.60	( 3.4*3.8- 6.8)	
SW					
NW					
Shade					
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist					
Flat roof	156	22.70	0.40	17.2	
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer	91	(35.40-26.00)*0.40	1.40	17.2	
Without air layer					
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
41 13.07 (35.40-26.00)					
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
25 13.07 (12.82-10.49)					
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp	399	1.160	344	1.00	
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
168 56 3 1.00					
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
228 76 3 1.00					
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
1508 1255 253					
[ 1297] (kcal/h) [ 1079] [ 218]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
1508 1508 0 0					
[ 1297] (kcal/h) [ 1297] [ 0] [ 0]					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					

Table of peak heat load detail of window with canopy(Cooling)

Arhitektonski fakultet 19/June/2018

<1'> Load detail of window glass with canopy

Upper:solar heat load = ((S.SHG - S.SHG for shadow) \* SG + S.SHG for shadow) \* shading factor \* area

Lower:SG = ( x \* y ) / ( Ww \* Hw ) <tanF, tanG> (!Area of heat transf. is contained sash area.

S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.

Azimuth

SE

207

94

72

1.0

72

0.34

(6.80 \* 0.95)

1.0

3.10

2.20

3.1

2.2

<

0,

0>

## Table of peak heat load detail(Heating)

[Room name:322 Kabinet 10 ] Floor: 4F Floor area: 17.2m<sup>2</sup> Ceiling height: 3.8m Peak time in heating:18:00  
Indoor temperature:20.0CDB , 50.0%RH Outdoor temperature:-6.0CDB , 72.7%RH

<1> Load of window glass = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE 440 1.05 1.00 (20.00+ 6.00) 2.00 2.20 6.8  
SW  
NW  
Shade  
Skylight

<2> Load of outer wall = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE 108 1.05 1.00 (20.00+ 6.00) 2.00 0.60 ( 3.4\*3.8- 6.8)  
SW  
NW  
Shade  
(!Area of outer wall=length of outer wall\*floor height[ceiling height+height of ceiling adv.attic.]-window area)

<3> Load of roof = azimuth factor \* increasing factor of ceiling height \* (temp.diff. + radiant cooling effect) \* OHTC \* area  
Overhead room exit  
Flat roof 220 1.00 1.00 (20.00+ 6.00) 6.00 0.40 17.2  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer 250 (20.00+ 6.00)\*0.40 1.40 17.2  
Without air layer  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m<sup>3</sup>/h) \* temp.diff. \* 0.33  
177 20.59 (20.00+ 6.00)  
Load of infiltration(LH) = infiltration vol.(m<sup>3</sup>/h) \* abs.humid.diff.(g/kg) \* 0.833  
96 20.59 ( 7.26- 1.65)  
(Humidifying vol.)(g/h) = infiltration vol. \* abs.humid.diff. \* 1.2 \* safety factor  
152 20.59 ( 7.26- 1.65) 1.10  
!Infiltration vol. = No of ventilation \* azimuth factor \* room capacity  
20.59 0.30 1.05 65.36

<8> Load of lighting = -(heat gain/W \* lighting consumption vol. \* ope.rate \* probable rate)  
Fluorescent lamp  
Incandescent lamp  
<9> Load of human body(SH) = -(SH of human body \* No of psns \* ope.rate \* probable rate)  
<10> Load of equipments = -(heat gain from internal equip. \* operating rate \* probable rate)  
<11> Fresh air load(SH) = F/A vol.(m<sup>3</sup>/h) \* temp.diff. \* 0.33 \* (1 - THEX)  
Fresh air load(LH) = F/A vol.(m<sup>3</sup>/h) \* abs.humid.diff.(g/kg) \* 0.833 \* (1 - THEX)  
(Humidifying vol.) = F/A vol. \* abs.humid.diff. \* 1.2 \* safety factor \* (1 - THEX)

<<Total>> Indoor heat load(W) = SH + LH  
1195 1195 0  
[ 1028] (kcal/h) [ 1028] [ 0]

Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
1195 1195 0 0  
[ 1028] (kcal/h) [ 1028] [ 0] [ 0]  
!Indoor heat load & total heat load are not contained latent heat.

Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air  
152 152 0

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

## Table of peak heat load detail(Cooling)

Room name:323 Kabinet 11 | Floor: 4F | Floor area: 15.7m2 | Ceiling height: 3.8m | Peak time in cooling:14:00  
Indoor temperature:26.0CDB | , 50.0%RH | Outdoor temperature:35.4CDB | , 35.6%RH

<1> Load of window glass  
-Material I / with blind-  
Upper:heat transfer load = temp.diff. \* OHTC \* area (!Area of heat transf. is contained sash area.  
Lower:solar heat load = area \* std.solar heat gain \* shading factor (!Area of solar heat gain is not contained sash area.  
Azimuth  
N  
E  
S  
W  
NE  
SE 141 (35.40-26.00) 2.20 6.8  
207 See <1>Load detail of window glass with canopy  
SW  
NW  
Shade  
Skylight

<2> Load of outer wall = effective temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE 42 14.20 0.60 ( 3.1\*3.8- 6.8)  
SW  
NW  
Shade  
(!Area of outer wall=length of outer wall  
\*floor height[ceiling height+height of ceiling adv attic]-window area)

<3> Load of roof = effective temp.diff. \* OHTC \* area  
Overhead room exist  
Flat roof 143 22.70 0.40 15.7  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer  
Without air layer 83 (35.40-26.00)\*0.40 1.40 15.7  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC/unit ambient length \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
37 11.93 (35.40-26.00)  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
23 11.93 (12.82-10.49)  
<8> Load of lighting = heat gain/W \* lighting consumption vol. \* ope.rate  
Fluorescent lamp 364 1.160 314 1.00  
Incandescent lamp  
<9> Load of human body(SH) = SH of human body \* No of psns. \* ope.rate  
168 56 3 1.00  
Load of human body(LH) = LH of human body \* No of psns. \* ope.rate  
228 76 3 1.00  
<10> Load of equipments = heat gain from internal equip. \* operating rate  
<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)  
Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff. \* 0.833 \* (1 - THEX)  
<<Total>> Indoor heat load(W) = SH + LH  
1436 1185 251  
[ 1235] (kcal/h) [ 1019] [ 216]  
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
1436 1436 0 0  
[ 1235] (kcal/h) [ 1235] [ 0] [ 0]  
OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

Table of peak heat load detail of window with canopy(Cooling)

Arhitektonski fakultet 19/June/2018

<1'> Load detail of window glass with canopy

Upper:solar heat load	=	(S.SHG - S.SHG for shadow) * SG + S.SHG for shadow) * shading factor * area									
Lower:SG	=	( x * y ) / ( Ww * Hw )	<tanF, tanG>		(!Area of heat transf. is contained sash area.						
S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.											
Azimuth	207	94	72		1.0	72		0.34		(6.80 * 0.95)	
SE	1.0	3.10	2.20	3.1	2.2		<	0,		0>	

## Table of peak heat load detail(Heating)

[Room name:323 Kabinet 11 ]		Floor: 4F		Floor area: 15.7m2		Ceiling height: 3.8m		Peak time in heating:18:00	
Indoor temperature:20.0CDB		, 50.0%RH		Outdoor temperature:-6.0CDB		, 72.7%RH			
<1> Load of window glass = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area									
Azimuth									
N									
E									
S									
W									
NE									
SE 440 1.05 1.00 (20.00+ 6.00) 2.00 2.20 6.8									
SW									
NW									
Shade									
Skylight									
<2> Load of outer wall = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area									
Azimuth									
N									
E									
S									
W									
NE									
SE 88 1.05 1.00 (20.00+ 6.00) 2.00 0.60 ( 3.1*3.8- 6.8)									
SW									
NW									
Shade									
(!Area of outer wall=length of outer wall*floor height[ceiling height+height of ceiling adv.attic.]-window area)									
<3> Load of roof = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area									
Overhead room exit									
Flat roof 201 1.00 1.00 (20.00+ 6.00) 6.00 0.40 15.7									
Inclined roof									
<4> Load of floor = temp.diff. * OHTC * area									
Earth floor									
With air layer									
Without air layer 229 (20.00+ 6.00)*0.40 1.40 15.7									
Pilotis									
<5> Load of inner wall = temp.diff. * OHTC * area									
Azimuth									
N									
E									
S									
W									
NE									
SE									
SW									
NW									
<6> Load of underground wall = temp.diff. * OHTC * ambient length									
(depth<=2.4m)									
Load of underground wall = temp.diff. * OHTC * area									
(depth>2.4m)									
<<Total>> Indoor heat load(W) = SH + LH									
1119 1119 0									
[ 962] (kcal/h) [ 962] [ 0]									
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)									
1119 1119 0 0									
[ 962] (kcal/h) [ 962] [ 0] [ 0]									
!Indoor heat load & total heat load are not contained latent heat.									
Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air									
139 139 0									
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33									
161 18.79 (20.00+ 6.00)									
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833									
88 18.79 ( 7.26- 1.65)									
(Humidifying vol.)(g/h) = infiltration vol. * abs.humid.diff. * 1.2 * safety factor									
139 18.79 ( 7.26- 1.65) 1.10									
!Infiltration vol. = No of ventilation * azimuth factor * room capacity									
18.79 0.30 1.05 59.66									
OHTC : Overall heat transfer coefficient									
SH : Sensible heat									
LH : Latent heat									
F/A : Fresh air									
THEX : Total heat exchange efficiency									



## Table of peak heat load detail(Cooling)

Room name:324 Sekretarica ] Floor: 4F Floor area: 18.2m2 Ceiling height: 3.8m Peak time in cooling:14:00  
Indoor temperature:26.0CDB , 50.0%RH Outdoor temperature:35.4CDB , 35.6%RH

<1> Load of window glass  
-Material I / with blind-  
Upper:heat transfer load = temp.diff. \* OHTC \* area (!Area of heat transf. is contained sash area.  
Lower:solar heat load = area \* std.solar heat gain \* shading factor (!Area of solar heat gain is not contained sash area.  
Azimuth  
N  
E  
S  
W  
NE  
SE 141 (35.40-26.00) 2.20 6.8  
207 See <1'>Load detail of window glass with canopy  
SW  
NW  
Shade  
Skylight

<2> Load of outer wall = effective temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE 59 14.20 0.60 ( 3.6\*3.8- 6.8)  
SE  
SW  
NW  
Shade  
(!Area of outer wall=length of outer wall  
\*floor height[ceiling height+height of ceiling adv attic]-window area)

<3> Load of roof = effective temp.diff. \* OHTC \* area  
Overhead room exist  
Flat roof 165 22.70 0.40 18.2  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer  
Without air layer 96 (35.40-26.00)\*0.40 1.40 18.2  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC/unit ambient length \* ambient length  
(depth<=2.4m)  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
43 13.83 (35.40-26.00)  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
27 13.83 (12.82-10.49)  
<8> Load of lighting = heat gain/W \* lighting consumption vol. \* ope.rate  
Fluorescent lamp 422 1.160 364 1.00  
Incandescent lamp  
<9> Load of human body(SH) = SH of human body \* No of psns. \* ope.rate  
168 56 3 1.00  
Load of human body(LH) = LH of human body \* No of psns. \* ope.rate  
228 76 3 1.00  
<10> Load of equipments = heat gain from internal equip. \* operating rate  
<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)  
Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff. \* 0.833 \* (1 - THEX)  
<<Total>> Indoor heat load(W) = SH + LH  
1556 1301 255  
[ 1338] (kcal/h) [ 1119] [ 219]  
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
1556 1556 0 0  
[ 1338] (kcal/h) [ 1338] [ 0] [ 0]  
OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

Table of peak heat load detail of window with canopy(Cooling)

Arhitektonski fakultet 19/June/2018

<1'> Load detail of window glass with canopy

Upper:solar heat load	=	((S.SHG - S.SHG for shadow) * SG + S.SHG for shadow) * shading factor * area									
Lower:SG	=	( x * y ) / ( Ww * Hw ) <tanF, tanG> (!Area of heat transf. is contained sash area.									
S.SHG::std.solar heat gain, SG::Glass surface solar radition ratio.											
Azimuth	207	94	72		1.0	72		0.34		(6.80 * 0.95)	
SE	1.0	3.10	2.20	3.1	2.2		<	0,		0>	

## Table of peak heat load detail(Heating)

[Room name:324 Sekretarica ]		Floor: 4F	Floor area: 18.2m2	Ceiling height: 3.8m	Peak time in heating:18:00
Indoor temperature:20.0CDB		, 50.0%RH	Outdoor temperature:-6.0CDB	, 72.7%RH	
<1> Load of window glass = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE	440	1.05	1.00	(20.00+ 6.00)	2.00 2.20 6.8
SW					
NW					
Shade					
Skylight					
<2> Load of outer wall = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE	121	1.05	1.00	(20.00+ 6.00)	2.00 0.60 ( 3.6*3.8- 6.8)
SW					
NW					
Shade					
(!Area of outer wall=length of outer wall*floor height[ceiling height+height of ceiling adv.attic.]-window area)					
<3> Load of roof = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area					
Overhead room exit					
Flat roof	233	1.00	1.00	(20.00+ 6.00)	6.00 0.40 18.2
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer	265	(20.00+ 6.00)*0.40	1.40	18.2	
Without air layer					
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
187	21.79	(20.00+ 6.00)			
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
102	21.79	( 7.26- 1.65)			
(Humidifying vol.)(g/h) = infiltration vol. * abs.humid.diff. * 1.2 * safety factor					
161	21.79	( 7.26- 1.65)	1.10		
!Infiltration vol. = No of ventilation * azimuth factor * room capacity					
21.79	0.30	1.05	69.16		
<8> Load of lighting = -(heat gain/W * lighting consumption vol. * ope.rate * probable rate)					
Fluorescent lamp					
Incandescent lamp					
<9> Load of human body(SH) = -(SH of human body * No of psns * ope.rate * probable rate)					
<10> Load of equipments = -(heat gain from internal equip. * operating rate * probable rate)					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833 * (1 - THEX)					
(Humidifying vol.) = F/A vol. * abs.humid.diff. * 1.2 * safety factor * (1 - THEX)					
<<Total>> Indoor heat load(W) = SH + LH					
1246 1246 0					
[ 1072] (kcal/h) [ 1072] [ 0]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
1246 1246 0 0					
[ 1072] (kcal/h) [ 1072] [ 0] [ 0]					
!Indoor heat load & total heat load are not contained latent heat.					
Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air					
161 161 0					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					

Table of peak heat load detail(Cooling)

[Room name:325 Trpezarija ]		Floor: 4F	Floor area: 23.3m2	Ceiling height: 3.8m	Peak time in cooling:15:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:35.3CDB	, 35.6%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
Shade					
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
Shade					
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist					
Flat roof	240	25.70	0.40	23.3	
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer	121	(35.30-26.00)*0.40	1.40	23.3	
Without air layer					
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
54 17.71 (35.30-26.00)					
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
33 17.71 (12.75-10.49)					
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp	541	1.160	466	1.00	
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
672 56 12 1.00					
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
912 76 12 1.00					
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
307 500.0 (35.30-26.00) 0.800					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
188 500.0 (12.75-10.49) 0.800					
<<Total>> Indoor heat load(W) = SH + LH					
2573 1628 945					
[ 2213] (kcal/h) [ 1400] [ 813]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
3068 2573 307 188					
[ 2638] (kcal/h) [ 2213] [ 264] [ 162]					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					

## Table of peak heat load detail(Heating)

[Room name:325 Trpezarija ]		Floor: 4F	Floor area: 23.3m2	Ceiling height: 3.8m	Peak time in heating:18:00
Indoor temperature:20.0CDB		, 50.0%RH	Outdoor temperature:-6.0CDB	, 72.7%RH	
<1> Load of window glass = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area Azimuth N E S W NE SE SW NW Shade Skylight					
<2> Load of outer wall = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area Azimuth N E S W NE SE SW NW Shade (!Area of outer wall=length of outer wall*floor height[ceiling height+height of ceiling adv.attic.]-window area)					
<3> Load of roof = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area Overhead room exit Flat roof 298 1.00 1.00 (20.00+ 6.00) 6.00 0.40 23.3 Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area Earth floor With air layer 339 (20.00+ 6.00)*0.40 1.40 23.3 Without air layer Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area Azimuth N E S W NE SE SW NW					
<6> Load of underground wall = temp.diff. * OHTC * ambient length (depth<=2.4m) Load of underground wall = temp.diff. * OHTC * area (depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33 251 29.22 (20.00+ 6.00) Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833 137 29.22 ( 7.26- 1.65) (Humidifying vol.) (g/h) = infiltration vol. * abs.humid.diff. * 1.2 * safety factor 216 29.22 ( 7.26- 1.65) 1.10 !Infiltration vol. = No of ventilation * azimuth factor * room capacity 29.22 0.30 1.10 88.54					
<8> Load of lighting = -(heat gain/W * lighting consumption vol. * ope.rate * probable rate) Fluorescent lamp Incandescent lamp					
<9> Load of human body(SH) = -(SH of human body * No of psns * ope.rate * probable rate)					
<10> Load of equipments = -(heat gain from internal equip. * operating rate * probable rate)					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX) 644 500.0 (20.00+ 6.00) 0.850 Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833 * (1 - THEX) 350 500.0 ( 7.26- 1.65) 0.850 (Humidifying vol.) = F/A vol. * abs.humid.diff. * 1.2 * safety factor * (1 - THEX) 555 500.0 ( 7.26- 1.65) 1.10 0.850					
<<Total>> Indoor heat load(W) = SH + LH 888 888 0 [ 764] (kcal/h) [ 764] [ 0] Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH) 1532 888 644 0 [ 1318] (kcal/h) [ 764] [ 554] [ 0] !Indoor heat load & total heat load are not contained latent heat. Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air 771 216 555					
OHTC : Overall heat transfer coefficient SH : Sensible heat LH : Latent heat F/A : Fresh air THEX : Total heat exchange efficiency					

Table of peak heat load detail(Cooling)

Room name:326 Arhiv st.radovi ] Floor: 4F Floor area: 23.4m2 Ceiling height: 3.8m Peak time in cooling:15:00  
Indoor temperature:26.0CDB , 50.0%RH Outdoor temperature:35.3CDB , 35.6%RH

<1> Load of window glass  
Material I / with blind-  
Upper:heat transfer load = temp.diff. \* OHTC \* area (!Area of heat transf. is contained sash area.  
Lower:solar heat load = area \* std.solar heat gain \* shading factor (!Area of solar heat gain is not contained sash area.  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW  
Shade  
Skylight

<2> Load of outer wall = effective temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW  
Shade  
(!Area of outer wall=length of outer wall  
\*floor height[ceiling height+height of ceiling adv attic]-window area)

<3> Load of roof = effective temp.diff. \* OHTC \* area  
Overhead room exist  
Flat roof 241 25.70 0.40 23.4  
Inclined roof

<4> Load of floor = temp.diff. \* OHTC \* area  
Earth floor  
With air layer  
Without air layer 122 (35.30-26.00)\*0.40 1.40 23.4  
Pilotis

<5> Load of inner wall = temp.diff. \* OHTC \* area  
Azimuth  
N  
E  
S  
W  
NE  
SE  
SW  
NW

<6> Load of underground wall = temp.diff. \* OHTC/unit ambient length \* ambient length  
(depth<=2.4m)  
  
Load of underground wall = temp.diff. \* OHTC \* area  
(depth>2.4m)

<7> Load of infiltration(SH) = infiltration vol.(m3/h) \* temp.diff. \* 0.33  
55 17.78 (35.30-26.00)  
  
Load of infiltration(LH) = infiltration vol.(m3/h) \* abs.humid.diff.(g/kg) \* 0.833  
33 17.78 (12.75-10.49)  
  
<8> Load of lighting = heat gain/W \* lighting consumption vol. \* operate  
Fluorescent lamp 543 1.160 468 1.00  
Incandescent lamp  
  
<9> Load of human body(SH) = SH of human body \* No of psns. \* operate  
112 56 2 1.00  
  
Load of human body(LH) = LH of human body \* No of psns. \* operate  
152 76 2 1.00  
  
<10> Load of equipments = heat gain from internal equip. \* operating rate  
  
<11> Fresh air load(SH) = F/A vol.(m3/h) \* temp.diff. \* 0.33 \* (1 - THEX)  
92 150.0 (35.30-26.00) 0.800  
  
Fresh air load(LH) = F/A vol.(m3/h) \* abs.humid.diff. \* 0.833 \* (1 - THEX)  
56 150.0 (12.75-10.49) 0.800  
  
<<Total>> Indoor heat load(W) = SH + LH  
1258 1073 185  
[ 1082] (kcal/h) [ 923] [ 159]  
  
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)  
1406 1258 92 56  
[ 1209] (kcal/h) [ 1082] [ 79] [ 48]

OHTC : Overall heat transfer coefficient  
SH : Sensible heat  
LH : Latent heat  
F/A : Fresh air  
THEX : Total heat exchange efficiency

## Table of peak heat load detail(Heating)

[Room name:326 Arhiv st.radovi ]		Floor: 4F	Floor area: 23.4m2	Ceiling height: 3.8m	Peak time in heating:18:00
Indoor temperature:20.0CDB		, 50.0%RH	Outdoor temperature:-6.0CDB	, 72.7%RH	
<1> Load of window glass = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area Azimuth N E S W NE SE SW NW Shade Skylight					
<2> Load of outer wall = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area Azimuth N E S W NE SE SW NW Shade (!Area of outer wall=length of outer wall*floor height[ceiling height+height of ceiling adv.attic.]-window area)					
<3> Load of roof = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area Overhead room exit Flat roof 300 1.00 1.00 (20.00+ 6.00) 6.00 0.40 23.4 Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area Earth floor With air layer 341 (20.00+ 6.00)*0.40 1.40 23.4 Without air layer Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area Azimuth N E S W NE SE SW NW					
<6> Load of underground wall = temp.diff. * OHTC * ambient length (depth<=2.4m) Load of underground wall = temp.diff. * OHTC * area (depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33 252 29.34 (20.00+ 6.00) Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833 137 29.34 ( 7.26- 1.65) (Humidifying vol.) (g/h) = infiltration vol. * abs.humid.diff. * 1.2 * safety factor 217 29.34 ( 7.26- 1.65) 1.10 !Infiltration vol. = No of ventilation * azimuth factor * room capacity 29.34 0.30 1.10 88.92					
<8> Load of lighting = -(heat gain/W * lighting consumption vol. * ope.rate * probable rate) Fluorescent lamp Incandescent lamp					
<9> Load of human body(SH) = -(SH of human body * No of psns * ope.rate * probable rate)					
<10> Load of equipments = -(heat gain from internal equip. * operating rate * probable rate)					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX) 193 150.0 (20.00+ 6.00) 0.850 Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833 * (1 - THEX) 105 150.0 ( 7.26- 1.65) 0.850 (Humidifying vol.) = F/A vol. * abs.humid.diff. * 1.2 * safety factor * (1 - THEX) 167 150.0 ( 7.26- 1.65) 1.10 0.850					
<<Total>> Indoor heat load(W) = SH + LH 893 893 0 [ 768] (kcal/h) [ 768] [ 0]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH) 1086 893 193 0 [ 934] (kcal/h) [ 768] [ 166] [ 0]					
!Indoor heat load & total heat load are not contained latent heat.					
Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air 384 217 167					
OHTC : Overall heat transfer coefficient SH : Sensible heat LH : Latent heat F/A : Fresh air THEX : Total heat exchange efficiency					

## Table of peak heat load detail(Cooling)

[Room name:327 Radna sala ]		Floor: 4F	Floor area: 21.4m2	Ceiling height: 3.8m	Peak time in cooling:15:00
Indoor temperature:26.0CDB		, 50.0%RH	Outdoor temperature:35.3CDB	, 35.6%RH	
<1> Load of window glass					
-Material I / with blind-					
Upper:heat transfer load = temp.diff. * OHTC * area (!Area of heat transf. is contained sash area.					
Lower:solar heat load = area * std.solar heat gain * shading factor (!Area of solar heat gain is not contained sash area.					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
Shade					
Skylight					
<2> Load of outer wall = effective temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
Shade					
(!Area of outer wall=length of outer wall					
*floor height[ceiling height+height of ceiling adv attic]-window area)					
<3> Load of roof = effective temp.diff. * OHTC * area					
Overhead room exist					
Flat roof	220	25.70	0.40	21.4	
Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area					
Earth floor					
With air layer	111	(35.30-26.00)*0.40	1.40	21.4	
Without air layer					
Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area					
Azimuth					
N					
E					
S					
W					
NE					
SE					
SW					
NW					
<6> Load of underground wall = temp.diff. * OHTC/unit ambient length * ambient length					
(depth<=2.4m)					
Load of underground wall = temp.diff. * OHTC * area					
(depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33					
50 16.26 (35.30-26.00)					
Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833					
31 16.26 (12.75-10.49)					
<8> Load of lighting = heat gain/W * lighting consumption vol. * ope.rate					
Fluorescent lamp	496	1.160	428	1.00	
Incandescent lamp					
<9> Load of human body(SH) = SH of human body * No of psns. * ope.rate					
672 56 12 1.00					
Load of human body(LH) = LH of human body * No of psns. * ope.rate					
912 76 12 1.00					
<10> Load of equipments = heat gain from internal equip. * operating rate					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX)					
307 500.0 (35.30-26.00) 0.800					
Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff. * 0.833 * (1 - THEX)					
188 500.0 (12.75-10.49) 0.800					
<<Total>> Indoor heat load(W) = SH + LH					
2492 1549 943					
[ 2143] (kcal/h) [ 1332] [ 811]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH)					
2987 2492 307 188					
[ 2569] (kcal/h) [ 2143] [ 264] [ 162]					
OHTC : Overall heat transfer coefficient					
SH : Sensible heat					
LH : Latent heat					
F/A : Fresh air					
THEX : Total heat exchange efficiency					



## Table of peak heat load detail(Heating)

[Room name:327 Radna sala ]		Floor: 4F	Floor area: 21.4m2	Ceiling height: 3.8m	Peak time in heating:18:00
Indoor temperature:20.0CDB		, 50.0%RH	Outdoor temperature:-6.0CDB	, 72.7%RH	
<1> Load of window glass = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area Azimuth N E S W NE SE SW NW Shade Skylight					
<2> Load of outer wall = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area Azimuth N E S W NE SE SW NW Shade (!Area of outer wall=length of outer wall*floor height[ceiling height+height of ceiling adv.attic.]-window area)					
<3> Load of roof = azimuth factor * increasing factor of ceiling height * (temp.diff. + radiant cooling effect) * OHTC * area Overhead room exit Flat roof 274 1.00 1.00 (20.00+ 6.00) 6.00 0.40 21.4 Inclined roof					
<4> Load of floor = temp.diff. * OHTC * area Earth floor With air layer 312 (20.00+ 6.00)*0.40 1.40 21.4 Without air layer Pilotis					
<5> Load of inner wall = temp.diff. * OHTC * area Azimuth N E S W NE SE SW NW					
<6> Load of underground wall = temp.diff. * OHTC * ambient length (depth<=2.4m) Load of underground wall = temp.diff. * OHTC * area (depth>2.4m)					
<7> Load of infiltration(SH) = infiltration vol.(m3/h) * temp.diff. * 0.33 230 26.84 (20.00+ 6.00) Load of infiltration(LH) = infiltration vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833 125 26.84 ( 7.26- 1.65) (Humidifying vol.) (g/h) = infiltration vol. * abs.humid.diff. * 1.2 * safety factor 199 26.84 ( 7.26- 1.65) 1.10 !Infiltration vol. = No of ventilation * azimuth factor * room capacity 26.84 0.30 1.10 81.32					
<8> Load of lighting = -(heat gain/W * lighting consumption vol. * ope.rate * probable rate) Fluorescent lamp Incandescent lamp					
<9> Load of human body(SH) = -(SH of human body * No of psns * ope.rate * probable rate)					
<10> Load of equipments = -(heat gain from internal equip. * operating rate * probable rate)					
<11> Fresh air load(SH) = F/A vol.(m3/h) * temp.diff. * 0.33 * (1 - THEX) 644 500.0 (20.00+ 6.00) 0.850 Fresh air load(LH) = F/A vol.(m3/h) * abs.humid.diff.(g/kg) * 0.833 * (1 - THEX) 350 500.0 ( 7.26- 1.65) 0.850 (Humidifying vol.) = F/A vol. * abs.humid.diff. * 1.2 * safety factor * (1 - THEX) 555 500.0 ( 7.26- 1.65) 1.10 0.850					
<<Total>> Indoor heat load(W) = SH + LH 816 816 0 [ 702] (kcal/h) [ 702] [ 0]					
Total heat load(W) = indoor heat load + fresh air load(SH) + fresh air load(LH) 1460 816 644 0 [ 1256] (kcal/h) [ 702] [ 554] [ 0] !Indoor heat load & total heat load are not contained latent heat. Humidifying vol.(g/h) = humidification of infiltration + humidification of outdoor air 754 199 555					
OHTC : Overall heat transfer coefficient SH : Sensible heat LH : Latent heat F/A : Fresh air THEX : Total heat exchange efficiency					

## 5.2. KOLIČINE VAZDUHA ZA VENTILACIJU

OBJEKAT: ARHITEKTONSKI FAKULTET PODGORICA

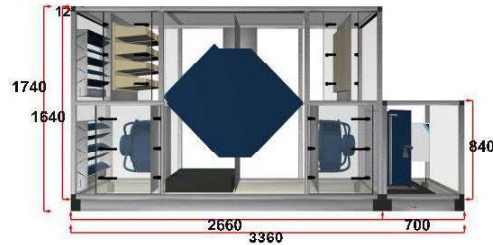
Količine svježeg vazduha

PODACI O PROSTORIJAMA					ASHRAE 62.1 (m³/h)					EN 15251 (m³/h)					USVOJENO (m³/h)	
sistem/etaža	br. pr.	naziv prostorije	A (m²)	broj ljudi	l/s*m²	l/s*č	po površini	po br. ljudi	ukupno	l/s*m²	l/s*č	po površini	po br. ljudi	ukupno	ubacivanje	izvlačenje
SISTEM 1 - KAFE/STUDENTSKI KLUB																
SUTEREN	015	KAFE/STUDENTSKI KLUB	103,22	110	0,3	2,5	111	990	1101	1	10	372	3960	4332	4400	4400
SISTEM 2 – KANCELARIJE II SPRAT																
II SPRAT	306	Sala osoblje	49	32	0,3	2,5	53	288	341	0,7	7	123	806	929	1000	1000
II SPRAT	325	Trpezarija	23,3	12	0,3	2,5	25	108	133	0,7	8	59	346	405	450	500
II SPRAT	326	Arhiv	23,4	2	0,3	2,5	25	18	43	0,7	7	59	50	109	100	150
II SPRAT	327	Radna sala	21,4	12	0,3	2,5	23	108	131	0,7	8	54	346	400	450	500
UKUPNO:															2000	2150
SISTEM 3 – AMFITEATAR																
II SPRAT	308	AMFITEATAR	215,2	159	0,3	2,5	232	1431	1663	0,4	10	310	5724	6034	6310	6310

## **5.3 IZBOR KLIMA KOMORA**



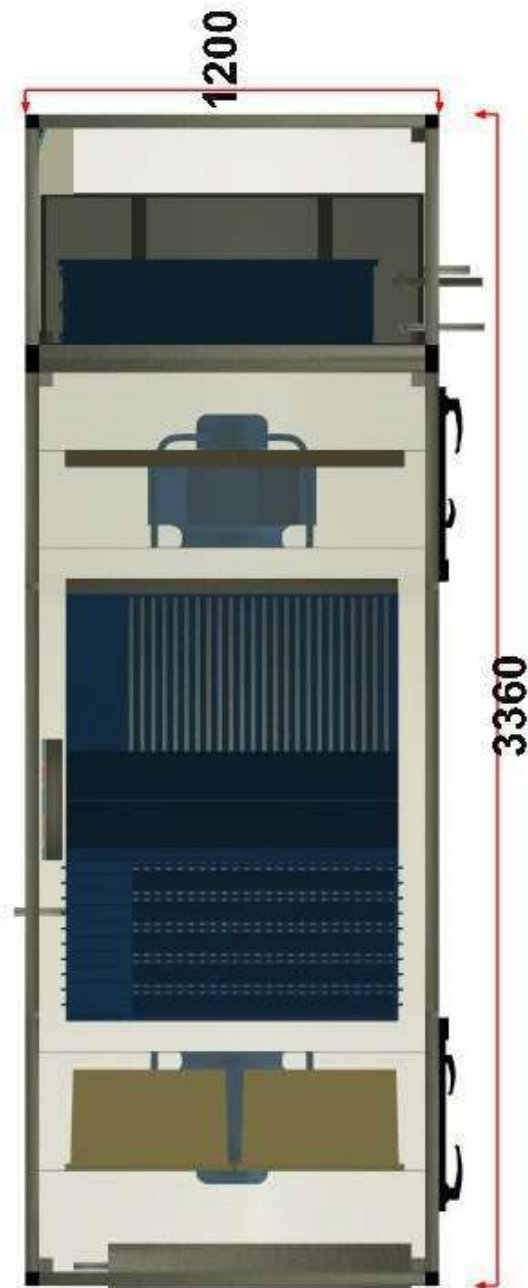
**Project** Arhitektonski fakultet Podgorica  
**Unit** SISTEM\_2\_KK\_STUDENSKI\_KLUB

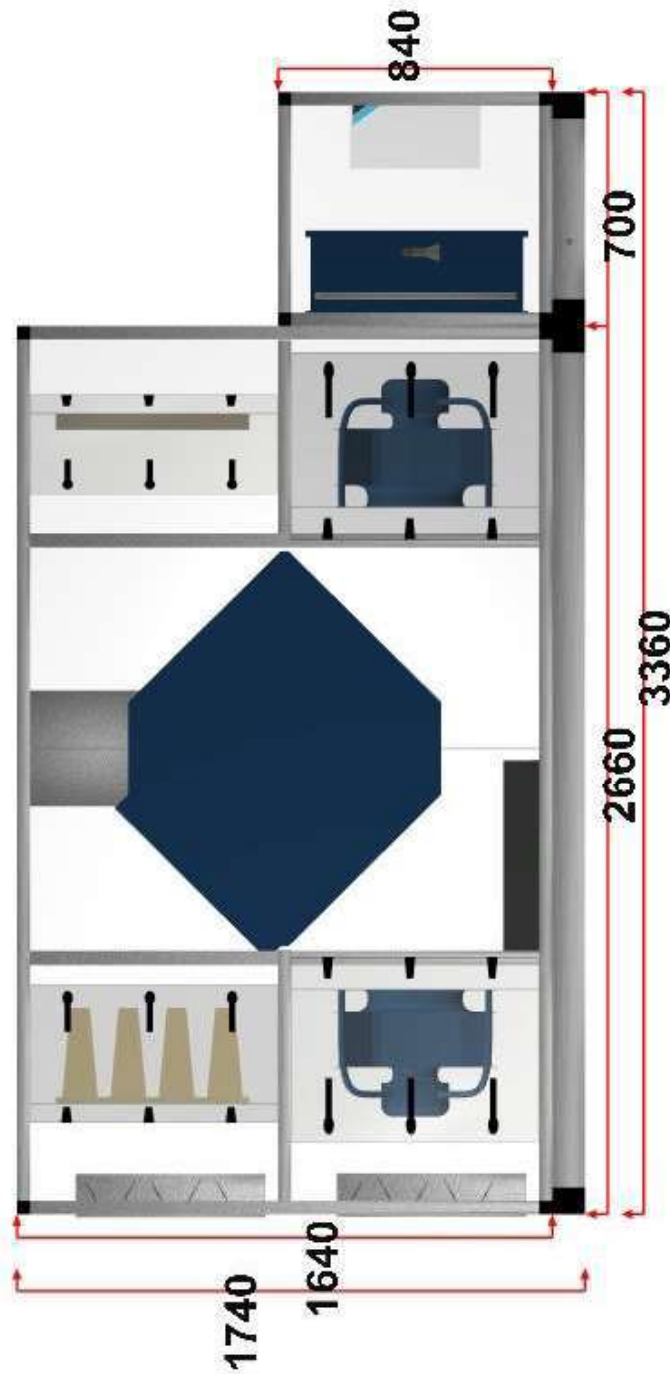


## Unit Data

Range / Series	D-AHU MODULAR_P
Model	SIZE 4
Panel • Insulation	42 mm • Foam
Model Box Ref.	Energy ThermiC° F2
Panel Inner Skin	Aluzinc 0.5 mm
Panel Outer Skin	Precoated 0.7 mm
Profile	Aluminium Anodized
	Thermal Break
AHU Base	100 mm Aluminium
Supply Width • Height	1200 mm • 840 mm
Return Width • Height	1200 mm • 840 mm
Length Overall	3360 mm
Weight	700 Kg
Connection Side	Left
Supply Air Flow	4400 m <sup>3</sup> /h • 1.22 m <sup>3</sup> /s
External Pressure Drop	200 Pa
Return Air Flow	4400 m <sup>3</sup> /h • 1.22 m <sup>3</sup> /s
External Pressure Drop	200 Pa
Electrical Connection	400V/3Ph/50Hz
Air Density	1.2 Kg/m <sup>3</sup>
Altitude	44 m a.s.l.
Specific fan power efficiency rating:	
SFPv (clean filters)	1414 W/(m <sup>3</sup> /s)
SFPe (medium filters)	1605 W/(m <sup>3</sup> /s)
ERP Compliant	ERP 2018







## 1) Damper Supply

Pressure Drop	7 Pa
Material	Aluminium
Mounting	Internal • Left
Dimensions (HxW)	580x880 mm
Torque	4 Nm

## 2) Filter Supply

Mounting	Slide
Air Velocity	2.11 m/s
Pressure Drop Design	Medium
Filter Class	F7 ePM1 50%
Filter Energy Classification	A
Filter Name	VariCEL VXL-E
Material	Fiber Glass
Dimensions	2x(490x592x290)
Clean Pressure Drop	53 Pa
Medium Pressure Drop	103 Pa
Dirty Pressure Drop	153 Pa

## 3) Recuperator Heat Cube Supply

Part Number	PCF-K 55
Material	Aluminium
Side	648 mm
Dry Efficiency (Eurovent)	85.6 %
Energy Class (EN13053)	H1 • 77.83 %
ByPass	Standard ByPass

### WINTER

Power	35.6 kW
Efficiency	95.9 %
<b>Supply</b>	
Flow Rate	4400 m <sup>3</sup> /h
Actual Pressure Drop	116 Pa
Temp. Dry Bulb Outdoor • Supply	-6 °C • 20.9 °C
Relative Humidity Outdoor • Supply	90 % • 14 %
Temp. Wet Bulb Outdoor • Supply	-6.4 °C • 8.8 °C

### Return

Flow Rate	4400 m <sup>3</sup> /h
Actual Pressure Drop	137 Pa
Temp. Dry Bulb Extract • Exhaust	22 °C • 6.1 °C
Relative Humidity Extract • Exhaust	50 % • 100 %
Temp. Wet Bulb Extract • Exhaust	15.5 °C • 6.1 °C

### SUMMER

Power	12.7 kW
-------	---------

Efficiency	73.8 %
<b>Supply</b>	
Flow Rate	4400 m <sup>3</sup> /h
Actual Pressure Drop	148 Pa
Temp. Dry Bulb Outdoor • Supply	37 °C • 28.9 °C
Relative Humidity Outdoor • Supply	28 % • 44 %
Temp. Wet Bulb Outdoor • Supply	22.5 °C • 20.1 °C
<b>Return</b>	
Flow Rate	4400 m <sup>3</sup> /h
Actual Pressure Drop	140 Pa
Temp. Dry Bulb Extract • Exhaust	26 °C • 34.8 °C
Relative Humidity Extract • Exhaust	50 % • 30 %
Temp. Wet Bulb Extract • Exhaust	18.7 °C • 21.5 °C

*Assumed that the system effect was considered in the design.*

#### 4) Fan Supply

Model	K3G355PH4905
Type	EC Centrifugal Fan
Material	Aluminium
Quantity	1x(Single Fan)
External Static Pressure	200 Pa
Internal Static Pressure	264 Pa
Total Static Pressure	464 Pa
Dynamic Pressure	53 Pa
Flow Design	4400 m <sup>3</sup> /h
Rotation Speed Work • Max	2312 RPM • 2870 RPM
Efficiency (Reg327/2011)	68.8 %
Efficiency	63.8 %
Electrical Power Input	0.99 kW
Power Class • PMREF (EN13053)	P1 • 1.32 kW
SFPv Class • SFPv (EN13053)	SFP1 • 707 W/(m <sup>3</sup> /s)

##### Motor Data

Efficiency Class	IE4
Power • Nominal Current	1.9 kW • 3 A
Electrical Connection	3Ph+N-380-480V

*Fan system effect is taken into account in the fan performances*

#### 5) Coil Cooling • Heating DX Supply

##### Geometry

Model	1022A2603090025EO109
Geometry • Rows	P22 • 3
Frame	Galvanized
Tube Material • Thickness	Copper • 0.35 mm
Fin Material • Space	Al 0.1 mm • 2.5 mm
Connections (Diam) • Type • Side	16 mm • Braised • Right
Circuit Number	1



Sensible Capacity	19.8 kW
Total Capacity[B]*	27.4 kW

#### Cooling Air Side

Air Flow • Velocity	4400 m <sup>3</sup> /h • 2.09 m/s
Temp. Dry Bulb In • Out	28.9 °C • 16 °C
Temp. Wet Bulb In • Out	20.1 °C • 13.9 °C
Relative Humidity In • Out	44.3 % • 79 %
Pressure Drop Dry • Wet	29Pa • 38 Pa

#### Cooling Fluid Side

Fluid	R410A
Evaporating Temperature	6 °C
Fluid Volume	4.5 dm <sup>3</sup>
1[D]* x EKEXV250[A]*	Mounted

#### Heating Air Side

Max Power[C]*(based on maximum condensing unit)	22 kW
Temp. Dry Bulb In • Out	20.9 °C • 35.3 °C

\* For VRV Xpress Input [A: EKEXV250] , [B: 27.4 kW] , [C: 22 kW] , [D: 1]

Calculated in Wet Condition

## 6) Filter Return

Mounting	Slide
Air Velocity	2.11 m/s
Pressure Drop Design	Medium
Filter Class	M5 ePM10 55%
Filter Energy Classification	E
Filter Name	Ecopleat Green
Material	Synthetic
Dimensions	2x(490x592x48)
Clean Pressure Drop	58 Pa
Medium Pressure Drop	108 Pa
Dirty Pressure Drop	158 Pa

## 7) Fan Return

Model	K3G355PH4905
Type	EC Centrifugal Fan
Material	Aluminium
Quantity	1x(Single Fan)
External Static Pressure	200 Pa
Internal Static Pressure	252 Pa
Total Static Pressure	452 Pa
Dynamic Pressure	53 Pa
Flow Design	4400 m <sup>3</sup> /h
Rotation Speed Work • Max	2299 RPM • 2870 RPM

Efficiency (Reg327/2011)	68.8 %
Efficiency	63.6 %
Electrical Power Input	0.97 kW
Power Class • PMREF (EN13053)	P1 • 1.29 kW
SFPv Class • SFPv (EN13053)	SFP1 • 707 W/(m <sup>3</sup> /s)

#### Motor Data

Efficiency Class	IE4
Power • Nominal Current	1.9 kW • 3 A
Electrical Connection	3Ph+N-380-480V

*Fan system effect is taken into account in the fan performances*

## 8) Damper Return

Pressure Drop	7 Pa
Material	Aluminium
Mounting	Internal • Right
Dimensions (HxW)	580x880 mm
Torque	4 Nm

## Section List

Num.	Height (mm)	Width (mm)	Length (mm)	Weight (Kg)	Transportable
1	1740	1200	2660	604	Container or Truck
2	940	1200	700	96	Container or Truck

## Options List

---

### Unit Options

Rain Hood Fresh Air  
Rain Hood Exhaust Air  
Flat Roof  
CO2  
Remote Interface  
Constant Airflow - Ambient

## Sound Report

### Supply

Sound Power (dB)	63Hz	125Hz	250Hz	500Hz	1kHz	2kHz	4kHz	8kHz	AVG dB (A)
Fan Inlet	60	76	77	73	68	70	73	64	78
Fan Outlet	62	76	76	76	76	76	77	68	83
Unit Inlet	54	70	71	67	59	58	53	44	68
Unit Outlet	58	71	71	71	70	68	65	56	75
Airborne	54	67	60	58	58	56	57	34	64

### Return

Sound Power (dB)	63Hz	125Hz	250Hz	500Hz	1kHz	2kHz	4kHz	8kHz	AVG dB (A)
Fan Inlet	60	76	77	73	68	70	73	64	78
Fan Outlet	62	76	76	76	76	75	77	68	82
Unit Inlet	58	75	76	72	65	66	65	56	74
Unit Outlet	62	76	76	76	76	75	77	68	82
Airborne	53	67	60	58	58	55	57	34	64

## NRVU - Regulation (EU) No 1253/2014

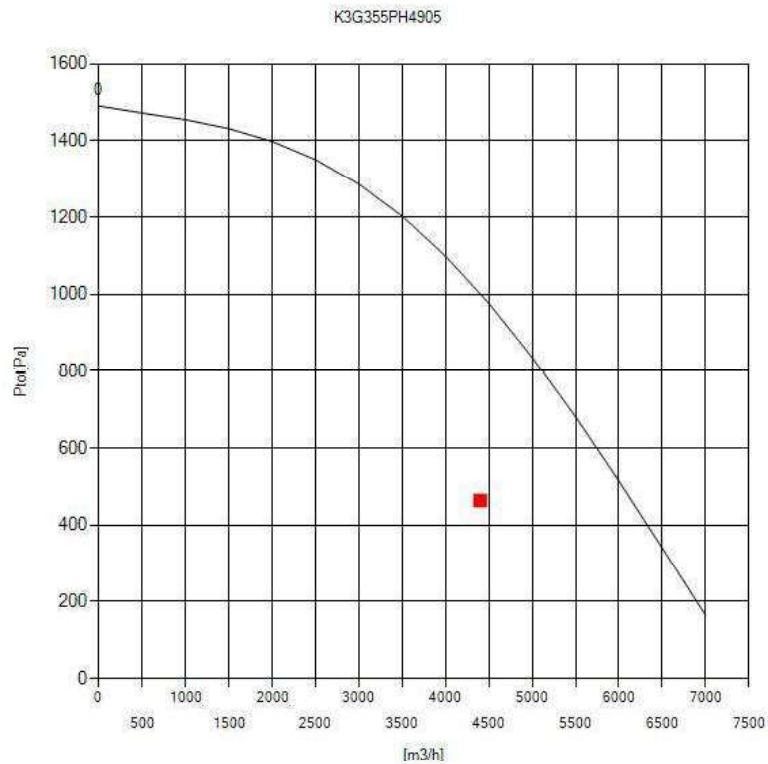
Manufacturer's Name	Daikin Applied Europe S.p.a.
Serial Number	331011
Typology (NRVU, UVU or BVU)*	NRVU BVU
Drive Type	Inverter (included on the electronic fan )
HRS Type	Other
HRS Thermal Efficiency (EN308)	82.8 %
Nominal NRVU Flow Rate	
<i>Supply</i>	1.22 m <sup>3</sup> /s
<i>Return</i>	1.22 m <sup>3</sup> /s
Effective Electric Power Input	
<i>Supply</i>	1.98 kW
SFP Internal	572 W/(m <sup>3</sup> /s)
Face Velocity at Flow Rate Design	
<i>Supply</i>	1.4 m/s
<i>Return</i>	1.4 m/s
Nominal Internal Pressure Drop	
<i>Supply</i>	169 Pa
<i>Return</i>	195 Pa
Nominal External Pressure Drop	
<i>Supply</i>	200 Pa
<i>Return</i>	200 Pa
Efficiency (Reg327/2011)	
<i>Supply</i>	69 %
<i>Return</i>	69 %
External Leakage (RU) +400Pa • - 400Pa	1.02 % • 0.51 %
Maximum Internal Leakage	1.5 %
Summer Outdoor Conditions	37 °C • 28 %
Winter Outdoor Conditions	-6 °C • 90 %
Filter Energy Classification	A -
Filter Service Warning**	Displayed on HMI Controller
Sound Power Level (LWA)	Please refer to Selection Software
Pre-/Dis-assembly Instructions	<a href="http://www.daikinapplied.eu/en/index/page/download">http://www.daikinapplied.eu/en/index/page/download</a>

\* In accordance with Commission Regulation (EU) No 1253/2014 of July 2014

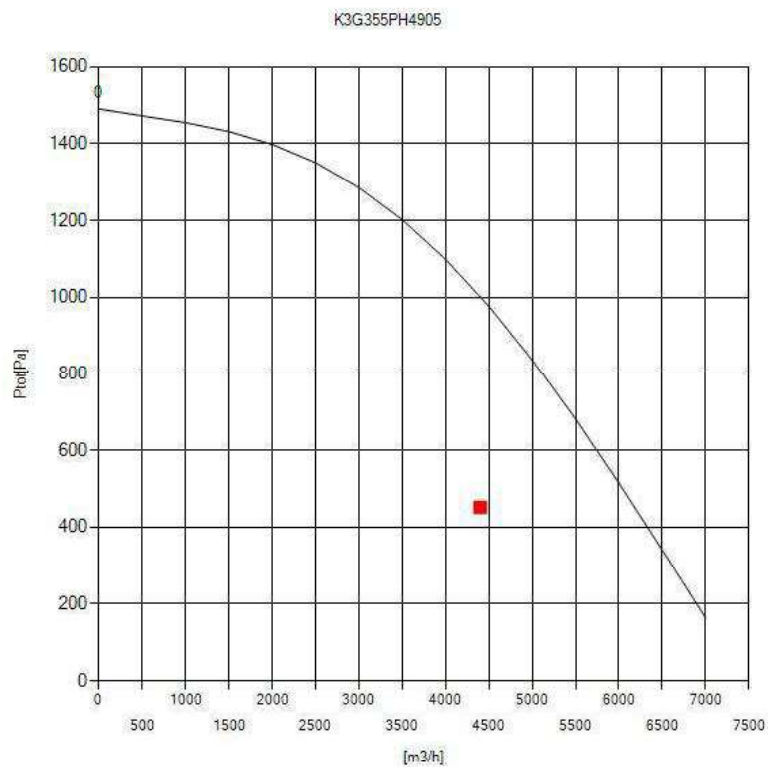
\*\* Clean/replace Filter(s) when maximum pressure drop is reached or when warning is displayed on HMI controller

## Fan Curves Diagrams

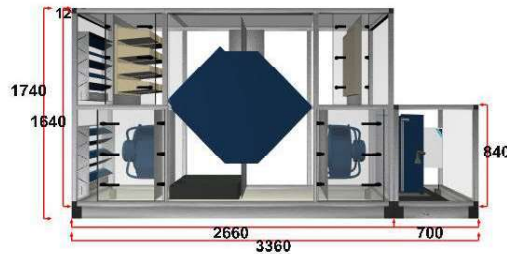
### 4) Fan Supply



### 7) Fan Return



**Project** Arhitektonski fakultet Podgorica  
**Unit** SISTEM\_2\_KK\_STUDENSKI\_KLUB



## Unit Data

Range / Series	MODULAR_P
Model	840 X 1200
Panel	SP 45
Insulation	Foam
Panel Inner Skin	Aluzinc 0.5 mm
Panel Outer Skin	Precoated 0.7 mm
Profile	Aluminium Anodized Thermal Break

## Prices

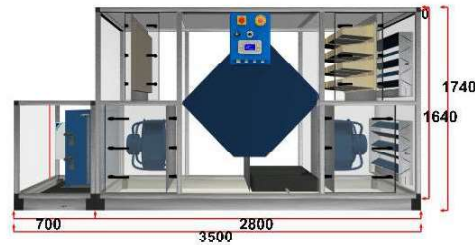
Unit	28489 €
Options	2120 €

**Total (List) 30609 €**

Standard terms and Conditions Validity 30 day Ex Work (ALL AHU's individual sections shall be checked carefully by the customer to assess whether a standard truck/container or a special truck/container might be required. An additional 150 mm dimension shall be added to the AHU's reported dimensions. The same additional 150mm is to be added on the overall height to consider Pallet height for transportation assessment)



**Project** Arhitektonski fakultet Podgorica  
**Unit** SISTEM\_9\_KK\_AMFITEATAR

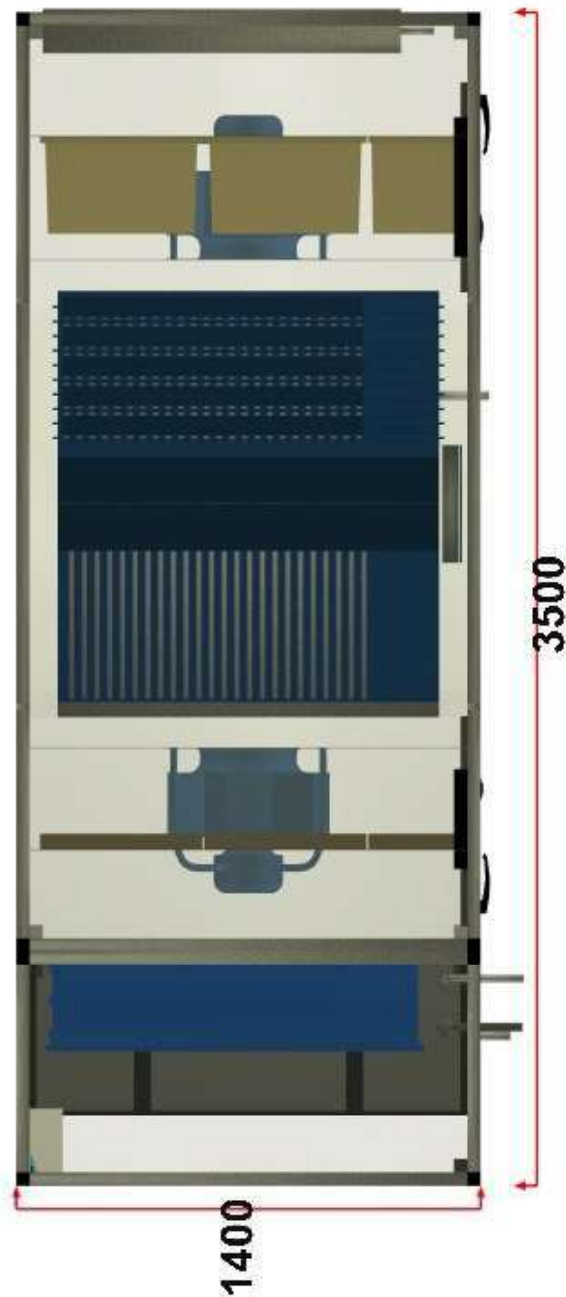


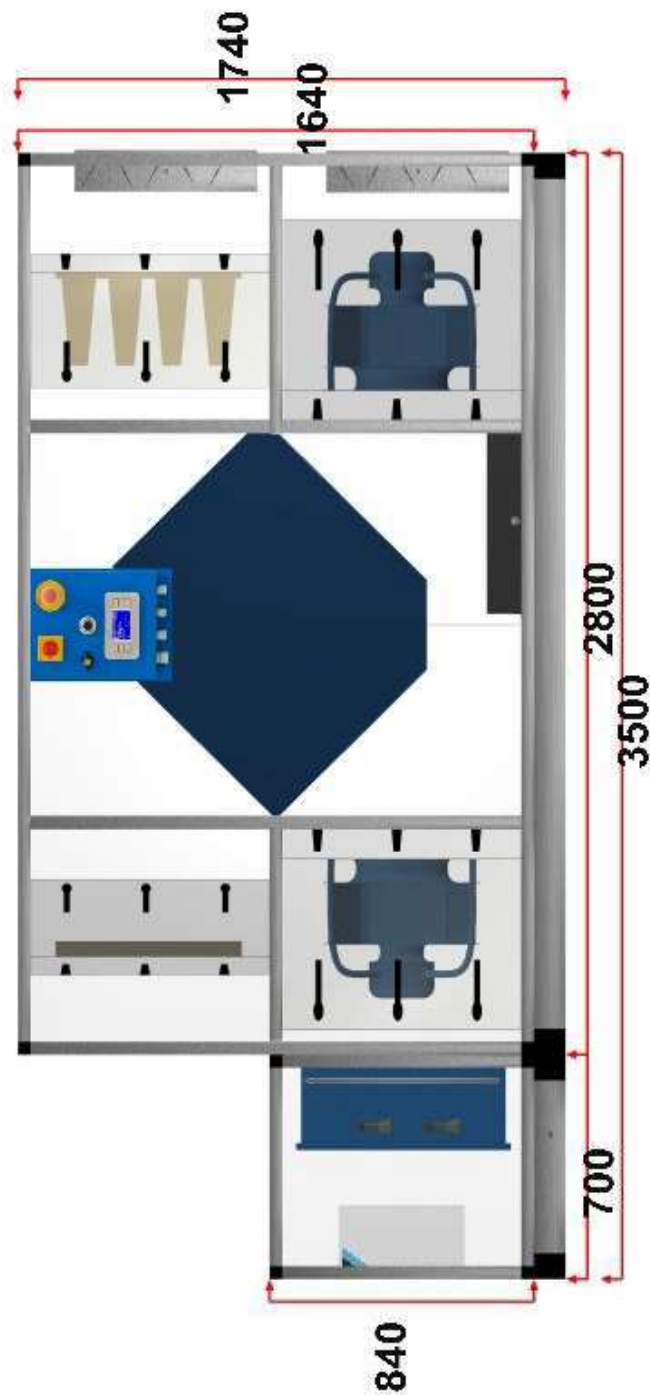
## Unit Data

Range / Series	D-AHU MODULAR_P
Model	SIZE 5
Panel • Insulation	42 mm • Foam
Model Box Ref.	Energy ThermiC° F2
Panel Inner Skin	Aluzinc 0.5 mm
Panel Outer Skin	Precoated 0.7 mm
Profile	Aluminium Anodized Thermal Break
AHU Base	100 mm Aluminium
Supply Width • Height	1400 mm • 840 mm
Return Width • Height	1400 mm • 840 mm
Length Overall	3500 mm
Weight	899 Kg
Connection Side	Left
Supply Air Flow	6310 m <sup>3</sup> /h • 1.75 m <sup>3</sup> /s
External Pressure Drop	200 Pa
Return Air Flow	6310 m <sup>3</sup> /h • 1.75 m <sup>3</sup> /s
External Pressure Drop	200 Pa
Electrical Connection	400V/3Ph/50Hz
Air Density	1.2 Kg/m <sup>3</sup>
Altitude	44 m a.s.l.
Specific fan power efficiency rating:	
SFPv (clean filters)	1512 W/(m <sup>3</sup> /s)
SFPe (medium filters)	1701 W/(m <sup>3</sup> /s)
ERP Compliant	ERP 2018









## 1) Damper Supply

Pressure Drop	10 Pa
Material	Aluminium
Mounting	Internal • Left
Dimensions (HxW)	580x1080 mm
Torque	4 Nm

## 2) Filter Supply

Mounting	Slide
Air Velocity	2.34 m/s
Pressure Drop Design	Medium
Filter Class	F7 ePM1 50%
Filter Energy Classification	A
Filter Name	VariCEL VXL-E
Material	Fiber Glass
Dimensions	2x(490x592x290) 1x(287x592x290)
Clean Pressure Drop	58 Pa
Medium Pressure Drop	108 Pa
Dirty Pressure Drop	158 Pa

## 3) Recuperator Heat Cube Supply

Part Number	PCF-K 55
Material	Aluminium
Side	648 mm
Dry Efficiency (Eurovent)	84.6 %
Energy Class (EN13053)	H1 • 76.99 %
ByPass	Standard ByPass

### WINTER

Power	50.7 kW
Efficiency	95.2 %
<b>Supply</b>	
Flow Rate	6310 m <sup>3</sup> /h
Actual Pressure Drop	155 Pa
Temp. Dry Bulb Outdoor • Supply	-6 °C • 20.7 °C
Relative Humidity Outdoor • Supply	90 % • 14 %
Temp. Wet Bulb Outdoor • Supply	-6.4 °C • 8.7 °C

### Return

Flow Rate	6310 m <sup>3</sup> /h
Actual Pressure Drop	183 Pa
Temp. Dry Bulb Extract • Exhaust	22 °C • 6.1 °C
Relative Humidity Extract • Exhaust	50 % • 100 %
Temp. Wet Bulb Extract • Exhaust	15.5 °C • 6.1 °C

### SUMMER

Power	21.1 kW
Efficiency	72.3 %
<b>Supply</b>	
Flow Rate	6310 m <sup>3</sup> /h
Actual Pressure Drop	198 Pa
Temp. Dry Bulb Outdoor • Supply	37 °C • 27.6 °C
Relative Humidity Outdoor • Supply	28 % • 48 %
Temp. Wet Bulb Outdoor • Supply	22.5 °C • 19.7 °C
<b>Return</b>	
Flow Rate	6310 m <sup>3</sup> /h
Actual Pressure Drop	185 Pa
Temp. Dry Bulb Extract • Exhaust	24 °C • 34.3 °C
Relative Humidity Extract • Exhaust	50 % • 28 %
Temp. Wet Bulb Extract • Exhaust	17.1 °C • 20.5 °C

*Assumed that the system effect was considered in the design.*

#### 4) Fan Supply

Model	K3G400PI9205
Type	EC Centrifugal Fan
Material	Aluminium
Quantity	1x(Single Fan)
External Static Pressure	200 Pa
Internal Static Pressure	339 Pa
Total Static Pressure	539 Pa
Dynamic Pressure	61 Pa
Flow Design	6310 m <sup>3</sup> /h
Rotation Speed Work • Max	2111 RPM • 2450 RPM
Efficiency (Reg327/2011)	70 %
Efficiency	69 %
Electrical Power Input	1.53 kW
Power Class • PMREF (EN13053)	P1 • 2.1 kW
SFPv Class • SFPv (EN13053)	SFP1 • 764 W/(m <sup>3</sup> /s)

#### Motor Data

Efficiency Class	IE4
Power • Nominal Current	2.5 kW • 3.8 A
Electrical Connection	3Ph+N-380-480V

*Fan system effect is taken into account in the fan performances*

#### 5) Coil Cooling • Heating DX Supply

##### Geometry

Model	1022A2604110025EO2(6+7)
Geometry • Rows	P22 • 4
Frame	Galvanized
Tube Material • Thickness	Copper • 0.35 mm
Fin Material • Space	Al 0.1 mm • 2.5 mm
Connections (Diam) • Type • Side	16 mm • Braised • Left

Circuit Number	2
Sensible Capacity	30 kW
Total Capacity[B]*	43 kW

#### Cooling Air Side

Air Flow • Velocity	6310 m <sup>3</sup> /h • 2.45 m/s
Temp. Dry Bulb In • Out	27.6 °C • 14 °C
Temp. Wet Bulb In • Out	19.7 °C • 12.7 °C
Relative Humidity In • Out	47.7 % • 86 %
Pressure Drop Dry • Wet	51Pa • 66 Pa

#### Cooling Fluid Side

Fluid	R410A
Evaporating Temperature	6 °C
Fluid Volume	2 x 3.9 dm <sup>3</sup>
2[D]* x EKEXV200[A]*	Mounted

#### Heating Air Side

Max Power[C]*(based on maximum condensing unit)	35.4 kW
Temp. Dry Bulb In • Out	20.7 °C • 36.9 °C

\* For VRV Xpress Input [A: EKEXV200] , [B: 43 kW] , [C: 35.4 kW] , [D: 2]

*Calculated in Wet Condition*

## 6) Filter Return

Mounting	Slide
Air Velocity	2.34 m/s
Pressure Drop Design	Medium
Filter Class	M5 ePM10 55%
Filter Energy Classification	E
Filter Name	Ecopleat Green
Material	Synthetic
Dimensions	2x(490x592x48) 1x(287x592x48)
Clean Pressure Drop	64 Pa
Medium Pressure Drop	114 Pa
Dirty Pressure Drop	164 Pa

## 7) Fan Return

Model	K3G400PI9205
Type	EC Centrifugal Fan
Material	Aluminium
Quantity	1x(Single Fan)
External Static Pressure	200 Pa
Internal Static Pressure	307 Pa
Total Static Pressure	507 Pa
Dynamic Pressure	61 Pa

Flow Design	6310 m <sup>3</sup> /h
Rotation Speed Work • Max	2081 RPM • 2450 RPM
Efficiency (Reg327/2011)	70 %
Efficiency	68.4 %
Electrical Power Input	1.46 kW
Power Class • PMREF (EN13053)	P1 • 1.99 kW
SFPv Class • SFPv (EN13053)	SFP1 • 748 W/(m <sup>3</sup> /s)

#### Motor Data

Efficiency Class	IE4
Power • Nominal Current	2.5 kW • 3.8 A
Electrical Connection	3Ph+N-380-480V

*Fan system effect is taken into account in the fan performances*

## 8) Damper Return

Pressure Drop	10 Pa
Material	Aluminium
Mounting	Internal • Right
Dimensions (HxW)	580x1080 mm
Torque	4 Nm

## Section List

Num.	Height (mm)	Width (mm)	Length (mm)	Weight (Kg)	Transportable
1	1740	1400	2800	785	Container or Truck
2	940	1400	700	114	Container or Truck

## Options List

---

### Unit Options

Rain Hood Fresh Air  
Rain Hood Exhaust Air  
Flat Roof  
CO2  
Remote Interface  
Constant Airflow - Ambient

## Sound Report

### Supply

Sound Power (dB)	63Hz	125Hz	250Hz	500Hz	1kHz	2kHz	4kHz	8kHz	AVG dB (A)
Fan Inlet	62	80	78	74	73	70	75	67	80
Fan Outlet	64	82	78	78	80	75	78	70	84
Unit Inlet	56	74	72	68	64	58	55	47	70
Unit Outlet	59	76	74	73	74	67	66	58	77
Airborne	55	72	62	60	62	55	58	36	66

### Return

Sound Power (dB)	63Hz	125Hz	250Hz	500Hz	1kHz	2kHz	4kHz	8kHz	AVG dB (A)
Fan Inlet	61	81	78	73	73	69	75	67	80
Fan Outlet	63	82	78	77	80	75	77	70	84
Unit Inlet	60	80	77	72	70	65	67	59	76
Unit Outlet	63	82	78	77	80	75	77	70	84
Airborne	54	73	62	59	62	55	57	36	66



## NRVU - Regulation (EU) No 1253/2014

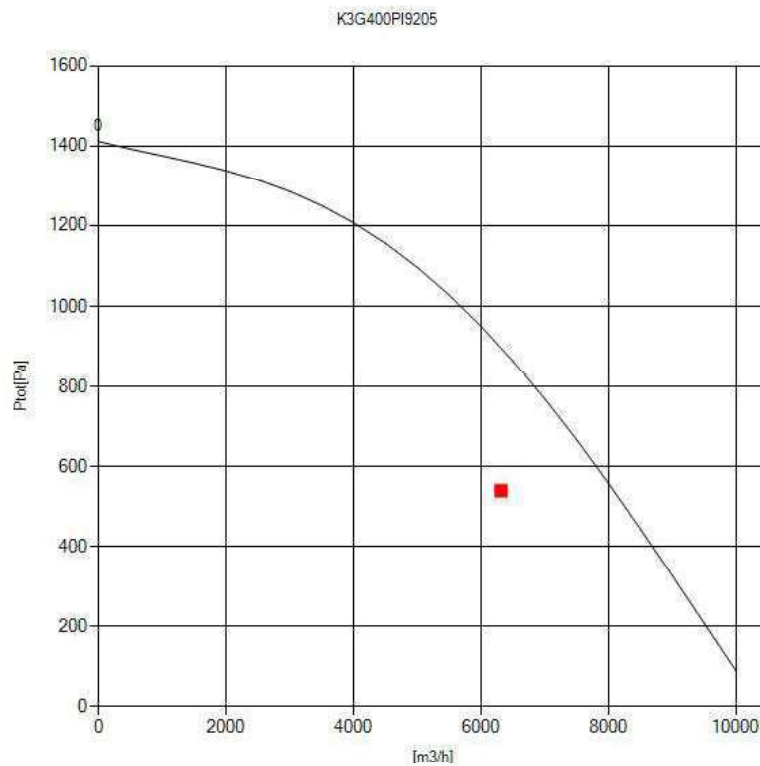
Manufacturer's Name	Daikin Applied Europe S.p.a.
Serial Number	330959
Typology (NRVU, UVU or BVU)*	NRVU BVU
Drive Type	Inverter (included on the electronic fan )
HRS Type	Other
HRS Thermal Efficiency (EN308)	81.9 %
Nominal NRVU Flow Rate	
<i>Supply</i>	1.75 m <sup>3</sup> /s
<i>Return</i>	1.75 m <sup>3</sup> /s
Effective Electric Power Input	
<i>Supply</i>	3.01 kW
SFP Internal	673 W/(m <sup>3</sup> /s)
Face Velocity at Flow Rate Design	
<i>Supply</i>	1.7 m/s
<i>Return</i>	1.7 m/s
Nominal Internal Pressure Drop	
<i>Supply</i>	213 Pa
<i>Return</i>	247 Pa
Nominal External Pressure Drop	
<i>Supply</i>	200 Pa
<i>Return</i>	200 Pa
Efficiency (Reg327/2011)	
<i>Supply</i>	70 %
<i>Return</i>	70 %
External Leakage (RU) +400Pa • - 400Pa	0.82 % • 0.41 %
Maximum Internal Leakage	1.5 %
Summer Outdoor Conditions	37 °C • 28 %
Winter Outdoor Conditions	-6 °C • 90 %
Filter Energy Classification	A -
Filter Service Warning**	Displayed on HMI Controller
Sound Power Level (LWA)	Please refer to Selection Software
Pre-/Dis-assembly Instructions	<a href="http://www.daikinapplied.eu/en/index/page/download">http://www.daikinapplied.eu/en/index/page/download</a>

\* In accordance with Commission Regulation (EU) No 1253/2014 of July 2014

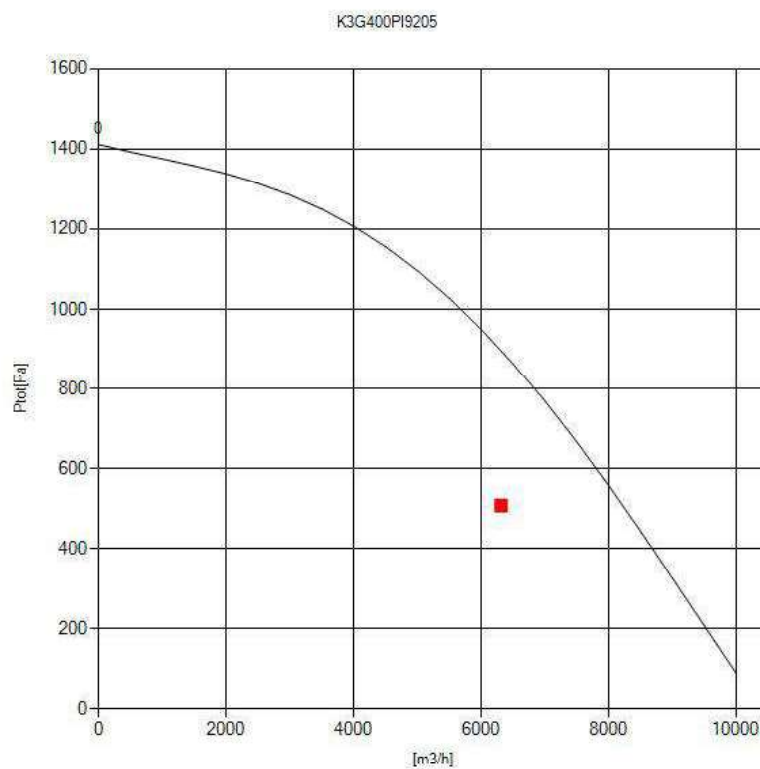
\*\* Clean/replace Filter(s) when maximum pressure drop is reached or when warning is displayed on HMI controller

## Fan Curves Diagrams

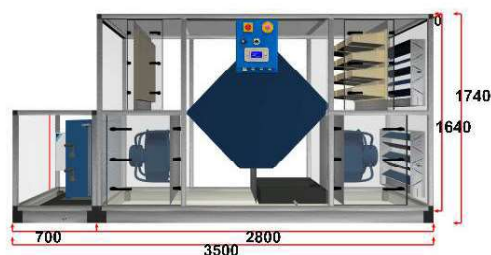
### 4) Fan Supply



### 7) Fan Return



**Project** Arhitektonski fakultet Podgorica  
**Unit** SISTEM\_9\_KK\_AMFITEATAR



## Unit Data

Range / Series	MODULAR_P
Model	840 X 1400
Panel	SP 45
Insulation	Foam
Panel Inner Skin	Aluzinc 0.5 mm
Panel Outer Skin	Precoated 0.7 mm
Profile	Aluminium Anodized Thermal Break

## Prices

Unit	32713 €
Options	3142 €
<b>Total (List)</b>	<b>35855 €</b>

Standard terms and Conditions Validity 30 day Ex Work (ALL AHU's individual sections shall be checked carefully by the customer to assess whether a standard truck/container or a special truck/container might be required. An additional 150 mm dimension shall be added to the AHU's reported dimensions. The same additional 150mm is to be added on the overall height to consider Pallet height for transportation assessment)

## **5.4 IZBOR REŠETKI ZA VENTILACIJU**



# AD - Grilles

Project: Untitled project

01-07-2019



## Requirements:

Air volume	qv	1100 m <sup>3</sup> /h
Room attenuation	Dr	4 dB
Length, L		1000
Height, H		100

## Results:

Total pressure loss	$\Delta p_t$	16 Pa
Sound power level	L <sub>wA</sub>	47 dB(A)
Sound pressure level	L <sub>pA</sub>	43 dB(A)

## AD - Grilles

AD is an adjustable single or double deflection grille made of aluminium. With adjustable blades, the grille is very useful for air supply and can be adapted to the required throw and air spread pattern.

The grille is available with several mounting options and can be delivered with mounting frame, opposed blade damper and plenum box accessories.

## Order code

AD-11-HMD-1000-100

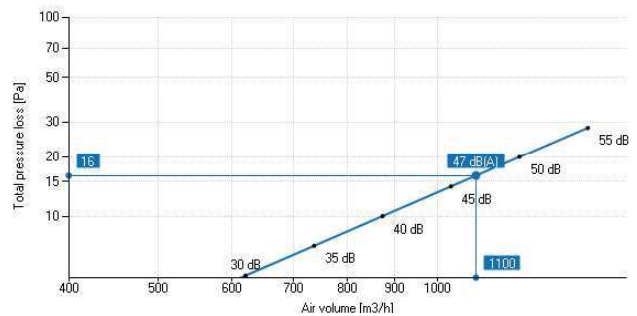
Working setup

None

Function

Extract

Hz	63	125	250	500	1K	2K	4K	8K
Kok [dB]	5	4	1	-2	-9	-16	-15	-8
$\Delta L$ [dB]	-	-	-	-	-	-	-	-





# AD - Grilles

Project: Untitled project

01-07-2019



## Requirements:

Air volume	qv	1678 m <sup>3</sup> /h
Room attenuation	Dr	4 dB
Length, L		1000
Height, H		150

## Results:

Total pressure loss	$\Delta p_t$	13 Pa
Sound power level	L <sub>wA</sub>	46 dB(A)
Sound pressure level	L <sub>pA</sub>	42 dB(A)

## AD - Grilles

AD is an adjustable single or double deflection grille made of aluminium. With adjustable blades, the grille is very useful for air supply and can be adapted to the required throw and air spread pattern.

The grille is available with several mounting options and can be delivered with mounting frame, opposed blade damper and plenum box accessories.

## Order code

AD-11-HMD-1000-150

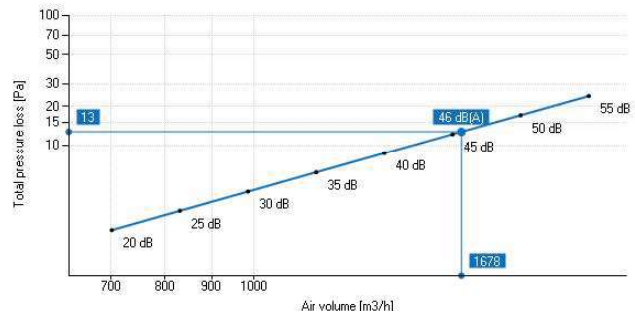
Working setup

None

Function

Extract

Hz	63	125	250	500	1K	2K	4K	8K
K <sub>ok</sub> [dB]	5	4	1	-2	-9	-16	-15	-8
$\Delta L$ [dB]	-	-	-	-	-	-	-	-



## **5.5. IZBOR VRV SISTEMA**



# VRV Selection

## Project Report

### Report details

Produced on: 7/9/2019  
Application version: 2019.7.2.5

### Project details

Project name: ARHITEKTONSKI FAKULTET PODGORICA (shared)  
Solution name: VRV  
Client Name:  
Customer reference:  
Quotation reference:  
Project number: 412178/483543

Selection parameters of the indoor units can be found in the Engineering Data Books  
Selection parameters of the outdoor units can be found in the Engineering Data Books  
Only the data published in the data book are correct. This program uses close approximations of these data.





## Material list

Model	Quantity	Description
ERQ200AW1	2	ERQ-AW1 (AHU application 3phase)
ERQ250AW1	1	ERQ-AW1 (AHU application 3phase)
REYQ12U	1	REYQ-U (VRV IV)
REYQ14U	3	REYQ-U (VRV IV)
REYQ16U	1	REYQ-U (VRV IV)
REYQ18U	1	REYQ-U (VRV IV)
REYQ20U	1	REYQ-U (VRV IV)
BS1Q10A	9	Branch selector unit
BS1Q16A	6	Branch selector unit
BS1Q25A	7	Branch selector unit
FXFQ50B	1	FXFQ-B - Round flow cassette
FXFQ100B	1	FXFQ-B - Round flow cassette
FXMQ200MB	3	FXMQ-MB - Ducted unit large ESP
FXSQ32A	2	FXSQ-A - Concealed ceiling unit with medium ESP
FXSQ50A	1	FXSQ-A - Concealed ceiling unit with medium ESP
FXSQ80A	1	FXSQ-A - Concealed ceiling unit with medium ESP
FXSQ100A	7	FXSQ-A - Concealed ceiling unit with medium ESP
FXSQ125A	6	FXSQ-A - Concealed ceiling unit with medium ESP
FXSQ140A	1	FXSQ-A - Concealed ceiling unit with medium ESP
FXZQ15A	4	FXZQ-A - Fully flat cassette
FXZQ20A	5	FXZQ-A - Fully flat cassette
FXZQ25A	7	FXZQ-A - Fully flat cassette
FXZQ32A	3	FXZQ-A - Fully flat cassette
FXZQ40A	2	FXZQ-A - Fully flat cassette
KHRQ22M20T	18	Refnet branch piping kit
KHRQ22M29T9	4	Refnet branch piping kit
KHRQ23M20T	1	Refnet branch piping kit
KHRQ23M29T9	1	Refnet branch piping kit
KHRQ23M64T	13	Refnet branch piping kit
AHU 1	1	D-AHU ADT
AHU 2	1	D-AHU ADT
DCM601A51	1	Intelligent Touch Manager
BRC1H519W	12	Remote controller (white)
BRC1H519W7	32	Remote controller (white)
BYCQ140E	2	Standard decoration panel
BYFQ60CW	21	New decoration panel (white)

Piping	Liquid	Suction	Discharge	Total
	m	m	m	m
6.4mm	83.4	0.0	0.0	83.4
9.5mm	334.3	0.0	0.0	334.3
12.7mm	106.2	83.4	130.1	319.7
15.9mm	55.5	291.5	2.8	349.8
19.1mm	0.0	16.9	52.1	69.0
22.2mm	0.0	25.9	102.5	128.4
28.6mm	0.0	161.7	28.0	189.7



## Indoor unit details

### Table of abbreviations

Abbreviation	Description
Name	Logical name of the device
FCU	Device model name
Tmp C	Indoor conditions in cooling
Rq TC	Required total cooling capacity
Rv TC	Revised total cooling capacity (asked from outdoor)
Max TC	Available total cooling capacity
Rq SC	Required sensible cooling capacity
Tevap	Evaporating temperature of indoor unit coil
Tdis C	Indoor unit discharge air temperature in cooling
Max SC	Available sensible cooling capacity
Tmp H	Indoor temperature in heating
Rq HC	Required heating capacity
Max HC	Available heating capacity
Tdis H	Indoor unit discharge air temperature in heating
Sound	Sound pressure level low and high
PS	Power supply (voltage and phases)
MCA	Minimum Circuit Amps
MOP	Maximum Overcurrent Protection
FLA	Fan Motor Input
RLA	Nominal Running Amps
WxHxD	WidthxHeightxD
Weight	Weight of the device
Min coil	Minimum coil volume
Max coil	Maximum coil volume
Air Flow Rate	Air Flow Rate



### SISTEM 1 - SUTEREN - REYQ14U

Capacity data at conditions and connection ratio (114) as entered

Name	FCU	Cooling						Heating			Air Flow Rate l/s
		Tmp C	Rq TC	Max TC	Rq SC	Tevap	Max SC	Tmp H	Rq HC	Max HC	
		°C (DBT/RH )	kW	kW	kW	°C	kW	°C	kW	kW	
S1-1	FXSQ125A	24.0/50%	10.9	12.3	n/a	6.0	9.1	20.0	9.8	16.0	600.00
S1-2	FXSQ125A	24.0/50%	11.1	12.3	n/a	6.0	9.1	20.0	8.1	16.0	600.00
S1-3	FXSQ100A	26.0/50%	9.9	11.0	n/a	6.0	7.9	20.0	8.2	12.5	533.33
S1-4	FXSQ50A	24.0/50%	4.2	4.9	n/a	6.0	3.7	20.0	4.5	6.3	253.33
			36.1						30.6		

Name	Room	Sound	PS	MCA	MOP	WxHxD	Weight
		dBA		A		mm	kg
S1-1	013 Visenamjen sa sala	33 - 39	220V 1ph	2.6	Factory Std	1,400 x 245 x 800	47.0
S1-2	012 Modelarnic a	33 - 39	220V 1ph	2.6	Factory Std	1,400 x 245 x 800	47.0
S1-3	001 Hol	31 - 36	220V 1ph	2.4	Factory Std	1,400 x 245 x 800	46.0
S1-4	001 Stampa, kopirnica	29 - 35	220V 1ph	1.1	Factory Std	700 x 245 x 800	29.0

### Remarks

#### Reduced operational load

The sum of the required indoor unit capacities is 36.1kW for cooling and 30.6kW for heating. However, the outdoor unit selection uses reduced load values for cooling of 35.8kW (=99%) and for heating of 30.5kW (=100%). Be aware that unrealistic reductions may lead to reduced comfort levels, different noise levels or increased wear and tear.

#### Outdoor vs. indoor position

Outdoor unit placed 13.0m above the indoor units.

### SISTEM 3 - PRIZEMLJE - REYQ12U

Capacity data at conditions and connection ratio (96) as entered

Name	FCU	Cooling						Heating			Air Flow Rate l/s
		Tmp C	Rq TC	Max TC	Rq SC	Tevap	Max SC	Tmp H	Rq HC	Max HC	
		°C (DBT/RH )	kW	kW	kW	°C	kW	°C	kW	kW	
S3.1	FXSQ100A	24.0/50%	9.1	9.8	n/a	6.0	7.4	20.0	5.8	12.5	533.33
S3.2	FXSQ125A	24.0/50%	10.2	12.3	n/a	6.0	9.1	20.0	7.0	16.0	600.00
S3.3	FXSQ32A	24.0/50%	2.7	3.2	n/a	6.0	2.4	20.0	2.1	4.0	158.33
S3.4	FXSQ32A	24.0/50%	2.9	3.2	n/a	6.0	2.4	20.0	2.6	4.0	158.33
			24.9						17.5		



Name	Room	Sound dBA	PS	MCA A	MOP	WxHxD mm	Weight kg
S3.1	115 Vjezbaonica 2	31 - 36	220V 1ph	2.4	Factory Std	1,400 x 245 x 800	46.0
S3.2	114 Vjezbaonica 1	33 - 39	220V 1ph	2.6	Factory Std	1,400 x 245 x 800	47.0
S3.3	113 Studentska sluzba 2	26 - 31	220V 1ph	0.8	Factory Std	550 x 245 x 800	24.0
S3.4	112 Studentska sluzba 1	26 - 31	220V 1ph	0.8	Factory Std	550 x 245 x 800	24.0

#### Remarks

#### Reduced operational load

The sum of the required indoor unit capacities is 24.9kW for cooling and 17.5kW for heating. However, the outdoor unit selection uses reduced load values for cooling of 24.2kW (=97%) and for heating of 17.3kW (=99%). Be aware that unrealistic reductions may lead to reduced comfort levels, different noise levels or increased wear and tear.

#### Outdoor vs. indoor position

Outdoor unit placed 9.0m above the indoor units.

#### SISTEM 4 - PRIZEMLJE - REYQ20U

Capacity data at conditions and connection ratio (105) as entered

Name	FCU	Cooling						Heating			Air Flow Rate l/s
		Tmp C	Rq TC	Max TC	Rq SC	Tevap	Max SC	Tmp H	Rq HC	Max HC	
		°C (DBT/RH )	kW	kW	kW	°C	kW	°C	kW	kW	
S4.1	FXMQ200MB	26.0/50%	20.6	22.0	n/a	6.0	15.9	20.0	23.5	25.0	966.67
S4.2	FXSQ100A	24.0/50%	9.1	9.8	n/a	6.0	7.4	20.0	5.7	12.5	533.33
S4.3	FXSQ125A	24.0/50%	9.9	12.3	n/a	6.0	9.1	20.0	7.0	16.0	600.00
S4.4	FXSQ100A	24.0/50%	8.6	9.8	n/a	6.0	7.4	20.0	9.0	12.5	533.33
			48.2						45.2		

Name	Room	Sound dBA	PS	MCA A	MOP	WxHxD mm	Weight kg
S4.1	107 Centralni hol	45 - 48	220V 1ph	10.3	Factory Std	1,380 x 470 x 1,100	132.0
S4.2	116 Vjezbaonica 3	31 - 36	220V 1ph	2.4	Factory Std	1,400 x 245 x 800	46.0
S4.3	117 Vjezbaonica 4	33 - 39	220V 1ph	2.6	Factory Std	1,400 x 245 x 800	47.0



Name	Room	Sound dBA	PS	MCA A	MOP	WxHxD mm	Weight kg
S4.4	111 Biblioteka	31 - 36	220V 1ph	2.4	Factory Std	1,400 x 245 x 800	46.0

#### Remarks

#### Reduced operational load

The sum of the required indoor unit capacities is 48.2kW for cooling and 45.2kW for heating. However, the outdoor unit selection uses reduced load values for cooling of 46.0kW (=95%) and for heating of 43.5kW (=96%). Be aware that unrealistic reductions may lead to reduced comfort levels, different noise levels or increased wear and tear.

#### Outdoor vs. indoor position

Outdoor unit placed 9.0m above the indoor units.

#### SISTEM 5 - I SPRAT - REYQ14U

Capacity data at conditions and connection ratio (116) as entered

Name	FCU	Cooling						Heating			Air Flow Rate l/s
		Tmp C	Rq TC	Max TC	Rq SC	Tevap	Max SC	Tmp H	Rq HC	Max HC	
		°C (DBT/RH )	kW	kW	kW	°C	kW	°C	kW	kW	
S5.1	FXSQ100A	24.0/50%	8.9	9.8	n/a	6.0	7.4	20.0	5.5	12.5	533.33
S5.2	FXSQ100A	24.0/50%	9.1	9.8	n/a	6.0	7.4	20.0	5.8	12.5	533.33
S5.3	FXSQ125A	24.0/50%	10.2	12.3	n/a	6.0	9.1	20.0	7.0	16.0	600.00
S5.4	FXSQ80A	24.0/50%	6.6	7.8	n/a	6.0	5.8	20.0	4.8	10.0	383.33
			34.8						23.1		

Name	Room	Sound dBA	PS	MCA A	MOP	WxHxD mm	Weight kg
S5.1	208 Vjezbaonica	31 - 36	220V 1ph	2.4	Factory Std	1,400 x 245 x 800	46.0
S5.2	207 Vjezbaonica	31 - 36	220V 1ph	2.4	Factory Std	1,400 x 245 x 800	46.0
S5.3	206 Vjezbaonica	33 - 39	220V 1ph	2.6	Factory Std	1,400 x 245 x 800	47.0
S5.4	202 Diplomska sala	29 - 35	220V 1ph	1.9	Factory Std	1,000 x 245 x 800	36.5

#### Remarks

#### Reduced operational load

The sum of the required indoor unit capacities is 34.8kW for cooling and 23.1kW for heating. However, the outdoor unit selection uses reduced load values for cooling of 34.0kW (=98%) and for heating of 22.8kW (=99%). Be aware that unrealistic reductions may lead to reduced comfort levels, different noise levels or increased wear and tear.

#### Outdoor vs. indoor position

Outdoor unit placed 5.0m above the indoor units.



## SISTEM 6 - I SPRAT - REYQ18U

Capacity data at conditions and connection ratio (114) as entered

Name	FCU	Cooling						Heating			Air Flow Rate l/s
		Tmp C	Rq TC	Max TC	Rq SC	Tevap	Max SC	Tmp H	Rq HC	Max HC	
		°C (DBT/RH )	kW	kW	kW	°C	kW	°C	kW	kW	
S6.1	FXMQ200MB	26.0/50%	15.8	22.0	n/a	6.0	15.9	20.0	17.7	25.0	966.67
S6.2	FXSQ100A	24.0/50%	9.1	9.8	n/a	6.0	7.4	20.0	5.7	12.5	533.33
S6.3	FXSQ125A	24.0/50%	9.9	12.3	n/a	6.0	9.1	20.0	7.0	16.0	600.00
S6.4	FXZQ15A	24.0/50%	1.5	1.5	n/a	6.0	1.3	20.0	1.2	1.9	141.67
S6.5	FXZQ25A	24.0/50%	2.1	2.5	n/a	6.0	1.8	20.0	1.7	3.2	150.00
S6.6	FXZQ25A	24.0/50%	2.4	2.5	n/a	6.0	1.8	20.0	2.3	3.2	150.00
S6.7	FXZQ25A	24.0/50%	2.0	2.5	n/a	6.0	1.8	20.0	1.7	3.2	150.00
			42.8						37.3		

Name	Room	Sound	PS	MCA	MOP	WxHxD	Weight kg
		dBA		A		mm	
S6.1	201 Hol	45 - 48	220V 1ph	10.3	Factory Std	1,380 x 470 x 1,100	132.0
S6.2	209 Vjezbaonica	31 - 36	220V 1ph	2.4	Factory Std	1,400 x 245 x 800	46.0
S6.3	210 Vjezbaonica	33 - 39	220V 1ph	2.6	Factory Std	1,400 x 245 x 800	47.0
S6.4	214 Racunovods tvo	26 - 32	230V 1ph	0.3	Factory Std	575 x 260 x 575	15.5
S6.5	215 Prodekan 1	26 - 33	230V 1ph	0.3	Factory Std	575 x 260 x 575	15.5
S6.6	216 Prodekan 2	26 - 33	230V 1ph	0.3	Factory Std	575 x 260 x 575	15.5
S6.7	217 Pravna sluzba	26 - 33	230V 1ph	0.3	Factory Std	575 x 260 x 575	15.5

### Remarks

#### Reduced operational load

The sum of the required indoor unit capacities is 42.8kW for cooling and 37.3kW for heating. However, the outdoor unit selection uses reduced load values for cooling of 41.9kW (=98%) and for heating of 37.0kW (=99%). Be aware that unrealistic reductions may lead to reduced comfort levels, different noise levels or increased wear and tear.

#### Outdoor vs. indoor position

Outdoor unit placed 5.0m above the indoor units.

## SISTEM 7 - II SPRAT - REYQ16U

Capacity data at conditions and connection ratio (123) as entered



Name	FCU	Cooling						Heating			Air Flow Rate l/s
		Tmp C	Rq TC	Max TC	Rq SC	Tevap	Max SC	Tmp H	Rq HC	Max HC	
		°C (DBT/RH )	kW	kW	kW	°C	kW	°C	kW	kW	
S7.1	FXFQ50B	24.0/50%	4.6	4.9	n/a	6.0	3.7	20.0	3.4	6.3	250.00
S7.2	FXFQ100B	24.0/50%	8.0	9.8	n/a	6.0	7.1	20.0	3.9	12.5	441.67
S7.3	FXMQ200MB	26.0/50%	16.4	22.0	n/a	6.0	15.9	20.0	18.5	25.0	966.67
S7.4	FXSQ140A	24.0/50%	12.8	14.0	n/a	6.0	10.4	20.0	6.0	18.0	650.00
			41.8						31.8		

Name	Room	Sound	PS	MCA A	MOP	WxHxD	Weight kg
		dBA				mm	
S7.1	307 Kabinet dekana	28 - 33	220V 1ph	0.4	Factory Std	840 x 204 x 840	21.0
S7.2	306 Sala nastavnog osoblja	33 - 41	220V 1ph	0.8	Factory Std	840 x 246 x 840	24.0
S7.3	301 Hol	45 - 48	220V 1ph	10.3	Factory Std	1,380 x 470 x 1,100	132.0
S7.4	302 Diplomska sala	34 - 42	220V 1ph	3.1	Factory Std	1,550 x 245 x 800	51.0

#### Remarks

#### Reduced operational load

The sum of the required indoor unit capacities is 41.8kW for cooling and 31.8kW for heating. However, the outdoor unit selection uses reduced load values for cooling of 40.6kW (=97%) and for heating of 31.7kW (=100%). Be aware that unrealistic reductions may lead to reduced comfort levels, different noise levels or increased wear and tear.

#### Outdoor vs. indoor position

Outdoor unit placed 1.0m above the indoor units.

#### SISTEM 8 - II SPRAT - REYQ14U

Capacity data at conditions and connection ratio (120) as entered

Name	FCU	Cooling						Heating			Air Flow Rate l/s
		Tmp C	Rq TC	Max TC	Rq SC	Tevap	Max SC	Tmp H	Rq HC	Max HC	
		°C (DBT/RH )	kW	kW	kW	°C	kW	°C	kW	kW	
S8.1	FXZQ20A	24.0/50%	1.7	2.0	n/a	6.0	1.5	20.0	1.4	2.5	145.00
S8.2	FXZQ20A	24.0/50%	1.6	2.0	n/a	6.0	1.5	20.0	1.3	2.5	145.00
S8.3	FXZQ20A	24.0/50%	1.6	2.0	n/a	6.0	1.5	20.0	1.4	2.5	145.00
S8.4	FXZQ20A	24.0/50%	1.6	2.0	n/a	6.0	1.5	20.0	1.4	2.5	145.00
S8.5	FXZQ20A	24.0/50%	1.7	2.0	n/a	6.0	1.5	20.0	1.3	2.5	145.00
S8.6	FXZQ25A	24.0/50%	2.4	2.5	n/a	6.0	1.8	20.0	2.3	3.2	150.00
S8.7	FXZQ40A	24.0/50%	3.3	3.9	n/a	6.0	2.9	20.0	1.7	5.0	191.67
S8.8	FXZQ15A	24.0/50%	1.5	1.5	n/a	6.0	1.3	20.0	1.2	1.9	141.67
S8.9	FXZQ40A	24.0/50%	3.2	3.9	n/a	6.0	2.9	20.0	1.7	5.0	191.67
S8.10	FXZQ32A	26.0/50%	2.8	3.5	n/a	6.0	2.3	20.0	2.7	4.0	166.67



Name	FCU	Cooling						Heating			Air Flow Rate l/s
		Tmp C	Rq TC	Max TC	Rq SC	Tevap	Max SC	Tmp H	Rq HC	Max HC	
		°C (DBT/RH )	kW	kW	kW	°C	kW	°C	kW	kW	
S8.11	FXZQ32A	26.0/50%	2.8	3.5	n/a	6.0	2.3	20.0	2.7	4.0	166.67
S8.12	FXZQ25A	24.0/50%	2.3	2.5	n/a	6.0	1.8	20.0	1.5	3.2	150.00
S8.13	FXZQ25A	24.0/50%	2.3	2.5	n/a	6.0	1.8	20.0	1.5	3.2	150.00
S8.14	FXZQ25A	24.0/50%	2.2	2.5	n/a	6.0	1.8	20.0	1.4	3.2	150.00
S8.15	FXZQ32A	24.0/50%	2.7	3.2	n/a	6.0	2.2	20.0	2.6	4.0	166.67
S8.16	FXZQ15A	24.0/50%	1.3	1.5	n/a	6.0	1.3	20.0	1.1	1.9	141.67
S8.17	FXZQ15A	24.0/50%	1.5	1.5	n/a	6.0	1.3	20.0	1.3	1.9	141.67
			36.5						28.5		

Name	Room	Sound	PS	MCA	MOP	WxHxD	Weight
		dBA		A		mm	kg
S8.1	324 Sekretarica	26 - 32	230V 1ph	0.3	Factory Std	575 x 260 x 575	15.5
S8.2	323 Kabinet 11	26 - 32	230V 1ph	0.3	Factory Std	575 x 260 x 575	15.5
S8.3	322 Kabinet 10	26 - 32	230V 1ph	0.3	Factory Std	575 x 260 x 575	15.5
S8.4	321 Kabinet 9	26 - 32	230V 1ph	0.3	Factory Std	575 x 260 x 575	15.5
S8.5	320 Kabinet 8	26 - 32	230V 1ph	0.3	Factory Std	575 x 260 x 575	15.5
S8.6	319 Kabinet 7	26 - 33	230V 1ph	0.3	Factory Std	575 x 260 x 575	15.5
S8.7	325 Trpezarija	28 - 37	230V 1ph	0.4	Factory Std	575 x 260 x 575	16.5
S8.8	326 Arhiv studentski radova	26 - 32	230V 1ph	0.3	Factory Std	575 x 260 x 575	15.5
S8.9	327 Radna sala	28 - 37	230V 1ph	0.4	Factory Std	575 x 260 x 575	16.5
S8.10	309.1 Hodnik	26 - 34	230V 1ph	0.4	Factory Std	575 x 260 x 575	16.5
S8.11	309.2 Hodnik	26 - 34	230V 1ph	0.4	Factory Std	575 x 260 x 575	16.5
S8.12	313 Kabinet 1	26 - 33	230V 1ph	0.3	Factory Std	575 x 260 x 575	15.5
S8.13	314 Kabinet 2	26 - 33	230V 1ph	0.3	Factory Std	575 x 260 x 575	15.5
S8.14	315 Kabinet 3	26 - 33	230V 1ph	0.3	Factory Std	575 x 260 x 575	15.5
S8.15	316 Kabinet 4	26 - 34	230V 1ph	0.4	Factory Std	575 x 260 x 575	16.5
S8.16	317 Kabinet 5	26 - 32	230V 1ph	0.3	Factory Std	575 x 260 x 575	15.5
S8.17	318 Kabinet 6	26 - 32	230V 1ph	0.3	Factory Std	575 x 260 x 575	15.5





## Remarks

### Reduced operational load

The sum of the required indoor unit capacities is 36.5kW for cooling and 28.5kW for heating. However, the outdoor unit selection uses reduced load values for cooling of 34.3kW (=94%) and for heating of 27.9kW (=98%). Be aware that unrealistic reductions may lead to reduced comfort levels, different noise levels or increased wear and tear.

### Outdoor vs. indoor position

Outdoor unit placed 1.0m above the indoor units.

### SISTEM 2 KK KLUB - ERQ250AW1

Capacity data at conditions and connection ratio (96) as entered

Name	FCU	Cooling						Heating			Air Flow Rate l/s
		Tmp C	Rq TC	Max TC	Rq SC	Tevap	Max SC	Tmp H	Rq HC	Max HC	
		°C (DBT/RH )	kW	kW	kW	°C	kW	°C	kW	kW	
AHU 1 box 1		n/a	26.9	30.8	n/a	6.0	n/a	n/a	28.0	34.7	n/a
			26.9						28.0		

Name	Room	Sound	PS	MCA	MOP	WxHxD	Weight
		dBA		A		mm	kg
AHU 1 box 1		-	230V 1ph			215 x 401 x 78	2.9

## Remarks

### Reduced operational load

The sum of the required indoor unit capacities is 28.0kW for heating. However, the outdoor unit selection uses reduced load values for heating of 25.0kW (=89%). Be aware that unrealistic reductions may lead to reduced comfort levels, different noise levels or increased wear and tear.

### Outdoor vs. indoor position

Outdoor unit placed at the same level as the indoor units.

### SISTEM 9-1 KK AMFITEATAR - ERQ200AW1

Capacity data at conditions and connection ratio (94) as entered

Name	FCU	Cooling						Heating			Air Flow Rate l/s
		Tmp C	Rq TC	Max TC	Rq SC	Tevap	Max SC	Tmp H	Rq HC	Max HC	
		°C (DBT/RH )	kW	kW	kW	°C	kW	°C	kW	kW	
AHU 2 box 1		n/a	21.2	24.6	n/a	6.0	n/a	n/a	20.0	27.7	n/a
			21.2						20.0		



Name	Room	Sound	PS	MCA	MOP	WxHxD	Weight
		dBA		A		mm	kg
AHU 2 box 1		-	230V 1ph			215 x 401 x 78	2.9

Remarks

Outdoor vs. indoor position

Outdoor unit placed at the same level as the indoor units.

SISTEM 9-2 KK AMFITEATAR - ERQ200AW1

Capacity data at conditions and connection ratio (94) as entered

Name	FCU	Cooling						Heating			Air Flow Rate
		Tmp C	Rq TC	Max TC	Rq SC	Tevap	Max SC	Tmp H	Rq HC	Max HC	
		°C (DBT/RH )	kW	kW	kW	°C	kW	°C	kW	kW	
AHU 2 box 2		n/a	21.2	24.6	n/a	6.0	n/a	n/a	20.0	27.7	n/a
			21.2						20.0		

Name	Room	Sound	PS	MCA	MOP	WxHxD	Weight
		dBA		A		mm	kg
AHU 2 box 2		-	230V 1ph			215 x 401 x 78	2.9

Remarks

Outdoor vs. indoor position

Outdoor unit placed at the same level as the indoor units.



## Outdoor unit details

### Table of abbreviations

Abbreviation	Description
Name	Logical name of the device
Model	Device model name
CR	Connection ratio
Tmp C	Outdoor conditions in cooling
WFR per module	Water flow per outdoor unit module
CC	Available cooling capacity
Rq CC	Required cooling capacity
PIC	Power input in cooling mode
InC	Water inlet temperature in cooling mode
OutC	Water outlet temperature in cooling mode
Tmp H	Outdoor conditions in heating (dry bulb temp. / RH)
HC	Available heating capacity (integrated heating capacity)
Rq HC	Required heating capacity
PIH	Power input in heating mode
InH	Water inlet temperature in heating mode
OutH	Water outlet temperature in heating mode
Piping	Largest distance from indoor unit to outdoor unit
Bse Refr	Standard factory refrigerant charge (16.4ft actual piping length) excluding extra refrigerant charge. For calculation of extra refrigerant charge refer to the databook
Ex Refr	Extra refrigerant charge
PS	Power supply (voltage and phases)
MCA	Minimum Circuit Amps
MOP	Maximum Overcurrent Protection
FLA	Fan Motor Input
RLA	Nominal Running Amps
WxHxD	WidthxHeightxD
Weight	Weight of the device
EER	EER value at nominal condition
IEER	IEER value at nominal condition
COP47	COP value at nominal condition and at ambient temperature of 8°C
COP17	COP value at nominal condition and at ambient temperature of -8°C



## Outdoor details

Name	Model	CR	Cooling			Heating			Piping
			Tmp C °C	CC kW	Rq CC kW	Tmp H °C (DBT/RH)	HC kW	Rq HC kW	
SISTEM 1 - SUTEREN	REYQ14U	114.3	37.0	37.9	36.1	-6.0/86%	31.3	30.6	51.0
SISTEM 3 - PRIZEMLJE	REYQ12U	95.8	37.0	25.7	24.9	-6.0/86%	25.3	17.5	53.5
SISTEM 4 - PRIZEMLJE	REYQ20U	105.0	37.0	46.9	48.2	-6.0/86%	43.7	45.2	54.5
SISTEM 5 - I SPRAT	REYQ14U	115.7	37.0	37.4	34.8	-6.0/86%	31.3	23.1	48.5
SISTEM 6 - I SPRAT	REYQ18U	114.4	37.0	43.9	42.8	-6.0/86%	39.1	37.3	60.5
SISTEM 7 - II SPRAT	REYQ16U	122.5	37.0	43.0	41.8	-6.0/86%	35.0	31.8	50.4
SISTEM 8 - II SPRAT	REYQ14U	119.6	37.0	37.5	36.5	-6.0/86%	30.9	28.5	66.4
SISTEM 2 KK KLUB	ERQ250AW1	96.1	37.0	27.7	26.9	-6.0/86%	25.2	28.0	7.5
SISTEM 9-1 KK AMFITEATAR	ERQ200AW1	94.4	37.0	22.1	21.2	-6.0/86%	21.1	20.0	7.5
SISTEM 9-2 KK AMFITEATAR	ERQ200AW1	94.4	37.0	22.1	21.2	-6.0/86%	21.1	20.0	7.5

Name	Model	PS	MCA	MOP	RLA	FLA	WxHxD mm	Weight kg
			A	A	A	A		
SISTEM 1 - SUTEREN	REYQ14U	400V 3Nph	27.0	32.0	15.6	1.8	1,240 x 1,685 x 765	314.0
BS 1	BS1Q16A	230V 1ph					388 x 207 x 326	12.0
BS 2	BS1Q16A	230V 1ph					388 x 207 x 326	12.0
BS 3	BS1Q10A	230V 1ph					388 x 207 x 326	12.0
BS 4	BS1Q10A	230V 1ph					388 x 207 x 326	12.0
SISTEM 3 - PRIZEMLJE	REYQ12U	400V 3Nph	24.0	32.0	13.8	1.5	930 x 1,685 x 765	230.0
BS 5	BS1Q25A	230V 1ph					388 x 207 x 326	15.0
BS 6	BS1Q10A	230V 1ph					388 x 207 x 326	12.0
SISTEM 4 - PRIZEMLJE	REYQ20U	400V 3Nph	39.0	50.0	28.5	2.6	1,240 x 1,685 x 765	317.0
BS 7	BS1Q25A	230V 1ph					388 x 207 x 326	15.0
BS 8	BS1Q25A	230V 1ph					388 x 207 x 326	15.0
BS 9	BS1Q10A	230V 1ph					388 x 207 x 326	12.0
SISTEM 5 - I SPRAT	REYQ14U	400V 3Nph	27.0	32.0	15.6	1.8	1,240 x 1,685 x 765	314.0
BS 10	BS1Q10A	230V 1ph					388 x 207 x 326	12.0
BS 11	BS1Q25A	230V 1ph					388 x 207 x 326	15.0
BS 12	BS1Q10A	230V 1ph					388 x 207 x 326	12.0
SISTEM 6 - I SPRAT	REYQ18U	400V 3Nph	35.0	40.0	22.0	2.6	1,240 x 1,685 x 765	317.0
BS 13	BS1Q25A	230V 1ph					388 x 207 x 326	15.0
BS 14	BS1Q25A	230V 1ph					388 x 207 x 326	15.0



Name	Model	PS	MCA A	MOP A	RLA A	FLA A	WxHxD mm	Weight kg
BS 15	BS1Q10A	230V 1ph					388 x 207 x 326	12.0
SISTEM 7 - II SPRAT	REYQ16U	400V 3Nph	31.0	40.0	18.5	2.6	1,240 x 1,685 x 765	314.0
BS 16	BS1Q10A	230V 1ph					388 x 207 x 326	12.0
BS 17	BS1Q10A	230V 1ph					388 x 207 x 326	12.0
BS 18	BS1Q25A	230V 1ph					388 x 207 x 326	15.0
BS 19	BS1Q16A	230V 1ph					388 x 207 x 326	12.0
SISTEM 8 - II SPRAT	REYQ14U	400V 3Nph	27.0	32.0	15.6	1.8	1,240 x 1,685 x 765	314.0
BS 20	BS1Q16A	230V 1ph					388 x 207 x 326	12.0
BS 21	BS1Q16A	230V 1ph					388 x 207 x 326	12.0
BS 22	BS1Q16A	230V 1ph					388 x 207 x 326	12.0
SISTEM 2 KK KLUB	ERQ250AW1	400V 3Nph	21.6	25.0			930 x 1,680 x 765	240.0
SISTEM 9-1 KK AMFITEATAR	ERQ200AW1	400V 3Nph	18.5	25.0			930 x 1,680 x 765	187.0
SISTEM 9-2 KK AMFITEATAR	ERQ200AW1	400V 3Nph	18.5	25.0			930 x 1,680 x 765	187.0

#### LOT21 - information

Name	Model	$\eta_{s,h}$ heating	$\eta_{s,c}$ cooling	SCOP	SEER
		%	%		
SISTEM 1 - SUTEREN	REYQ14U	255.8	168.3	4.30	6.50
SISTEM 3 - PRIZEMLJE	REYQ12U	257.0	183.8	4.70	6.50
SISTEM 4 - PRIZEMLJE	REYQ20U	246.7	162.7	4.10	6.20
SISTEM 5 - I SPRAT	REYQ14U	255.8	168.3	4.30	6.50
SISTEM 6 - I SPRAT	REYQ18U	250.6	172.5	4.40	6.30
SISTEM 7 - II SPRAT	REYQ16U	243.1	167.5	4.30	6.20
SISTEM 8 - II SPRAT	REYQ14U	255.8	168.3	4.30	6.50
SISTEM 2 KK KLUB	ERQ250AW1				
SISTEM 9-1 KK AMFITEATAR	ERQ200AW1				
SISTEM 9-2 KK AMFITEATAR	ERQ200AW1				

For more information go to: <https://energylabel.daikin.eu/>.

#### Refrigerant information

Name	Model	Refrigerant type	GWP	Base charge kg	Extra charge kg	TCO2 equivalent
SISTEM 1 - SUTEREN	REYQ14U	R410A	2087.5	11.8	7.7	40.8
SISTEM 3 - PRIZEMLJE	REYQ12U	R410A	2087.5	9.9	5.4	31.9
SISTEM 4 - PRIZEMLJE	REYQ20U	R410A	2087.5	11.8	14.0	53.9

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SISTEM 5 - I SPRAT	REYQ14U	R410A	2087.5	11.8	7.8	41
SISTEM 6 - I SPRAT	REYQ18U	R410A	2087.5	11.8	14.4	54.7
SISTEM 7 - II SPRAT	REYQ16U	R410A	2087.5	11.8	6.9	39.1
SISTEM 8 - II SPRAT	REYQ14U	R410A	2087.5	11.8	10.0	45.6
SISTEM 2 KK KLUB	ERQ250AW1	R410A	2087.5	8.4	unknown	17.5
SISTEM 9-1 KK AMFITEATAR	ERQ200AW1	R410A	2087.5	7.7	unknown	16.1
SISTEM 9-2 KK AMFITEATAR	ERQ200AW1	R410A	2087.5	7.7	unknown	16.1

The system(s) contain fluorinated greenhouse gases.

When extra refrigerant charge requirements are not calculated, TCO2 equivalent is calculated only considering the base refrigerant charge. Depending on the field pipe length extra refrigerant needs to be added which will increase the TCO2 equivalent.

The extra charge is calculated based on the pipe lengths specified. This may differ from the actual pipe lengths on site and therefore also from the real extra charge and the real TCO2 equivalent.

#### SISTEM 1 - SUTEREN - REYQ14U

Model	Quantity	Description
REYQ14U	1	REYQ-U (VRV IV)
BS1Q10A	2	Branch selector unit
BS1Q16A	2	Branch selector unit
FXSQ50A	1	FXSQ-A - Concealed ceiling unit with medium ESP
FXSQ100A	1	FXSQ-A - Concealed ceiling unit with medium ESP
FXSQ125A	2	FXSQ-A - Concealed ceiling unit with medium ESP
KHRQ23M20T	1	Refnet branch piping kit
KHRQ23M29T9	1	Refnet branch piping kit
KHRQ23M64T	1	Refnet branch piping kit
BRC1H519W	4	Remote controller (white)

Piping	Liquid	Suction	Discharge	Total
	m	m	m	m
6.4mm	2.0	0.0	0.0	2.0
9.5mm	42.5	0.0	0.0	42.5
12.7mm	24.0	2.0	31.0	57.0
15.9mm	0.0	37.0	1.0	38.0
19.1mm	0.0	1.0	4.5	5.5
22.2mm	0.0	4.5	24.0	28.5
28.6mm	0.0	24.0	0.0	24.0



## Refrigerant information

Refrigerant type	GWP	Base charge kg	Extra charge kg	TCO2 equivalent
R410A	2087.5	11.8	7.7*)	40.8

The system(s) contain fluorinated greenhouse gases.

\*) Extra refrigerant charge = 0.5 (A) + 1.3 (B) + 0.3 (C) + 1.04 × [ 24.0 m (ø12.7 mm) × 0.12 + 42.5 m (ø9.5 mm) × 0.059 + 2.0 m (ø6.4 mm) × 0.022 ] = 7.7kg

The extra charge is calculated based on the pipe lengths specified. This may differ from the actual pipe lengths on site and therefore also from the real extra charge and the real TCO2 equivalent.

## Piping limitations

Description	Value
Maximum total length	1,000.0m
Maximum longest actual length	165.0m
Maximum longest equivalent length	190.0m
Maximum main pipe length (size up of main pipe required if longer)	-
Maximum length first branch to indoor unit(size up of intermediate pipes required if longer)	40.0m
Maximum length first branch to indoor unit	90.0m
Maximum length of indoor units to nearest branch	40.0m
Maximum length difference between longest and shortest distance to indoor units	40.0m
Maximum height difference, outdoor unit below indoor units	90.0m
Minimum connection ratio, outdoor unit below indoor units	-
Maximum height difference, outdoor unit above indoor units	90.0m
Minimum connection ratio, outdoor unit above indoor units	-
Maximum height difference in technical cooling, outdoor unit below indoor units	90.0m
Maximum height difference in technical cooling, outdoor unit above indoor units	90.0m
Maximum height difference between indoor units	30.0m
Connection ratio range	50.0% - 130.0%
Refrigerant pipe diameters	15.9mm (liquid) x 28.6mm (gas) x 22.2mm (discharge)
Maximum equivalent length from BP unit or VRV indoor to VRV REFNET (size up of intermediate pipes required if longer)	-
Maximum equivalent length from BP unit or VRV indoor to VRV REFNET	90.0m
Maximum actual length between CM and HM	-
Maximum height difference between CM and HM	-

## Pipe capacities

Maximum Connection Index	Diameters
149.9	9.5mmx15.9mmx12.7mm
199.9	9.5mmx19.1mmx15.9mm
289.9	9.5mmx22.2mmx19.1mm
419.9	12.7mmx28.6mmx19.1mm
639.9	15.9mmx28.6mmx28.6mm
919.9	19.1mmx34.9mmx28.6mm
> 919.9	19.1mmx41.3mmx28.6mm



Maximum Connection Index	Diameters
Main pipe size up	15.9mmx28.6mmx22.2mm

#### Remarks

Please make sure to provide a drain pipe connection to each multi BS-box in the system.



### SISTEM 3 - PRIZEMLJE - REYQ12U

Model	Quantity	Description
REYQ12U	1	REYQ-U (VRV IV)
BS1Q10A	1	Branch selector unit
BS1Q25A	1	Branch selector unit
FXSQ32A	2	FXSQ-A - Concealed ceiling unit with medium ESP
FXSQ100A	1	FXSQ-A - Concealed ceiling unit with medium ESP
FXSQ125A	1	FXSQ-A - Concealed ceiling unit with medium ESP
KHRQ22M20T	1	Refnet branch piping kit
KHRQ22M29T9	1	Refnet branch piping kit
KHRQ23M64T	1	Refnet branch piping kit
BRC1H519W	4	Remote controller (white)

Piping	Liquid m	Suction m	Discharge m	Total m
6.4mm	10.0	0.0	0.0	10.0
9.5mm	38.0	0.0	0.0	38.0
12.7mm	20.5	10.0	16.0	46.5
15.9mm	0.0	34.5	0.0	34.5
19.1mm	0.0	0.0	23.0	23.0
22.2mm	0.0	3.5	0.0	3.5
28.6mm	0.0	20.5	0.0	20.5

### Refrigerant information

Refrigerant type	GWP	Base charge kg	Extra charge kg	TCO2 equivalent
R410A	2087.5	9.9	5.4*)	31.9

The system(s) contain fluorinated greenhouse gases.

\*) Extra refrigerant charge =  $0.25 (C) + 1.04 \times [ 20.5 \text{ m } (\varnothing 12.7 \text{ mm}) \times 0.12 + 38.0 \text{ m } (\varnothing 9.5 \text{ mm}) \times 0.059 + 10.0 \text{ m } (\varnothing 6.4 \text{ mm}) \times 0.022 ] = 5.4 \text{ kg}$

The extra charge is calculated based on the pipe lengths specified. This may differ from the actual pipe lengths on site and therefore also from the real extra charge and the real TCO2 equivalent.

### Piping limitations

Description	Value
Maximum total length	1,000.0m
Maximum longest actual length	165.0m
Maximum longest equivalent length	190.0m
Maximum main pipe length (size up of main pipe required if longer)	-
Maximum length first branch to indoor unit (size up of intermediate pipes required if longer)	40.0m
Maximum length first branch to indoor unit	90.0m
Maximum length of indoor units to nearest branch	40.0m
Maximum length difference between longest and shortest distance to indoor units	40.0m



Maximum height difference, outdoor unit below indoor units	90.0m
Minimum connection ratio, outdoor unit below indoor units	-
Maximum height difference, outdoor unit above indoor units	90.0m
Minimum connection ratio, outdoor unit above indoor units	-
Maximum height difference in technical cooling, outdoor unit below indoor units	90.0m
Maximum height difference in technical cooling, outdoor unit above indoor units	90.0m
Maximum height difference between indoor units	30.0m
Connection ratio range	50.0% - 130.0%
Refrigerant pipe diameters	15.9mm (liquid) x 28.6mm (gas) x 19.1mm (discharge)
Maximum equivalent length from BP unit or VRV indoor to VRV REFNET (size up of intermediate pipes required if longer)	-
Maximum equivalent length from BP unit or VRV indoor to VRV REFNET	90.0m
Maximum actual length between CM and HM	-
Maximum height difference between CM and HM	-

### Pipe capacities

Maximum Connection Index	Diameters
149.9	9.5mmx15.9mmx12.7mm
199.9	9.5mmx19.1mmx15.9mm
289.9	9.5mmx22.2mmx19.1mm
419.9	12.7mmx28.6mmx19.1mm
639.9	15.9mmx28.6mmx28.6mm
919.9	19.1mmx34.9mmx28.6mm
> 919.9	19.1mmx41.3mmx28.6mm
Main pipe size up	15.9mmx28.6mmx19.1mm

### Remarks

Please make sure to provide a drain pipe connection to each multi BS-box in the system.



#### SISTEM 4 - PRIZEMLJE - REYQ20U

Model	Quantity	Description
REYQ20U	1	REYQ-U (VRV IV)
BS1Q10A	1	Branch selector unit
BS1Q25A	2	Branch selector unit
FXMQ200MB	1	FXMQ-MB - Ducted unit large ESP
FXSQ100A	2	FXSQ-A - Concealed ceiling unit with medium ESP
FXSQ125A	1	FXSQ-A - Concealed ceiling unit with medium ESP
KHRQ22M29T9	1	Refnet branch piping kit
KHRQ23M64T	2	Refnet branch piping kit
BRC1H519W	4	Remote controller (white)

Piping	Liquid	Suction	Discharge	Total
	m	m	m	m
9.5mm	47.5	0.0	0.0	47.5
12.7mm	1.0	0.0	12.0	13.0
15.9mm	28.0	37.5	0.0	65.5
19.1mm	0.0	3.0	6.5	9.5
22.2mm	0.0	7.0	0.0	7.0
28.6mm	0.0	29.0	28.0	57.0

#### Refrigerant information

Refrigerant type	GWP	Base charge kg	Extra charge kg	TCO2 equivalent
R410A	2087.5	11.8	14.0*)	53.9

The system(s) contain fluorinated greenhouse gases.

\*) Extra refrigerant charge = 0.5 (A) + 4.8 (B) + 0.45 (C) + 1.04 × [ 28.0 m (ø15.9 mm) × 0.18 + 1.0 m (ø12.7 mm) × 0.12 + 47.5 m (ø9.5 mm) × 0.059 ] = 14.0kg

The extra charge is calculated based on the pipe lengths specified. This may differ from the actual pipe lengths on site and therefore also from the real extra charge and the real TCO2 equivalent.

#### Piping limitations

Description	Value
Maximum total length	1,000.0m
Maximum longest actual length	165.0m
Maximum longest equivalent length	190.0m
Maximum main pipe length (size up of main pipe required if longer)	-
Maximum length first branch to indoor unit(size up of intermediate pipes required if longer)	40.0m
Maximum length first branch to indoor unit	90.0m
Maximum length of indoor units to nearest branch	40.0m
Maximum length difference between longest and shortest distance to indoor units	40.0m
Maximum height difference, outdoor unit below indoor units	90.0m
Minimum connection ratio, outdoor unit below indoor units	-



Maximum height difference, outdoor unit above indoor units	90.0m
Minimum connection ratio, outdoor unit above indoor units	-
Maximum height difference in technical cooling, outdoor unit below indoor units	90.0m
Maximum height difference in technical cooling, outdoor unit above indoor units	90.0m
Maximum height difference between indoor units	30.0m
Connection ratio range	50.0% - 130.0%
Refrigerant pipe diameters	19.1mm (liquid) x 28.6mm (gas) x 28.6mm (discharge)
Maximum equivalent length from BP unit or VRV indoor to VRV REFNET (size up of intermediate pipes required if longer)	-
Maximum equivalent length from BP unit or VRV indoor to VRV REFNET	90.0m
Maximum actual length between CM and HM	-
Maximum height difference between CM and HM	-

### Pipe capacities

Maximum Connection Index	Diameters
149.9	9.5mmx15.9mmx12.7mm
199.9	9.5mmx19.1mmx15.9mm
289.9	9.5mmx22.2mmx19.1mm
419.9	12.7mmx28.6mmx19.1mm
639.9	15.9mmx28.6mmx28.6mm
919.9	19.1mmx34.9mmx28.6mm
> 919.9	19.1mmx41.3mmx28.6mm
Main pipe size up	19.1mmx28.6mmx28.6mm

### Remarks

Please make sure to provide a drain pipe connection to each multi BS-box in the system.



## SISTEM 5 - I SPRAT - REYQ14U

Model	Quantity	Description
REYQ14U	1	REYQ-U (VRV IV)
BS1Q10A	2	Branch selector unit
BS1Q25A	1	Branch selector unit
FXSQ80A	1	FXSQ-A - Concealed ceiling unit with medium ESP
FXSQ100A	2	FXSQ-A - Concealed ceiling unit with medium ESP
FXSQ125A	1	FXSQ-A - Concealed ceiling unit with medium ESP
KHRQ22M29T9	1	Refnet branch piping kit
KHRQ23M64T	2	Refnet branch piping kit
BRC1H519W7	4	Remote controller (white)

Piping	Liquid	Suction	Discharge	Total
	m	m	m	m
9.5mm	55.0	0.0	0.0	55.0
12.7mm	19.0	0.0	22.5	41.5
15.9mm	0.0	51.5	0.0	51.5
19.1mm	0.0	0.0	4.0	4.0
22.2mm	0.0	3.5	17.5	21.0
28.6mm	0.0	19.0	0.0	19.0

## Refrigerant information

Refrigerant type	GWP	Base charge kg	Extra charge kg	TCO2 equivalent
R410A	2087.5	11.8	7.8*)	41

The system(s) contain fluorinated greenhouse gases.

\*) Extra refrigerant charge = 0.5 (A) + 1.3 (B) + 0.3 (C) + 1.04 × [ 19.0 m (ø12.7 mm) × 0.12 + 55.0 m (ø9.5 mm) × 0.059 ] = 7.8kg

The extra charge is calculated based on the pipe lengths specified. This may differ from the actual pipe lengths on site and therefore also from the real extra charge and the real TCO2 equivalent.

## Piping limitations

Description	Value
Maximum total length	1,000.0m
Maximum longest actual length	165.0m
Maximum longest equivalent length	190.0m
Maximum main pipe length (size up of main pipe required if longer)	-
Maximum length first branch to indoor unit(size up of intermediate pipes required if longer)	40.0m
Maximum length first branch to indoor unit	90.0m
Maximum length of indoor units to nearest branch	40.0m
Maximum length difference between longest and shortest distance to indoor units	40.0m
Maximum height difference, outdoor unit below indoor units	90.0m
Minimum connection ratio, outdoor unit below indoor units	-
Maximum height difference, outdoor unit above indoor units	90.0m



Minimum connection ratio, outdoor unit above indoor units	-
Maximum height difference in technical cooling, outdoor unit below indoor units	90.0m
Maximum height difference in technical cooling, outdoor unit above indoor units	90.0m
Maximum height difference between indoor units	30.0m
Connection ratio range	50.0% - 130.0%
Refrigerant pipe diameters	15.9mm (liquid) x 28.6mm (gas) x 22.2mm (discharge)
Maximum equivalent length from BP unit or VRV indoor to VRV REFNET (size up of intermediate pipes required if longer)	-
Maximum equivalent length from BP unit or VRV indoor to VRV REFNET	90.0m
Maximum actual length between CM and HM	-
Maximum height difference between CM and HM	-

### Pipe capacities

Maximum Connection Index	Diameters
149.9	9.5mmx15.9mmx12.7mm
199.9	9.5mmx19.1mmx15.9mm
289.9	9.5mmx22.2mmx19.1mm
419.9	12.7mmx28.6mmx19.1mm
639.9	15.9mmx28.6mmx28.6mm
919.9	19.1mmx34.9mmx28.6mm
> 919.9	19.1mmx41.3mmx28.6mm
Main pipe size up	15.9mmx28.6mmx22.2mm

### Remarks

Please make sure to provide a drain pipe connection to each multi BS-box in the system.

## SISTEM 6 - I SPRAT - REYQ18U

Model	Quantity	Description
REYQ18U	1	REYQ-U (VRV IV)
BS1Q10A	1	Branch selector unit
BS1Q25A	2	Branch selector unit
FXMQ200MB	1	FXMQ-MB - Ducted unit large ESP
FXSQ100A	1	FXSQ-A - Concealed ceiling unit with medium ESP
FXSQ125A	1	FXSQ-A - Concealed ceiling unit with medium ESP
FXZQ15A	1	FXZQ-A - Fully flat cassette
FXZQ25A	3	FXZQ-A - Fully flat cassette
KHRQ22M20T	3	Refnet branch piping kit
KHRQ22M29T9	1	Refnet branch piping kit
KHRQ23M64T	2	Refnet branch piping kit
BRC1H519W7	7	Remote controller (white)
BYFQ60CW	4	New decoration panel (white)

Piping	Liquid m	Suction m	Discharge m	Total m
6.4mm	16.0	0.0	0.0	16.0
9.5mm	50.5	0.0	0.0	50.5
12.7mm	1.0	16.0	10.0	27.0
15.9mm	27.5	40.0	0.0	67.5
19.1mm	0.0	4.5	5.5	10.0
22.2mm	0.0	6.0	27.5	33.5
28.6mm	0.0	28.5	0.0	28.5

### Refrigerant information

Refrigerant type	GWP	Base charge kg	Extra charge kg	TCO2 equivalent
R410A	2087.5	11.8	14.4*)	54.7

The system(s) contain fluorinated greenhouse gases.

\*) Extra refrigerant charge = 0.5 (A) + 4.7 (B) + 0.45 (C) + 1.04 × [ 27.5 m (ø15.9 mm) × 0.18 + 1.0 m (ø12.7 mm) × 0.12 + 50.5 m (ø9.5 mm) × 0.059 + 16.0 m (ø6.4 mm) × 0.022 ] = 14.4kg

The extra charge is calculated based on the pipe lengths specified. This may differ from the actual pipe lengths on site and therefore also from the real extra charge and the real TCO2 equivalent.

### Piping limitations

Description	Value
Maximum total length	1,000.0m
Maximum longest actual length	165.0m
Maximum longest equivalent length	190.0m
Maximum main pipe length (size up of main pipe required if longer)	-
Maximum length first branch to indoor unit(size up of intermediate pipes required if longer)	40.0m



Maximum length first branch to indoor unit	90.0m
Maximum length of indoor units to nearest branch	40.0m
Maximum length difference between longest and shortest distance to indoor units	40.0m
Maximum height difference, outdoor unit below indoor units	90.0m
Minimum connection ratio, outdoor unit below indoor units	-
Maximum height difference, outdoor unit above indoor units	90.0m
Minimum connection ratio, outdoor unit above indoor units	-
Maximum height difference in technical cooling, outdoor unit below indoor units	90.0m
Maximum height difference in technical cooling, outdoor unit above indoor units	90.0m
Maximum height difference between indoor units	30.0m
Connection ratio range	50.0% - 130.0%
Refrigerant pipe diameters	19.1mm (liquid) x 28.6mm (gas) x 22.2mm (discharge)
Maximum equivalent length from BP unit or VRV indoor to VRV REFNET (size up of intermediate pipes required if longer)	-
Maximum equivalent length from BP unit or VRV indoor to VRV REFNET	90.0m
Maximum actual length between CM and HM	-
Maximum height difference between CM and HM	-

#### Pipe capacities

Maximum Connection Index	Diameters
149.9	9.5mmx15.9mmx12.7mm
199.9	9.5mmx19.1mmx15.9mm
289.9	9.5mmx22.2mmx19.1mm
419.9	12.7mmx28.6mmx19.1mm
639.9	15.9mmx28.6mmx28.6mm
919.9	19.1mmx34.9mmx28.6mm
> 919.9	19.1mmx41.3mmx28.6mm
Main pipe size up	19.1mmx28.6mmx22.2mm

#### Remarks

Please make sure to provide a drain pipe connection to each multi BS-box in the system.



## SISTEM 7 - II SPRAT - REYQ16U

Model	Quantity	Description
REYQ16U	1	REYQ-U (VRV IV)
BS1Q10A	2	Branch selector unit
BS1Q16A	1	Branch selector unit
BS1Q25A	1	Branch selector unit
FXFQ50B	1	FXFQ-B - Round flow cassette
FXFQ100B	1	FXFQ-B - Round flow cassette
FXMQ200MB	1	FXMQ-MB - Ducted unit large ESP
FXSQ140A	1	FXSQ-A - Concealed ceiling unit with medium ESP
KHRQ23M64T	3	Refnet branch piping kit
BRC1H519W7	4	Remote controller (white)
BYCQ140E	2	Standard decoration panel

Piping	Liquid	Suction	Discharge	Total
	m	m	m	m
6.4mm	2.9	0.0	0.0	2.9
9.5mm	40.3	0.0	0.0	40.3
12.7mm	16.6	2.9	23.9	43.4
15.9mm	0.0	34.3	0.0	34.3
19.1mm	0.0	4.6	4.0	8.6
22.2mm	0.0	1.4	14.0	15.4
28.6mm	0.0	16.6	0.0	16.6

### Refrigerant information

Refrigerant type	GWP	Base charge kg	Extra charge kg	TCO2 equivalent
R410A	2087.5	11.8	6.9*)	39.1

The system(s) contain fluorinated greenhouse gases.

\*) Extra refrigerant charge = 0.5 (A) + 1.4 (B) + 0.4 (C) + 1.04 × [ 16.6 m (ø12.7 mm) × 0.12 + 40.3 m (ø9.5 mm) × 0.059 + 2.9 m (ø6.4 mm) × 0.022 ] = 6.9kg

The extra charge is calculated based on the pipe lengths specified. This may differ from the actual pipe lengths on site and therefore also from the real extra charge and the real TCO2 equivalent.

### Piping limitations

Description	Value
Maximum total length	1,000.0m
Maximum longest actual length	165.0m
Maximum longest equivalent length	190.0m
Maximum main pipe length (size up of main pipe required if longer)	-
Maximum length first branch to indoor unit(size up of intermediate pipes required if longer)	40.0m
Maximum length first branch to indoor unit	90.0m
Maximum length of indoor units to nearest branch	40.0m



Maximum length difference between longest and shortest distance to indoor units	40.0m
Maximum height difference, outdoor unit below indoor units	90.0m
Minimum connection ratio, outdoor unit below indoor units	-
Maximum height difference, outdoor unit above indoor units	90.0m
Minimum connection ratio, outdoor unit above indoor units	-
Maximum height difference in technical cooling, outdoor unit below indoor units	90.0m
Maximum height difference in technical cooling, outdoor unit above indoor units	90.0m
Maximum height difference between indoor units	30.0m
Connection ratio range	50.0% - 130.0%
Refrigerant pipe diameters	15.9mm (liquid) x 28.6mm (gas) x 22.2mm (discharge)
Maximum equivalent length from BP unit or VRV indoor to VRV REFNET (size up of intermediate pipes required if longer)	-
Maximum equivalent length from BP unit or VRV indoor to VRV REFNET	90.0m
Maximum actual length between CM and HM	-
Maximum height difference between CM and HM	-

#### Pipe capacities

Maximum Connection Index	Diameters
149.9	9.5mmx15.9mmx12.7mm
199.9	9.5mmx19.1mmx15.9mm
289.9	9.5mmx22.2mmx19.1mm
419.9	12.7mmx28.6mmx19.1mm
639.9	15.9mmx28.6mmx28.6mm
919.9	19.1mmx34.9mmx28.6mm
> 919.9	19.1mmx41.3mmx28.6mm
Main pipe size up	15.9mmx28.6mmx22.2mm

#### Remarks

Please make sure to provide a drain pipe connection to each multi BS-box in the system.



## SISTEM 8 - II SPRAT - REYQ14U

Model	Quantity	Description
REYQ14U	1	REYQ-U (VRV IV)
BS1Q16A	3	Branch selector unit
FXZQ15A	3	FXZQ-A - Fully flat cassette
FXZQ20A	5	FXZQ-A - Fully flat cassette
FXZQ25A	4	FXZQ-A - Fully flat cassette
FXZQ32A	3	FXZQ-A - Fully flat cassette
FXZQ40A	2	FXZQ-A - Fully flat cassette
KHRQ22M20T	14	Refnet branch piping kit
KHRQ23M64T	2	Refnet branch piping kit
BRC1H519W7	17	Remote controller (white)
BYFQ60CW	17	New decoration panel (white)

Piping	Liquid	Suction	Discharge	Total
	m	m	m	m
6.4mm	52.5	0.0	0.0	52.5
9.5mm	60.5	0.0	0.0	60.5
12.7mm	24.1	52.5	14.7	91.3
15.9mm	0.0	56.7	1.8	58.5
19.1mm	0.0	3.8	4.6	8.4
22.2mm	0.0	0.0	19.5	19.5
28.6mm	0.0	24.1	0.0	24.1

## Refrigerant information

Refrigerant type	GWP	Base charge kg	Extra charge kg	TCO2 equivalent
R410A	2087.5	11.8	10.0*)	45.6

The system(s) contain fluorinated greenhouse gases.

\*) Extra refrigerant charge =  $0.5 (A) + 1.3 (B) + 0.3 (C) + 1.04 \times [24.1 \text{ m } (\varnothing 12.7 \text{ mm}) \times 0.12 + 60.5 \text{ m } (\varnothing 9.5 \text{ mm}) \times 0.059 + 52.5 \text{ m } (\varnothing 6.4 \text{ mm}) \times 0.022] = 10.0 \text{ kg}$

The extra charge is calculated based on the pipe lengths specified. This may differ from the actual pipe lengths on site and therefore also from the real extra charge and the real TCO2 equivalent.

## Piping limitations

Description	Value
Maximum total length	1,000.0m
Maximum longest actual length	165.0m
Maximum longest equivalent length	190.0m
Maximum main pipe length (size up of main pipe required if longer)	-
Maximum length first branch to indoor unit (size up of intermediate pipes required if longer)	40.0m
Maximum length first branch to indoor unit	90.0m
Maximum length of indoor units to nearest branch	40.0m



Maximum length difference between longest and shortest distance to indoor units	40.0m
Maximum height difference, outdoor unit below indoor units	90.0m
Minimum connection ratio, outdoor unit below indoor units	-
Maximum height difference, outdoor unit above indoor units	90.0m
Minimum connection ratio, outdoor unit above indoor units	-
Maximum height difference in technical cooling, outdoor unit below indoor units	90.0m
Maximum height difference in technical cooling, outdoor unit above indoor units	90.0m
Maximum height difference between indoor units	30.0m
Connection ratio range	50.0% - 130.0%
Refrigerant pipe diameters	15.9mm (liquid) x 28.6mm (gas) x 22.2mm (discharge)
Maximum equivalent length from BP unit or VRV indoor to VRV REFNET (size up of intermediate pipes required if longer)	-
Maximum equivalent length from BP unit or VRV indoor to VRV REFNET	90.0m
Maximum actual length between CM and HM	-
Maximum height difference between CM and HM	-

### Pipe capacities

Maximum Connection Index	Diameters
149.9	9.5mmx15.9mmx12.7mm
199.9	9.5mmx19.1mmx15.9mm
289.9	9.5mmx22.2mmx19.1mm
419.9	12.7mmx28.6mmx19.1mm
639.9	15.9mmx28.6mmx28.6mm
919.9	19.1mmx34.9mmx28.6mm
> 919.9	19.1mmx41.3mmx28.6mm
Main pipe size up	15.9mmx28.6mmx22.2mm

### Remarks

Please make sure to provide a drain pipe connection to each multi BS-box in the system.



## SISTEM 2 KK KLUB - ERQ250AW1

Model	Quantity	Description
ERQ250AW1	1	ERQ-AW1 (AHU application 3phase)

### Refrigerant information

Refrigerant type	GWP	Base charge kg	Extra charge kg	TCO2 equivalent
R410A	2087.5	8.4	unknown	17.5

The system(s) contain fluorinated greenhouse gases.

### Piping limitations

Description	Value
Maximum total length	50.0m
Maximum longest actual length	50.0m
Maximum longest equivalent length	50.0m
Maximum main pipe length (size up of main pipe required if longer)	-
Maximum length first branch to indoor unit(size up of intermediate pipes required if longer)	40.0m
Maximum length first branch to indoor unit	50.0m
Maximum length of indoor units to nearest branch	40.0m
Maximum length difference between longest and shortest distance to indoor units	40.0m
Maximum height difference, outdoor unit below indoor units	30.0m
Minimum connection ratio, outdoor unit below indoor units	-
Maximum height difference, outdoor unit above indoor units	30.0m
Minimum connection ratio, outdoor unit above indoor units	-
Maximum height difference in technical cooling, outdoor unit below indoor units	30.0m
Maximum height difference in technical cooling, outdoor unit above indoor units	30.0m
Maximum height difference between indoor units	-
Connection ratio range	50.0% - 110.0%
Refrigerant pipe diameters	9.5mm (liquid) x 22.2mm (gas)
Maximum equivalent length from BP unit or VRV indoor to VRV REFNET (size up of intermediate pipes required if longer)	-
Maximum equivalent length from BP unit or VRV indoor to VRV REFNET	50.0m
Maximum actual length between CM and HM	-
Maximum height difference between CM and HM	-

### Pipe capacities

Maximum Connection Index	Diameters
149.9	9.5mmx15.9mm
199.9	9.5mmx19.1mm
289.9	9.5mmx22.2mm
419.9	12.7mmx28.6mm
639.9	15.9mmx28.6mm



Maximum Connection Index	Diameters
919.9	19.1mmx34.9mm
> 919.9	19.1mmx41.3mm
Main pipe size up	9.5mmx22.2mm



## SISTEM 9-1 KK AMFITEATAR - ERQ200AW1

Model	Quantity	Description
ERQ200AW1	1	ERQ-AW1 (AHU application 3phase)

### Refrigerant information

Refrigerant type	GWP	Base charge kg	Extra charge kg	TCO2 equivalent
R410A	2087.5	7.7	unknown	16.1

The system(s) contain fluorinated greenhouse gases.

### Piping limitations

Description	Value
Maximum total length	50.0m
Maximum longest actual length	50.0m
Maximum longest equivalent length	50.0m
Maximum main pipe length (size up of main pipe required if longer)	-
Maximum length first branch to indoor unit(size up of intermediate pipes required if longer)	40.0m
Maximum length first branch to indoor unit	50.0m
Maximum length of indoor units to nearest branch	40.0m
Maximum length difference between longest and shortest distance to indoor units	40.0m
Maximum height difference, outdoor unit below indoor units	30.0m
Minimum connection ratio, outdoor unit below indoor units	-
Maximum height difference, outdoor unit above indoor units	30.0m
Minimum connection ratio, outdoor unit above indoor units	-
Maximum height difference in technical cooling, outdoor unit below indoor units	30.0m
Maximum height difference in technical cooling, outdoor unit above indoor units	30.0m
Maximum height difference between indoor units	-
Connection ratio range	50.0% - 110.0%
Refrigerant pipe diameters	9.5mm (liquid) x 19.1mm (gas)
Maximum equivalent length from BP unit or VRV indoor to VRV REFNET (size up of intermediate pipes required if longer)	-
Maximum equivalent length from BP unit or VRV indoor to VRV REFNET	50.0m
Maximum actual length between CM and HM	-
Maximum height difference between CM and HM	-

### Pipe capacities

Maximum Connection Index	Diameters
149.9	9.5mmx15.9mm
199.9	9.5mmx19.1mm
289.9	9.5mmx22.2mm
419.9	12.7mmx28.6mm
639.9	15.9mmx28.6mm



Maximum Connection Index	Diameters
919.9	19.1mmx34.9mm
> 919.9	19.1mmx41.3mm
Main pipe size up	9.5mmx19.1mm





## SISTEM 9-2 KK AMFITEATAR - ERQ200AW1

Model	Quantity	Description
ERQ200AW1	1	ERQ-AW1 (AHU application 3phase)

### Refrigerant information

Refrigerant type	GWP	Base charge kg	Extra charge kg	TCO2 equivalent
R410A	2087.5	7.7	unknown	16.1

The system(s) contain fluorinated greenhouse gases.

### Piping limitations

Description	Value
Maximum total length	50.0m
Maximum longest actual length	50.0m
Maximum longest equivalent length	50.0m
Maximum main pipe length (size up of main pipe required if longer)	-
Maximum length first branch to indoor unit(size up of intermediate pipes required if longer)	40.0m
Maximum length first branch to indoor unit	50.0m
Maximum length of indoor units to nearest branch	40.0m
Maximum length difference between longest and shortest distance to indoor units	40.0m
Maximum height difference, outdoor unit below indoor units	30.0m
Minimum connection ratio, outdoor unit below indoor units	-
Maximum height difference, outdoor unit above indoor units	30.0m
Minimum connection ratio, outdoor unit above indoor units	-
Maximum height difference in technical cooling, outdoor unit below indoor units	30.0m
Maximum height difference in technical cooling, outdoor unit above indoor units	30.0m
Maximum height difference between indoor units	-
Connection ratio range	50.0% - 110.0%
Refrigerant pipe diameters	9.5mm (liquid) x 19.1mm (gas)
Maximum equivalent length from BP unit or VRV indoor to VRV REFNET (size up of intermediate pipes required if longer)	-
Maximum equivalent length from BP unit or VRV indoor to VRV REFNET	50.0m
Maximum actual length between CM and HM	-
Maximum height difference between CM and HM	-

### Pipe capacities

Maximum Connection Index	Diameters
149.9	9.5mmx15.9mm
199.9	9.5mmx19.1mm
289.9	9.5mmx22.2mm
419.9	12.7mmx28.6mm
639.9	15.9mmx28.6mm

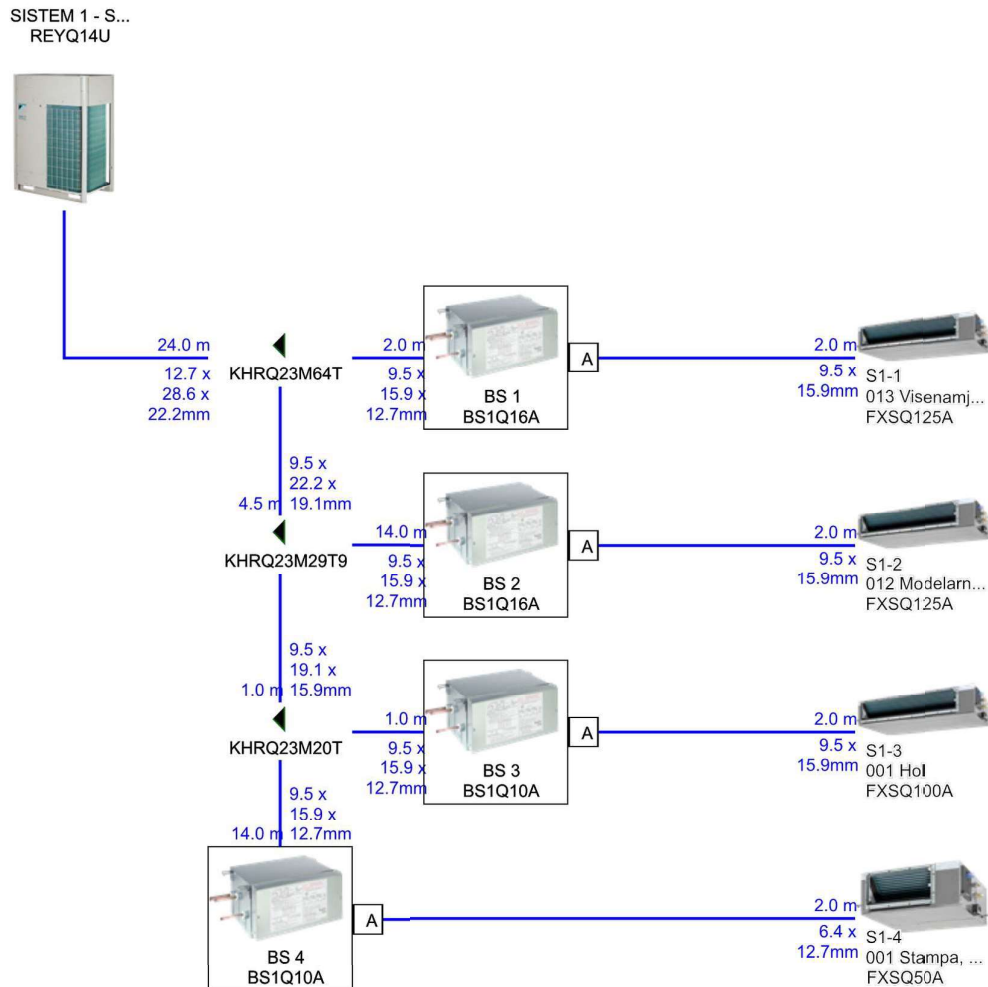
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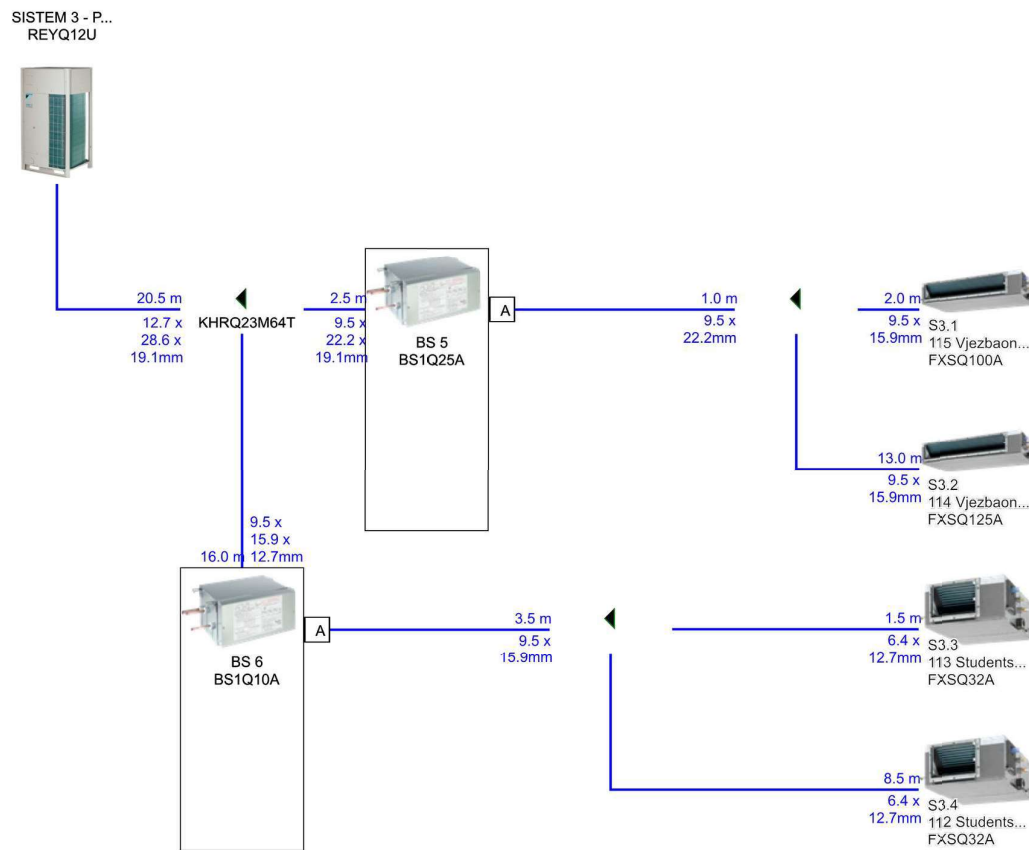
Maximum Connection Index	Diameters
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> 919.9	19.1mmx41.3mm
Main pipe size up	9.5mmx19.1mm

## Piping diagrams

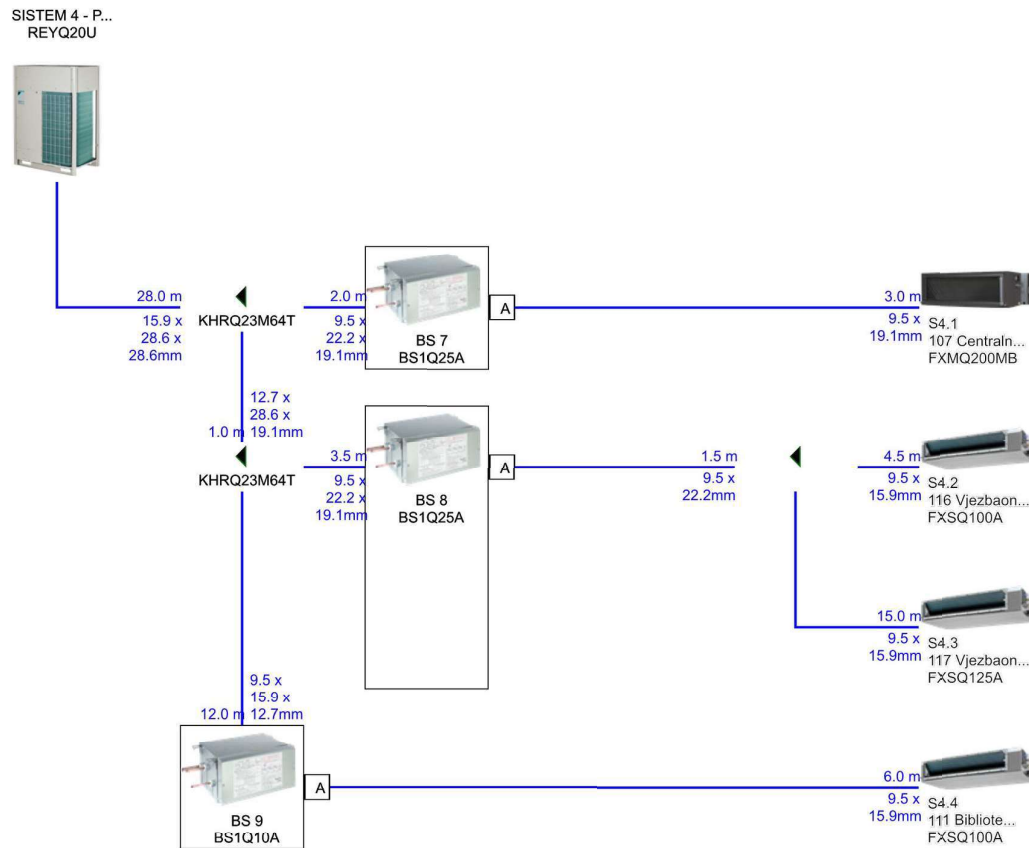
### Piping SISTEM 1 - SUTEREN



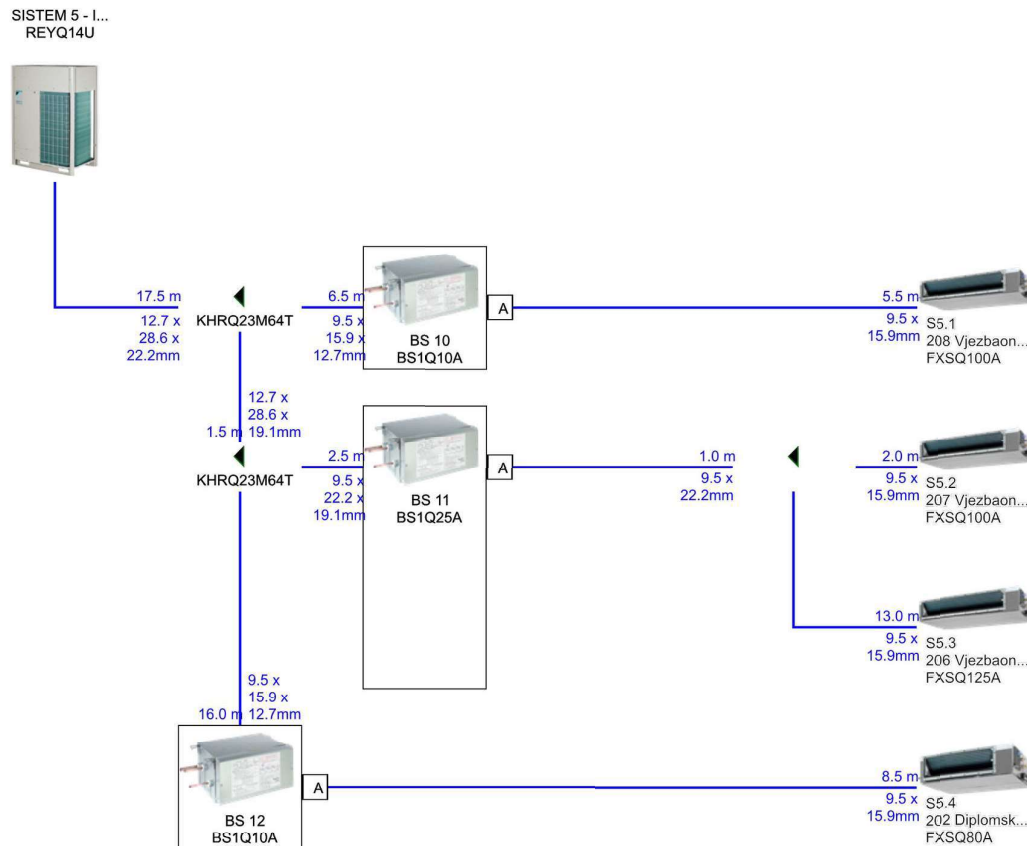
## Piping SISTEM 3 - PRIZEMLJE



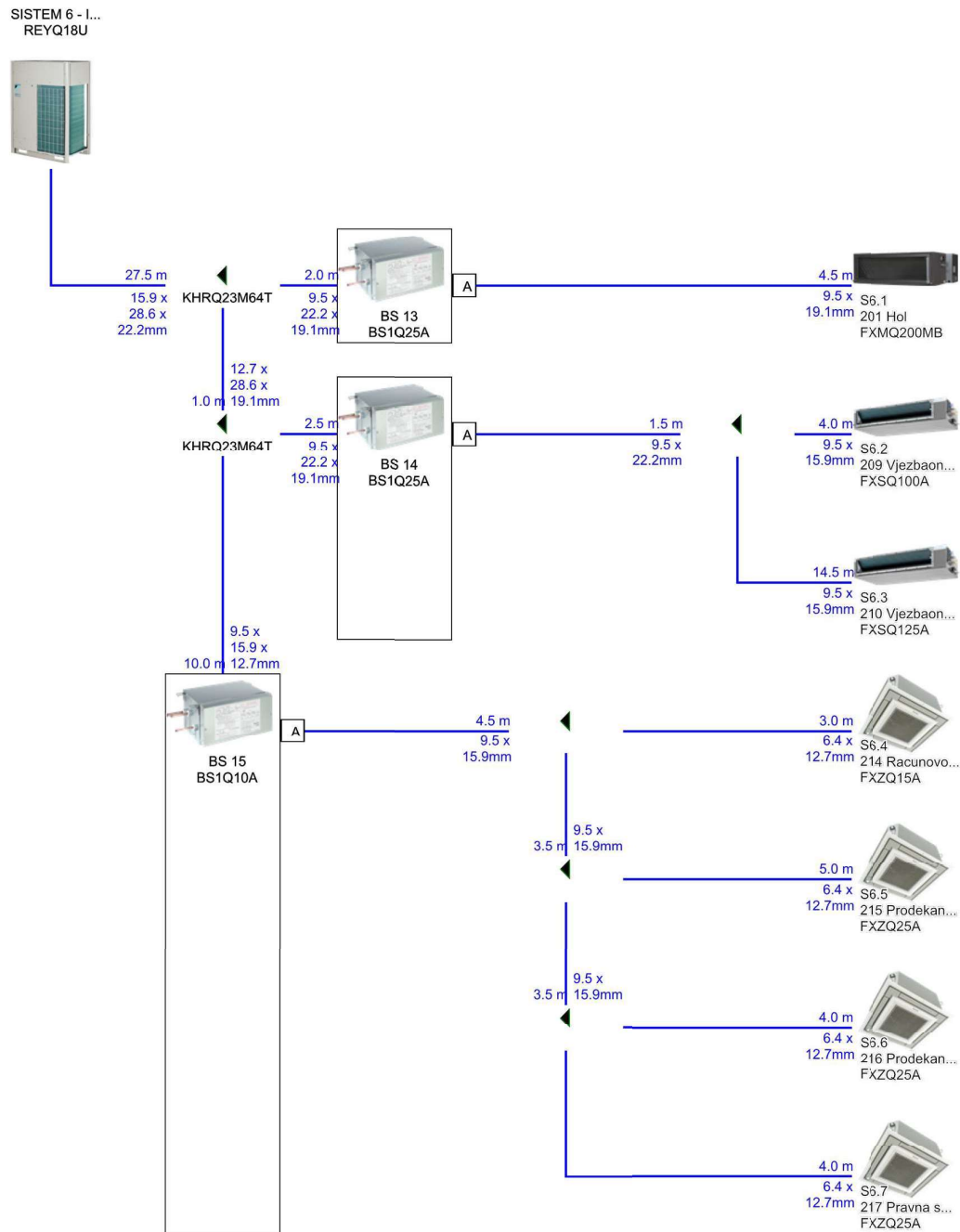
## Piping SISTEM 4 - PRIZEMLJE



## Piping SISTEM 5 - I SPRAT

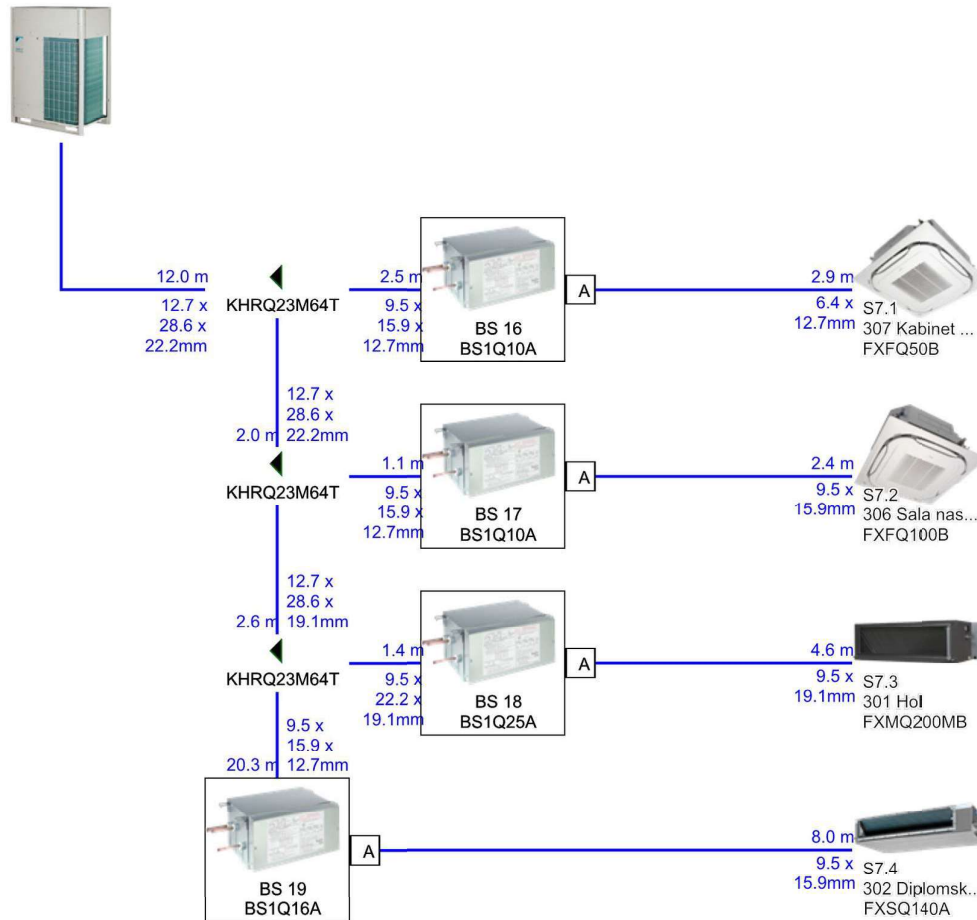


## Piping SISTEM 6 - I SPRAT

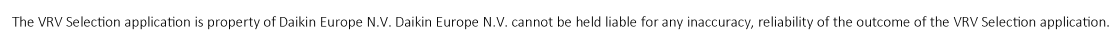


## Piping SISTEM 7 - II SPRAT

SISTEM 7 - I...  
REYQ16U







## Piping SISTEM 2 KK KLUB

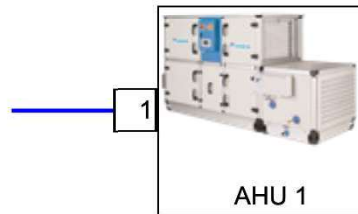
SISTEM 2 KK ...  
ERQ250AW1



9.5 x  
22.2mm



AHU 1 box 1  
EKEXV250



AHU 1

# Piping SISTEM 9-1 KK AMFITEATAR

SISTEM 9-1 K...  
ERQ200AW1



9.5 x  
19.1mm



To SISTEM 9-2 KK AMFITEATAR



## Piping SISTEM 9-2 KK AMFITEATAR

SISTEM 9-2 K...  
ERQ200AW1



To SISTEM 9-1 KK AMFITEATAR

AHU 2 box 1  
EKEXV200

9.5 x  
19.1mm AHU 2 box 2  
EKEXV200

1

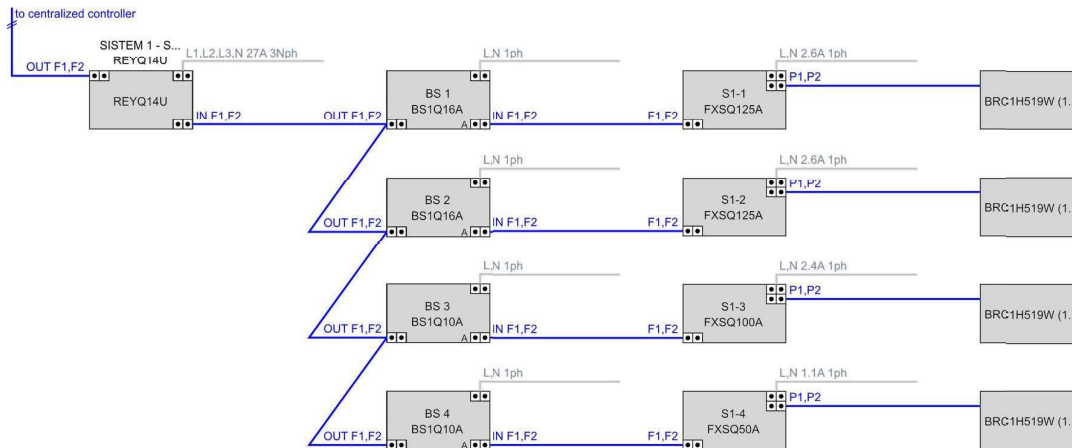
2



AHU 2

## Wiring diagrams

### Wiring SISTEM 1 - SUTEREN



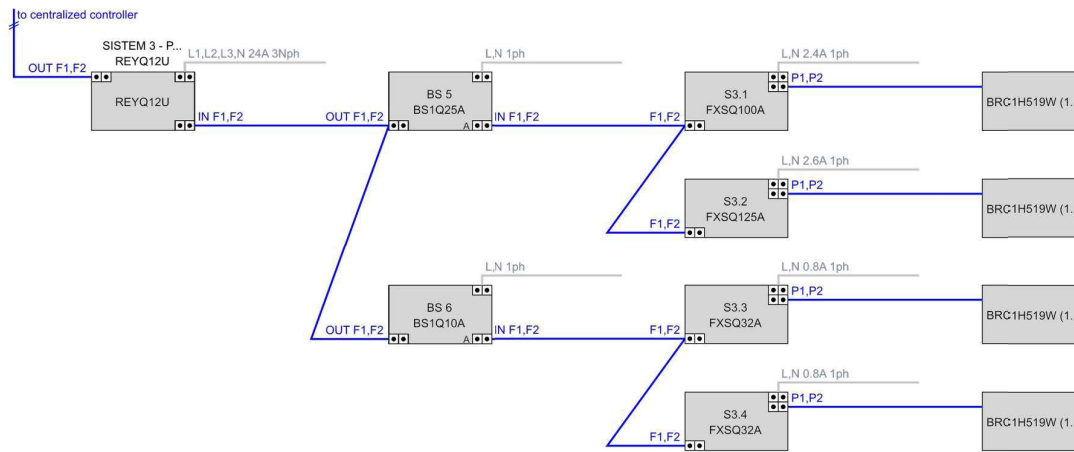
### Remarks

F1F2 = AWG 18-2 is required - however always refer to local code for further information.

P1P2 = AWG 18-2 is required - however always refer to local code for further information.



## Wiring SISTEM 3 - PRIZEMLJE



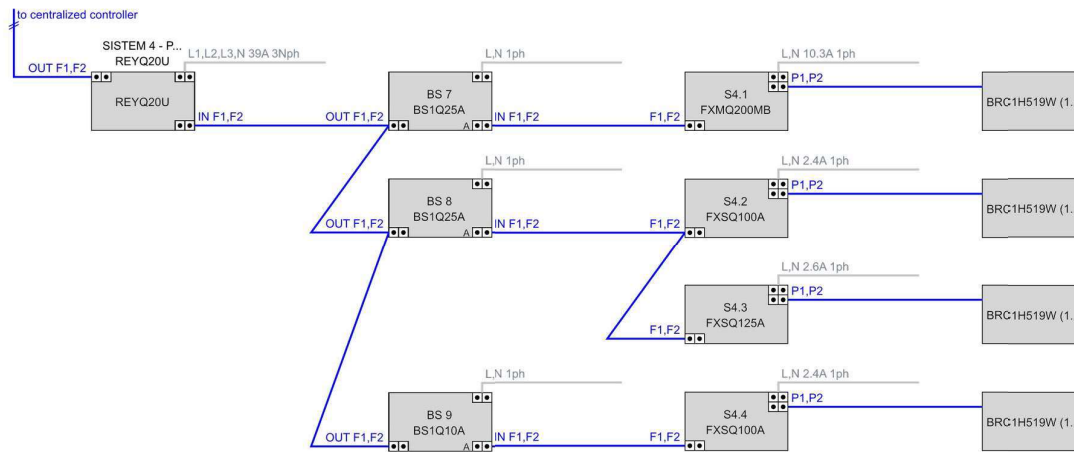
## Remarks

F1F2 = AWG 18-2 is required - however always refer to local code for further information.

P1P2 = AWG 18-2 is required - however always refer to local code for further information.



## Wiring SISTEM 4 - PRIZEMLJE



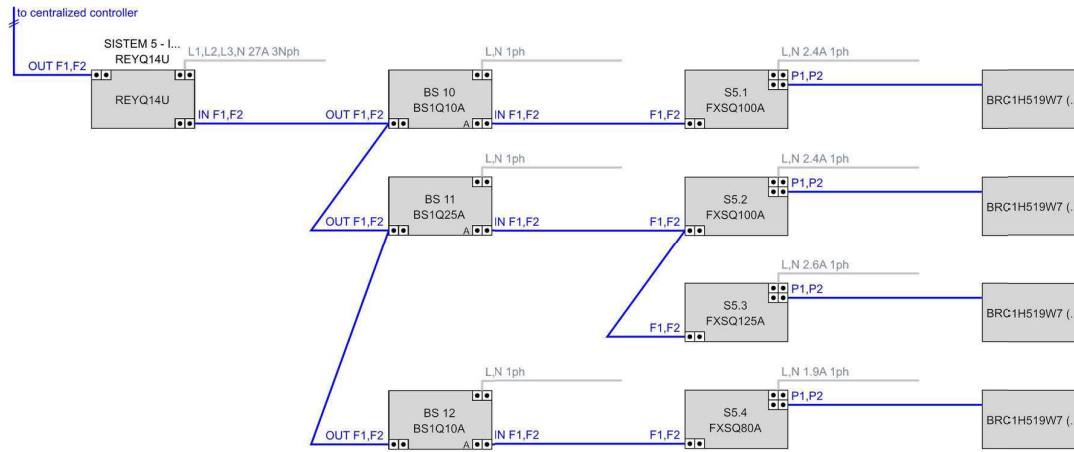
## Remarks

F1F2 = AWG 18-2 is required - however always refer to local code for further information.

P1P2 = AWG 18-2 is required - however always refer to local code for further information.



## Wiring SISTEM 5 - I SPRAT



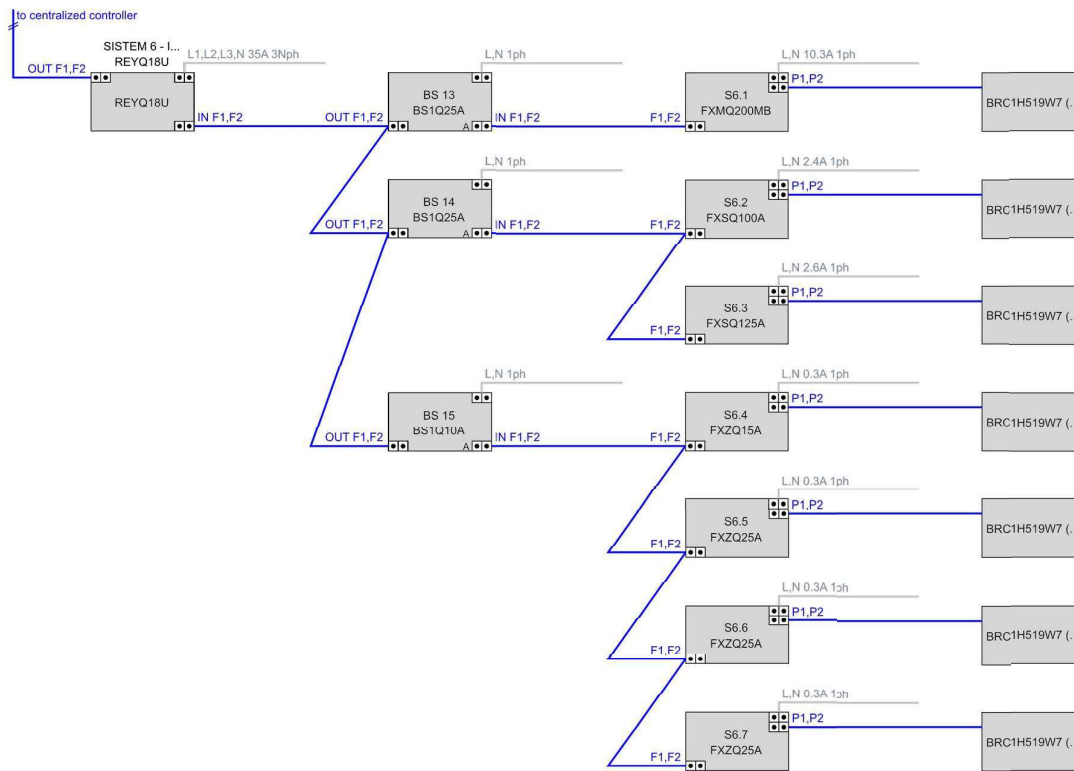
## Remarks

F1F2 = AWG 18-2 is required - however always refer to local code for further information.

P1P2 = AWG 18-2 is required - however always refer to local code for further information.



## Wiring SISTEM 6 - I SPRAT



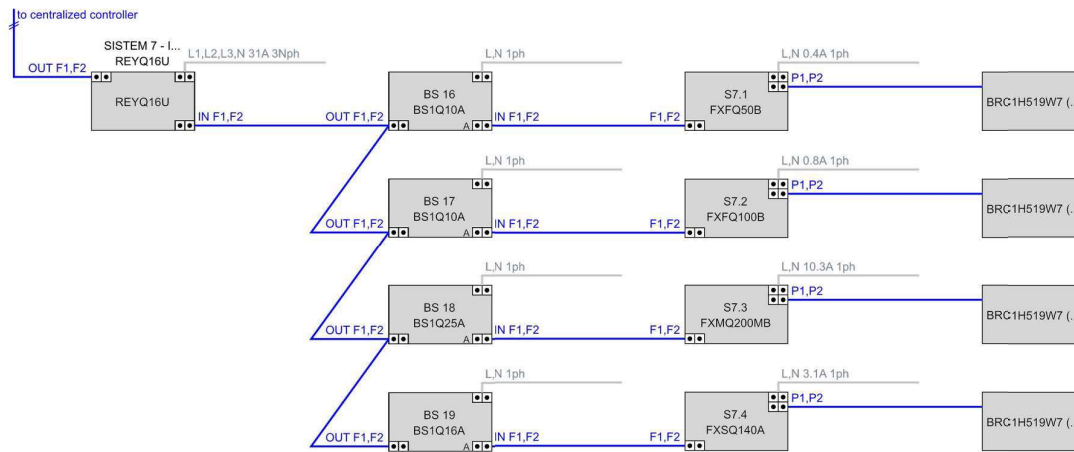
## Remarks

F1F2 = AWG 18-2 is required - however always refer to local code for further information.

P1P2 = AWG 18-2 is required - however always refer to local code for further information.



## Wiring SISTEM 7 - II SPRAT



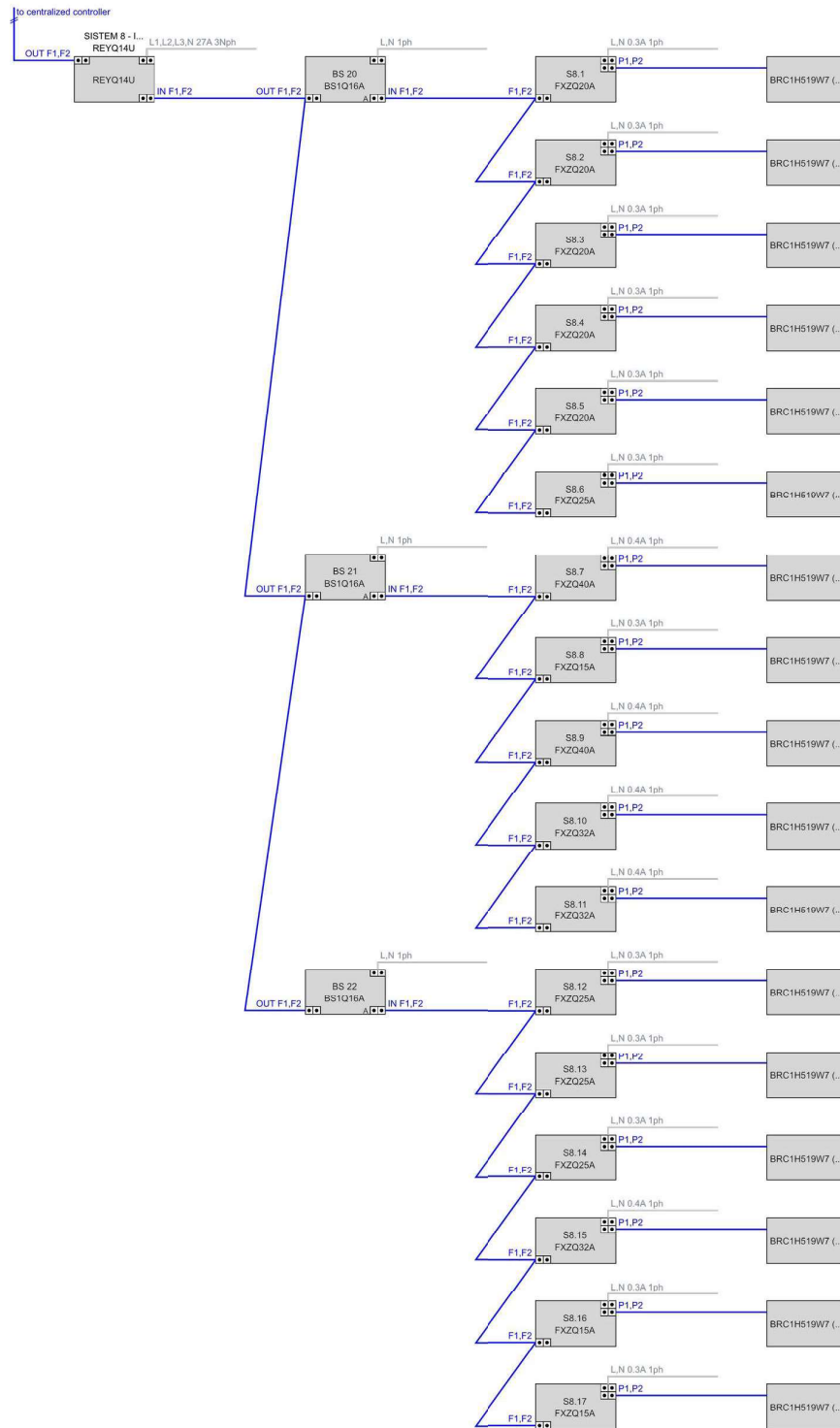
## Remarks

F1F2 = AWG 18-2 is required - however always refer to local code for further information.

P1P2 = AWG 18-2 is required - however always refer to local code for further information.



## Wiring SISTEM 8 - II SPRAT



## Remarks

F1F2 = AWG 18-2 is required - however always refer to local code for further information.

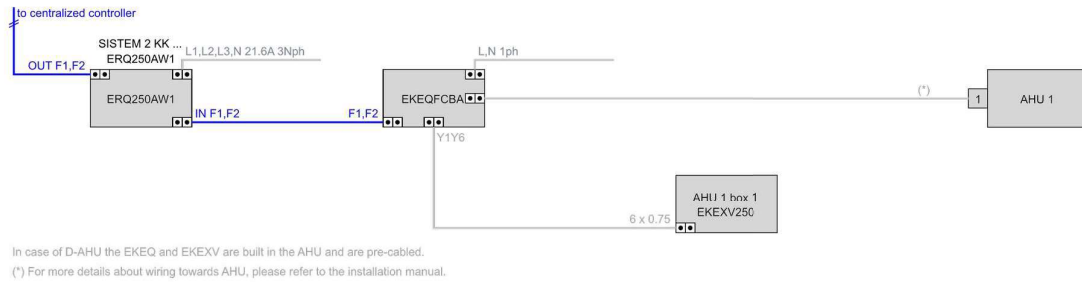
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P1P2 = AWG 18-2 is required - however always refer to local code for further information.



## Wiring SISTEM 2 KK KLUB

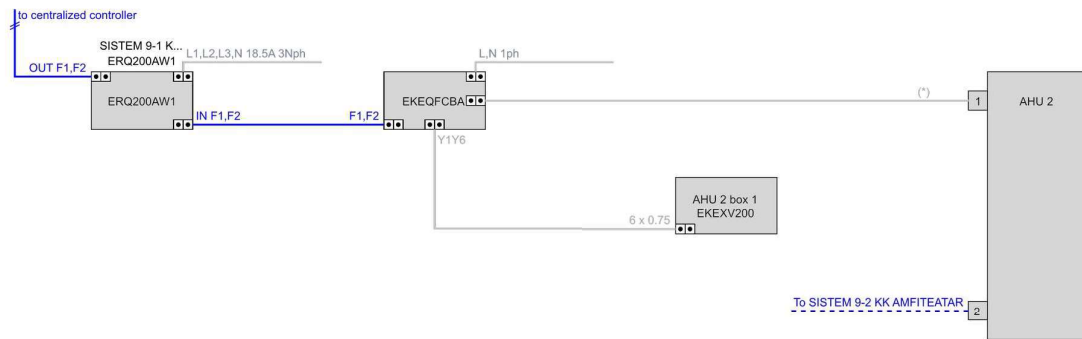


## Remarks

F1F2 = AWG 18-2 is required - however always refer to local code for further information.



## Wiring SISTEM 9-1 KK AMFITEATAR



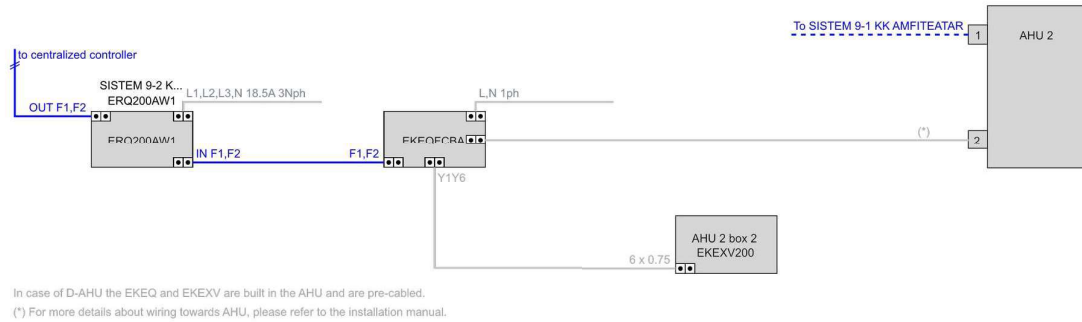
In case of D-AHU the EKEQ and EKE XV are built in the AHU and are pre-cabled.  
(\*) For more details about wiring towards AHU, please refer to the installation manual.

## Remarks

F1F2 = AWG 18-2 is required - however always refer to local code for further information.



## Wiring SISTEM 9-2 KK AMFITEATAR



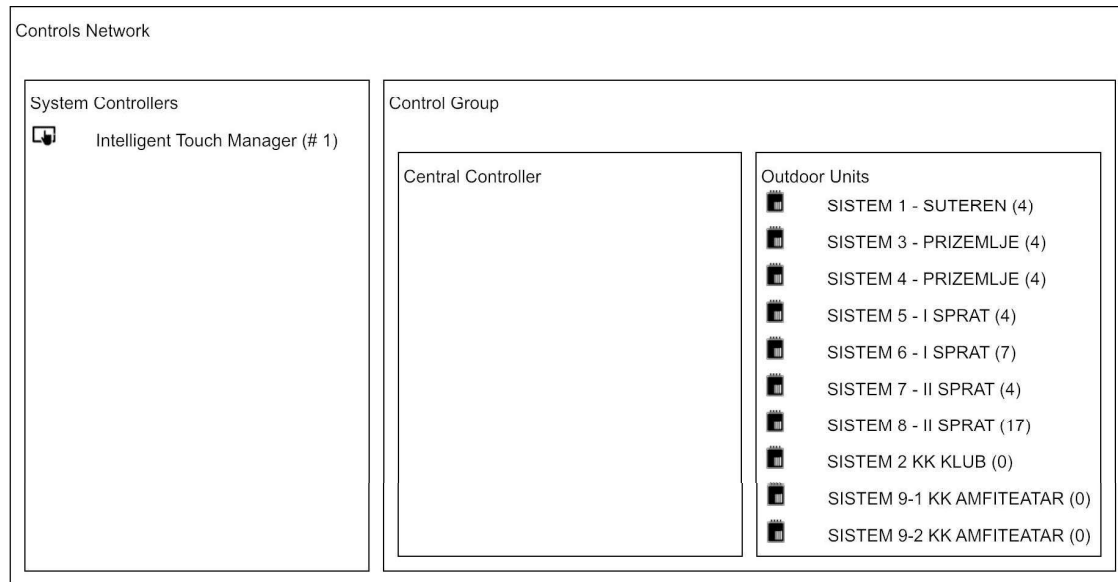
## Remarks

F1F2 = AWG 18-2 is required - however always refer to local code for further information.



## Centralized controllers

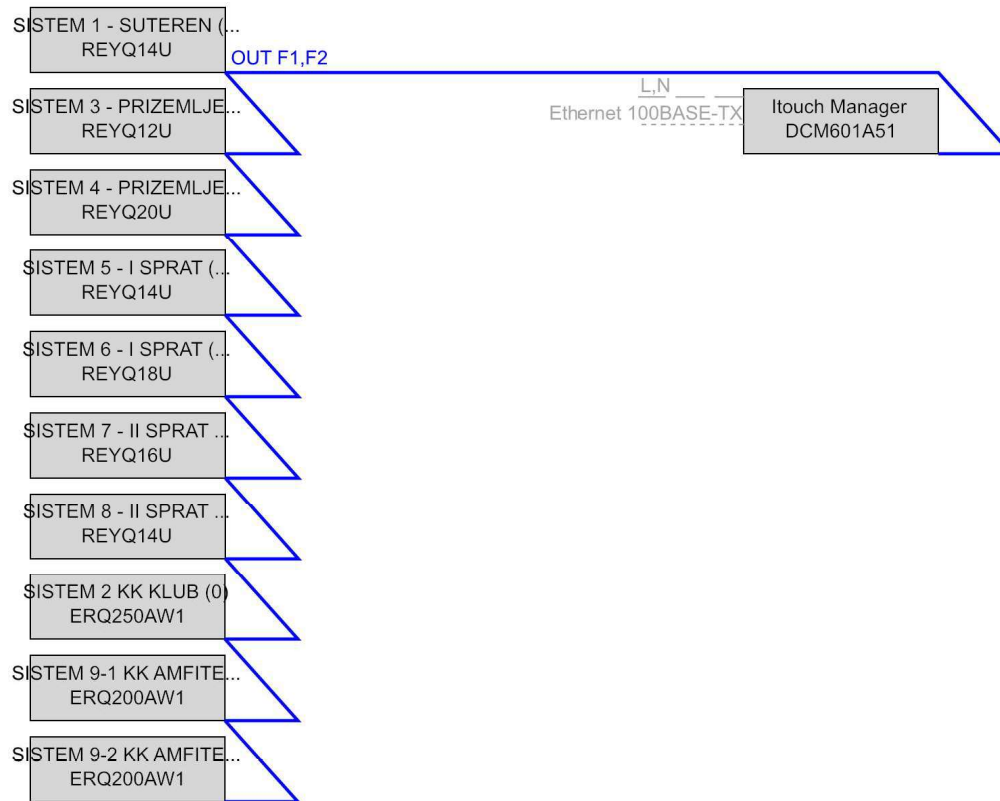
### Concept





## Controller wiring diagrams

### Control Group







## Best Practices

### Residual Current Circuit Breaker

For better protection of installations against the risk of fire, power supply of indoor and outdoor units must be protected with a Residual Current Circuit Breaker. For protection against fire, we recommend a sensitivity of 300mA. The selected RCCB should be of the type B, suitable for inverter devices and indicated by the symbols here below. Further electrical characteristics of the RCCB must be selected in accordance with local regulation.



For a complete list of all required safety precautions, warnings and attention points, please consult the “general safety precautions manual” delivered with the unit.

## **5.6. IZBOR HRV SISTEMA (REKUPERATORA)**



# 1. Specification Data

Selected ventilation device: VAM1000J, Ultra-High 14

Room Airflow Conditions	
Total supply air	1000m³/h
Total exhaust air	1000m³/h
External Static Pressure (ESP)	
Design supply ESP	150.0Pa
Design exhaust ESP	150.0Pa
Altitude Selection	
Altitude	44m

Cooling		Heating	
Room Air Conditions (RA)		Room Air Conditions (RA)	
Dry bulb temperature	26.0°C	Dry bulb temperature	20.0°C
Relative humidity	50%	Relative humidity	50%
Ambient Air Conditions (OA)		Ambient Air Conditions (OA)	
Dry bulb temperature	37.0°C	Dry bulb temperature	-4.0°C
Relative humidity	28%	Relative humidity	90%
Discharge Temperature Setting		Discharge Temperature Setting	
Temperature	18.0°C	Temperature	25.0°C
		Electric Heaters	
		Inlet heater	0.000kW

# 2. Selection Data

Ratios	
Exhaust / Supply ratio	1.00
Additional resistance	
Supply side	10.9Pa
Exhaust side	10.9Pa

Cooling		Heating	
Efficiencies		Efficiencies	
Temperature exchange efficiency	79.6%	Temperature exchange efficiency	79.6%
Enthalpy exchange efficiency	62.6%	Enthalpy exchange efficiency	68.6%
Savings over Heat Exchanger		Savings over Heat Exchanger	
Latent heat savings	0.371kW	Latent heat savings	2.208kW
Sensible heat savings	2.912kW	Sensible heat savings	4.653kW
Total heat savings	3.283kW	Total heat savings	6.862kW
Heaters		Heaters	
Switch on inlet heater above	59.5°C	Switch on inlet heater below	5.0°C
Inlet heater (user settings)		Inlet heater (user settings)	2.500kW

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Inlet heater (calculated minimum)		Inlet heater (calculated minimum)	1.648kW
		Supply heater (user settings)	
		Supply heater (calculated minimum)	

### 3. Commissioning parameters

Fan mode	
Supply	Ultra-High 14
Exhaust	Ultra-High 14
ESP data	
Supply side	10.9Pa
Exhaust side	10.9Pa

### 4. Technical data

Mechanical Data		Electrical Data	
W×H×D	1350×368×1170mm	Power supply	VE
Weight	70.0kg	Frequency	50/60Hz
Speed Related Data		Phases	1
Sound level		Voltage	220V
Current		Min~max V	220~240
Wattage		MCA	4.9A
Ambient Operation Range		MFA	16.0A
Min~max temperature	-10.0~46.0°C	RLA	
Maximum relative humidity	80%	FLA	
Heater Threshold Temperature		Duct Data	
Minimum temperature	-10.0°C	Duct diameter	250mm
Room Operation Range		Relative Humidity Maxima	
Min~max temperature	0.0~40.0°C	Exhaust air (EA)	95%
Maximum relative humidity	80%	Ventilation out air (VO)	95%

### 5. Psychrometric Points

Cooling			
Room Air (RA)		Exhaust Air (EA)	
Dry bulb temperature	26.0°C	Dry bulb temperature	34.8°C
Wet bulb temperature	18.6°C	Wet bulb temperature	20.9°C
Relative humidity	50.0%	Relative humidity	29.0%
Absolute humidity	0.0106kg/kg	Absolute humidity	0.0101kg/kg
Enthalpy	53.1kJ/kg	Enthalpy	60.9kJ/kg
Outdoor Air (OA)		Supply Air (SA)	
Dry bulb temperature	37.0°C	Dry bulb temperature	28.2°C
Wet bulb temperature	22.2°C	Wet bulb temperature	20.0°C
Relative humidity	28.0%	Relative humidity	47.7%

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Absolute humidity	0.0110kg/kg	Absolute humidity	0.0115kg/kg
Enthalpy	65.6kJ/kg	Enthalpy	57.7kJ/kg
<b>Ventilation In (VI)</b>		<b>Ventilation Out (VO)</b>	
Dry bulb temperature	37.0°C	Dry bulb temperature	28.2°C
Wet bulb temperature	22.2°C	Wet bulb temperature	20.0°C
Relative humidity	28.0%	Relative humidity	47.7%
Absolute humidity	0.0110kg/kg	Absolute humidity	0.0115kg/kg
Enthalpy	65.6kJ/kg	Enthalpy	57.7kJ/kg

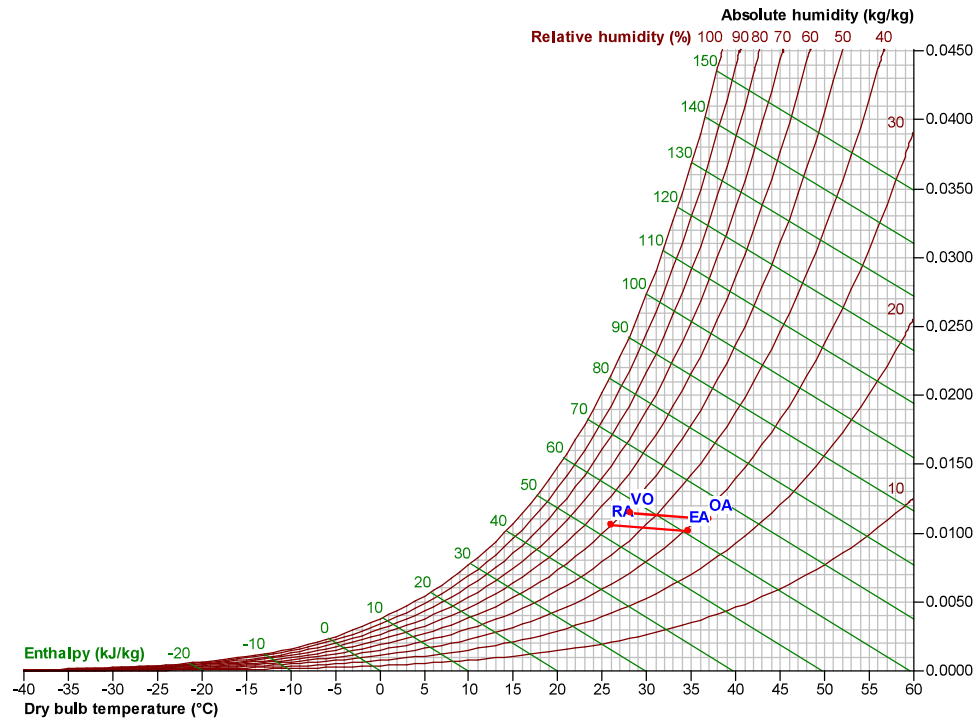
Heating			
Room Air (RA)		Exhaust Air (EA)	
Dry bulb temperature	20.0°C	Dry bulb temperature	6.3°C
Wet bulb temperature	13.7°C	Wet bulb temperature	4.8°C
Relative humidity	50.0%	Relative humidity	79.7%
Absolute humidity	0.0073kg/kg	Absolute humidity	0.0047kg/kg
Enthalpy	38.6kJ/kg	Enthalpy	18.3kJ/kg
Outdoor Air (OA)		Supply Air (SA)	
Dry bulb temperature	-4.0°C	Dry bulb temperature	16.5°C
Wet bulb temperature	-4.4°C	Wet bulb temperature	10.0°C
Relative humidity	90.0%	Relative humidity	43.1%
Absolute humidity	0.0024kg/kg	Absolute humidity	0.0050kg/kg
Enthalpy	2.1kJ/kg	Enthalpy	29.3kJ/kg
Ventilation In (VI)		Ventilation Out (VO)	
Dry bulb temperature	2.8°C	Dry bulb temperature	16.5°C
Wet bulb temperature	-0.3°C	Wet bulb temperature	10.0°C
Relative humidity	52.6%	Relative humidity	43.1%
Absolute humidity	0.0024kg/kg	Absolute humidity	0.0050kg/kg
Enthalpy	9.0kJ/kg	Enthalpy	29.3kJ/kg

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## 6. Psychrometric Diagram

### 6.1. Cooling

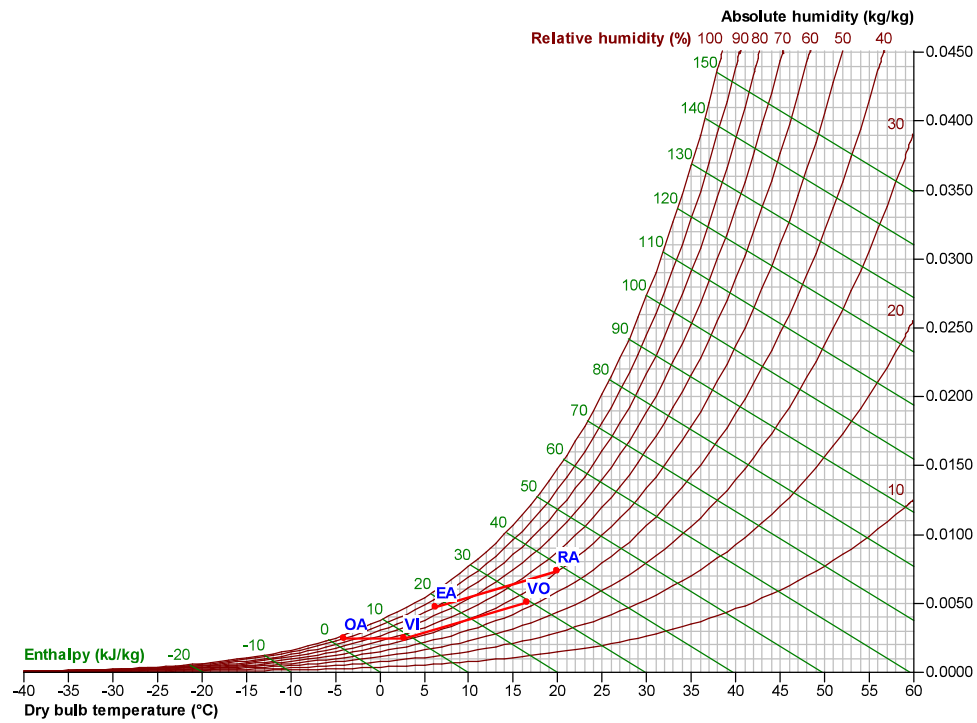


This Ventilation Xpress is property of Daikin Europe NV, Daikin Europe NV cannot be held liable for any inaccuracy, reliability of the outcome of this program.





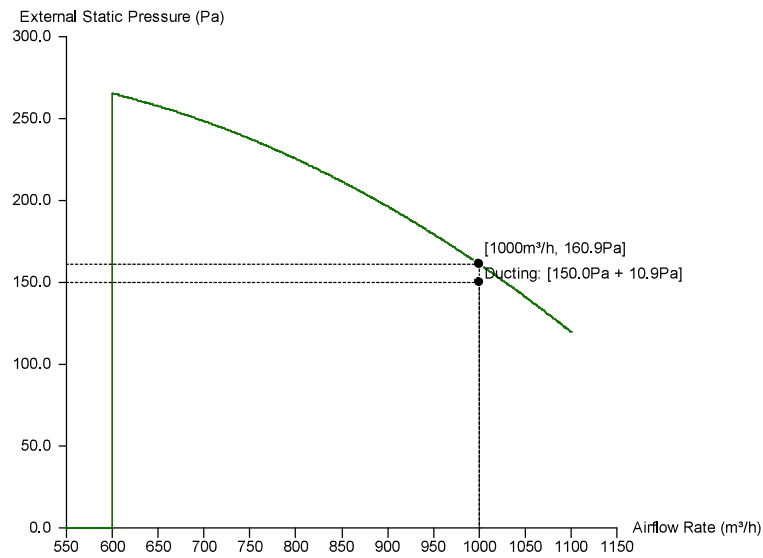
## 6.2. Heating



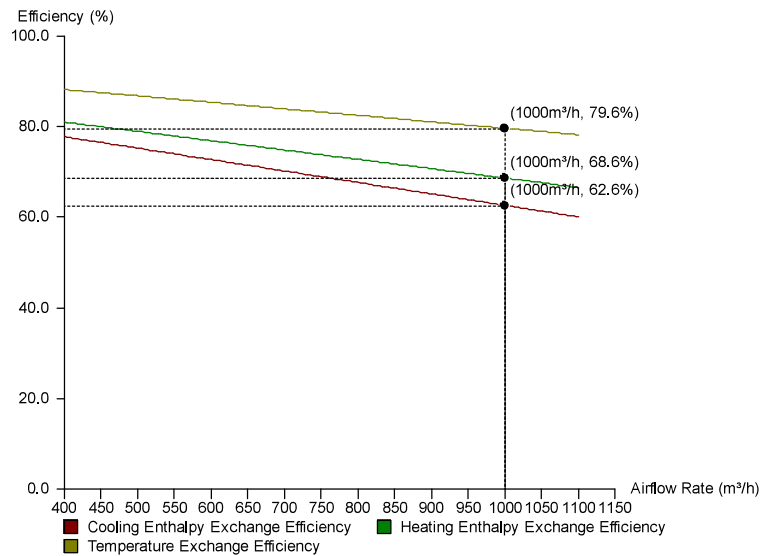
This Ventilation Xpress is property of Daikin Europe NV, Daikin Europe NV cannot be held liable for any inaccuracy, reliability of the outcome of this program.



## 7. Fan Characteristics

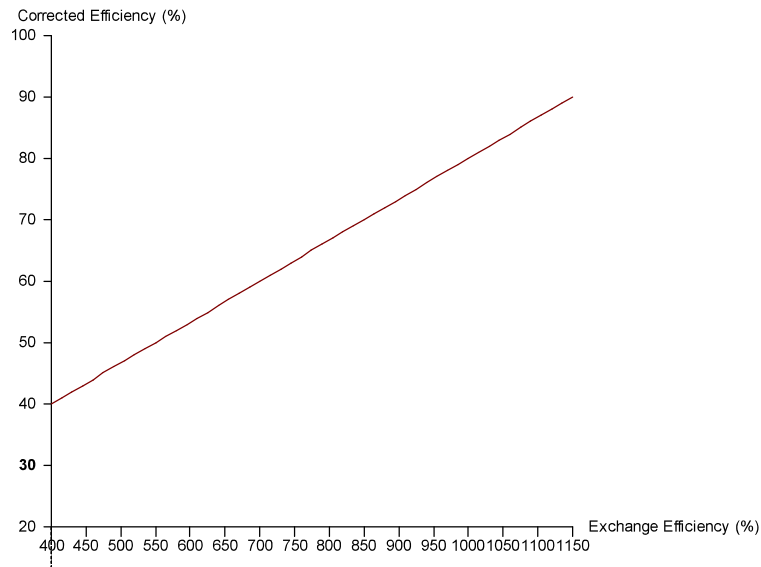


## 8. Efficiency Data

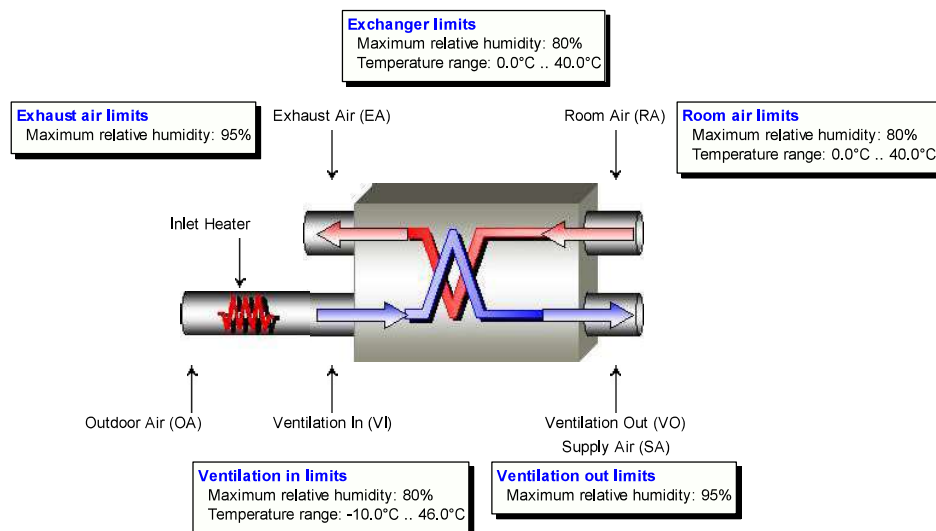


This Ventilation Xpress is property of Daikin Europe NV, Daikin Europe NV cannot be held liable for any inaccuracy, reliability of the outcome of this program.

## 9. Corrected Efficiency Data



## 10. Configuration Data



The minimum ventilation in temperature is -10.0°C. However, below -10.0°C, an inlet heater will be selected to avoid an intermittent operation and make sure the supply air fan operates continuously.

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## **5.7. IZBOR VENTILATORA**

## CBF 100LS BATHROOM FAN

Item no. **5959**

Version: 50 Hz

Document type: **Product card**  
Document date: **2019-07-09**  
Generated by: **Systemair Online Catalogue**

### Description

- BF axial fan for bathrooms
- CBF centrifugal fan for bathrooms, toilets and store rooms
- Both types can be installed on the wall or the ceiling

The BF/CBF units are extraction fans manufactured from ABS plastic. These fans, can be connected either through the light switch, so that they start when the light is turned on, or to a separate switch. The CBF has a spring-loaded back draft damper.

There are three models: standard model (S), a model with timer (T) and a model with timer and humidity sensor (TH). A time delay of between 1 and 20 minutes can be set on the timer after removing the unit's front cover. The humidity sensor can be set to a value between 40 and 95% relative humidity. The BF fan has an adjustment knob that is easily accessible at the bottom of the fan. To adjust the humidity sensor on the CBF fan, the front cover should be removed first.

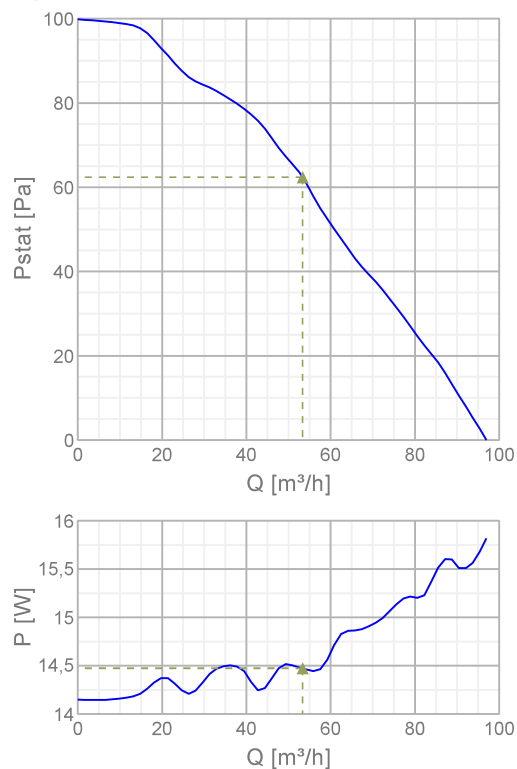


### Technical parameters

Nominal data		
Voltage	230	V
Frequency	50	Hz
Phase	1	~
Input power (P1)	15,8	W
Current	0,104	A
Max. airflow	96,8	m³/h
Fan impeller speed	2233	r.p.m.
Weight	1,2	kg
Temperature data		
Max. temperature of transported air	70	°C
Max. temperature of transported air when voltage-controlled	70	°C
Sound data		
Sound pressure level at 3 m (20m² Sabin)	51	dB(A)
Protection / Classification		
Insulation class	B	
Enclosure class, motor	-	

## Performance

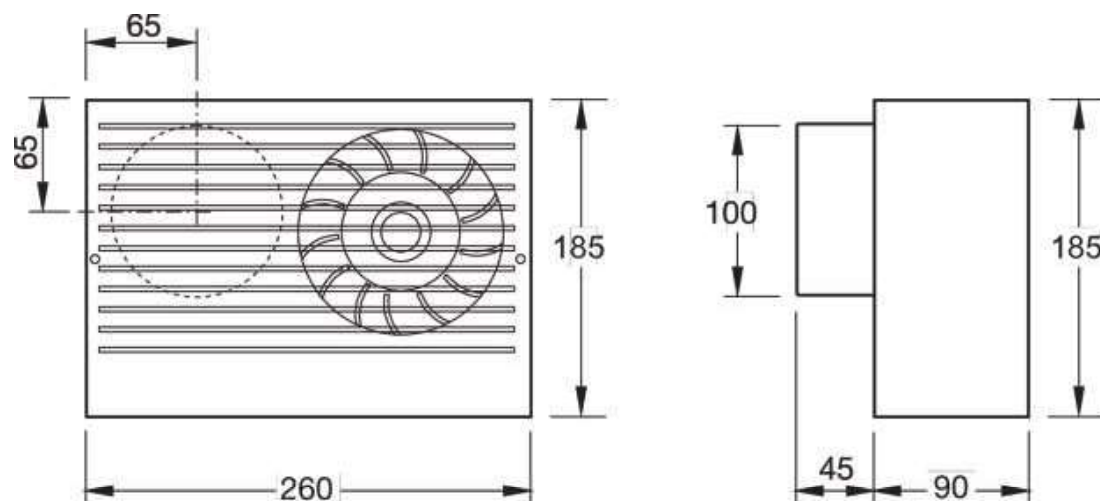
### Diagrams



### Max efficiency

Hydraulic data										
▲ Working air flow	53,3 m³/h									
▲ Working static pressure	62,4 Pa									
▲ Power	14,5 W									
Speed	2452 r.p.m.									
Current	0,0977 A									
SFP	0,977 kW/(m³/s)									
Voltage	230 V									
Sound power level		63	125	250	500	1k	2k	4k	8k	Tot
Inlet	dB(A)	19	34	54	52	51	46	40	30	58

## Dimensions



## Accessories

### Accessories

[BVK 100 Wall vent kit \(5965\)](#)

## Documentation



CBF100\_IMO\_SE,GB,FR,\_DE.pdf (472,22kB)



Decl.of Conformity CBF.pdf (521,32kB)

## Specification text

# PRIO 200EC CIRC. DUCT FAN

Item no. 78186

Document type: Product card  
Document date: 2019-06-25  
Generated by: Systemair Online Catalogue



## Description

- EC-motors, high level of efficiency
- Low SFP values
- 100% speed controllable
- Integrated motor protection
- Can be installed in any position
- Compact design
- Low sound level
- Potentiometer included for ease of commissioning

EC fans are intelligent devices using integrated motor electronics, ensuring that the motor always runs at optimal load. With EC motors the proportion of energy utilized effectively is higher, which as a result reduces the energy usage considerably, compared with AC motors.

Another special feature of EC fans is their energy-saving potential not only at full load, but especially when speed controlled, i.e. at part load. When operating at part load, the energy used is much lower than with an asynchronous motor of equivalent output.

Reduced energy usage guarantees a drop in operating costs.

The prioAir series is designed for installation in ducts. The prioAir models have 25 mm long spigot connections in acc. with EN 1506:1997. The fans have aerodynamically optimized impellers and guide vanes. Motor protection is integrated in the electronics of the motor. The air tight casing (tightness class C in acc. with EN12237:2003) is manufactured from special composite material.

The mounting clamp facilitates easy installation and removal, and prevents the transfer of vibrations to the duct. Mounting bracket to the wall or ceiling as accessory.

For installation in damp locations we recommend to use a run-on timer. The fans are delivered with a pre-wired potentiometer (0-10 V) that allows you to easily find the required working point.



## Technical parameters

Nominal data		
Voltage	230	V
Frequency	50/60	Hz
Phase	1	~
Input power (P1)	117	W
Current	0,921	A
Max. airflow	1318	m³/h
Fan impeller speed	3463	r.p.m.
Weight	2,4	kg
Temperature data		
Max. temperature of transported air	55	°C
Sound data		
Sound pressure level at 3 m (20m² Sabin)	52	dB(A)



## Protection / Classification

Insulation class

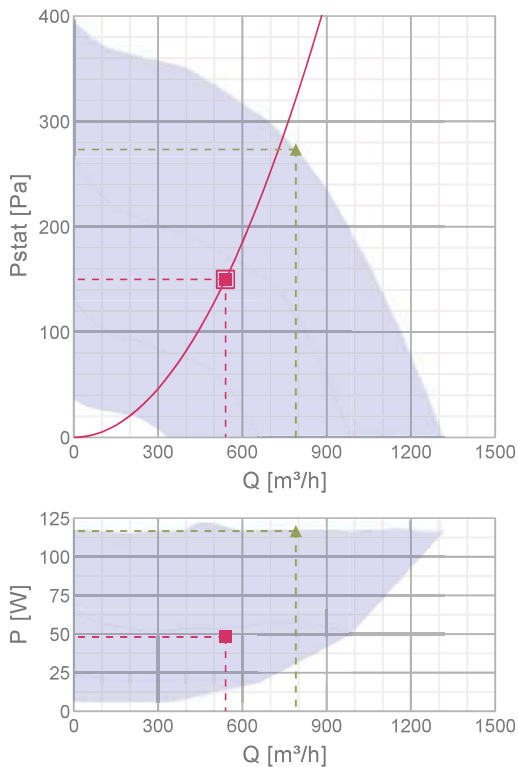
B

Enclosure class, motor

IP44

## Performance

### Diagrams



### Selection

#### Hydraulic data

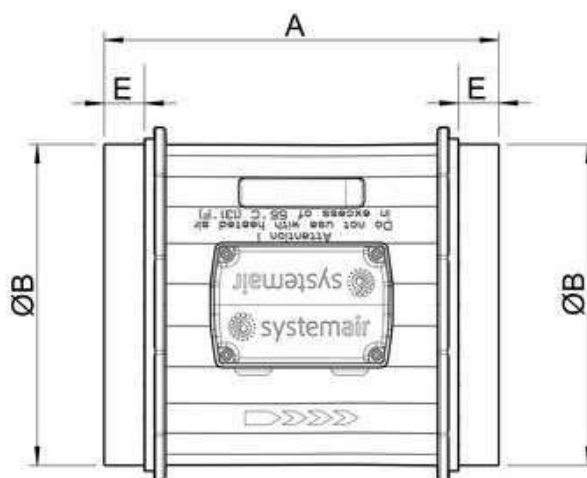
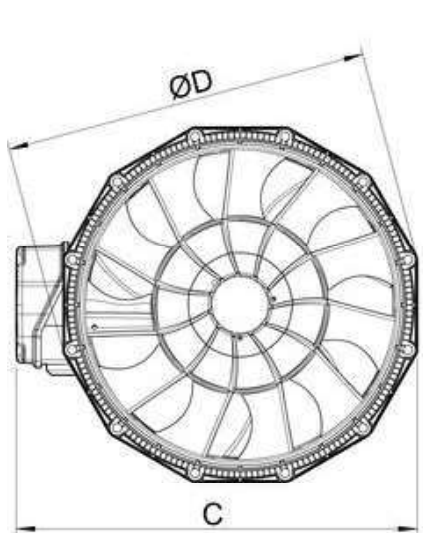
<input type="checkbox"/> Required air flow	540 m³/h
<input type="checkbox"/> Required static pressure	150 Pa
<input checked="" type="checkbox"/> Working air flow	540 m³/h
<input checked="" type="checkbox"/> Working static pressure	150 Pa
<input checked="" type="checkbox"/> Power	48 W
Speed	2582 r.p.m.
Current	0,384 A
SFP	0,32 kW/(m³/s)
Voltage	230 V

Sound power level		63	125	250	500	1k	2k	4k	8k	Tot
Inlet	dB(A)	39	51	64	62	64	60	55	45	69
Outlet	dB(A)	36	51	56	59	60	56	52	45	65
Surrounding	dB(A)	6	25	33	45	47	44	36	21	50

## Max efficiency

Hydraulic data										
▲ Working air flow										790 m <sup>3</sup> /h
▲ Working static pressure										273 Pa
▲ Power										117 W
Speed										3512 r.p.m.
Current										0,91 A
SFP										0,531 kW/(m <sup>3</sup> /s)
Voltage										230 V
Sound power level		63	125	250	500	1k	2k	4k	8k	Tot
Inlet	dB(A)	45	54	70	71	73	69	64	56	77
Outlet	dB(A)	43	54	58	67	68	65	61	56	72
Surrounding	dB(A)	13	27	38	52	56	53	45	32	59

## Dimensions

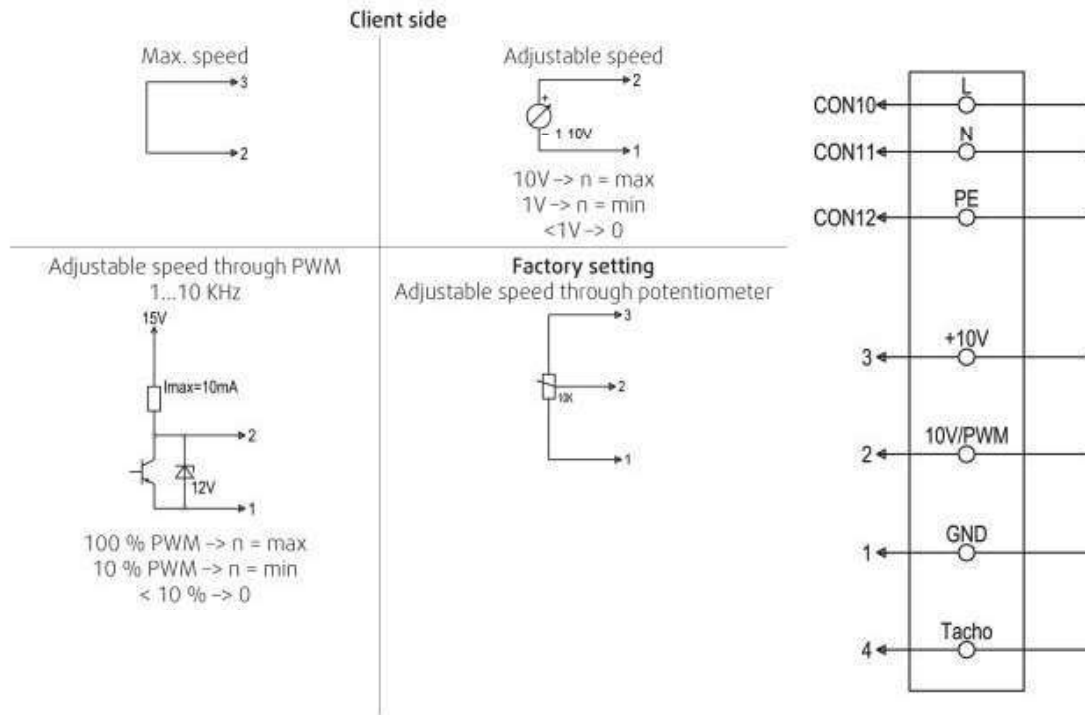


	A	øB	C	øD	E
prio 200	245	199	249	227	25

## Wiring

### 9.3.1.1 Wiring diagram prioAir EC

The fans are delivered with a pre-wired potentiometer (0–10 V)



Wire no.	Connection	Color	Function/assignment
CON10	L	black or brown	Power supply 230 V AC, 50...60 Hz, see name plate for voltage range
CON11	N	blue	Neutral conductor
CON12	PE	green/yellow	Protective conductor
1	GND	blue	GND-connection of the controller interface
2	0...10 V PWM	yellow	Controller input 0...10 V or PWM
3	10 V	red	Voltage output 10 V / Short-circuit-proof power supply for external devices (e.g. poti) prioAir 150EC, prioAir 160EC → I <sub>max</sub> =1.1mA prioAir 200ECprioAir 250EC → I <sub>max</sub> =10mA
4	Tacho	white	Speed output: Open Collector, 1 impulse per revolution, electrically isolated, I <sub>sink_max</sub> = 10 mA

## Accessories

### Electric accessories

[RT 0-30 Room Thermostat \(5151\)](#)  
[CO2RT-R-D Transmitter \(6993\)](#)  
[Presence detector/IR24-P \(6995\)](#)  
[MTV-1/010 Controller 0...10V+ \(30650\)](#)  
[MTP 10, 10K, Speed control \(32731\)](#)  
[EC-Vent Room Unit \(3018\)](#)  
[EC-Vent control board \(3115\)](#)  
[REV-3POL/03 ON/OFF \(33978\)](#)  
[MTP 20, on/off, 3-step \(310220\)](#)  
[EC-Basic-H humidity \(24807\)](#)  
[EC-Basic-T temperature \(24805\)](#)  
[EC-Basic-U universal 0-10V \(24806\)](#)  
[EC-Basic-CO2 and temperature \(24808\)](#)  
[CXE/AVC Modbus \(37256\)](#)

## Accessories

[CB 200/S1/3.0KW 400V/2Duct hea \(5294\)](#)  
[CB 200-3.0 230V/1 Duct heater \(5370\)](#)  
[CB 200-5.0 400V/2 Duct heater \(5371\)](#)  
[CB 200-2.1 230V/1 Duct heater \(5384\)](#)  
[CBM 200-5.0 400V/2 Duct heater \(5483\)](#)  
[VBF 200 Water heating battery \(1732\)](#)  
[CWK 200-3-2.5 Duct cooler.circ \(30023\)](#)  
[VBC 200-2 Water heating batt \(5459\)](#)  
[LDC 200-600 Silencer \(5194\)](#)  
[LDC 200-900 Silencer \(5195\)](#)  
[FFR 200 Filter cassette \(1773\)](#)  
[FGR 200 Filter cassette \(1812\)](#)  
[FK 200 Fast clamp \(1611\)](#)  
[VKK-200 Back draft damper \(1626\)](#)  
[IGK-200 Wall Grid \(1633\)](#)  
[RSK-200 Back draft damper \(5602\)](#)  
[SG 200 Protection guard \(5609\)](#)  
[VBC 200-3 Water heating batt \(9841\)](#)  
[LDC 200-300 Silencer \(53369\)](#)  
[prio 200 mount, bracket compl. \(79315\)](#)

## Documentation



manual\_prioair\_en\_[006].pdf (7,45MB)



eu declaration of conformity\_prio\_en\_001.pdf (47,97kB)



prio\_air200\_o\_rahmen.dxf (5,47MB)

## Specification text

.

## MTP 10, 10K, SPEED CONTROL

Item no. 32731

Document type: Product card  
Document date: 2019-06-25  
Generated by: Systemair Online Catalogue

### Description

Potentiometer 10kΩ for speed controlling  
- Combined flush or surface mounting

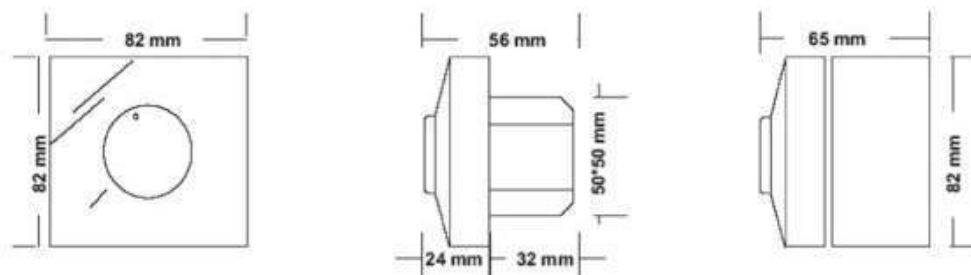
For the manual control of speed and air flow of electrical fans with 0-10V output. The jetproof IP 54 enclosure is achieved with the included surface mounting case. (Flush-mounting without the surface mounting case, gives a splash proof IP 44 enclosure also suitable for highly demand environments as bathrooms etc).




### Technical parameters


Default group	
Control signal	0...10 kOhm
Endosure class	IP44
Voltage supply	10 V DC
Rangeability	0...10 V
Contact	1 NO
Switching capacity	4A / 250V
Dimension	
Weight	0,2 kg

### Dimensions

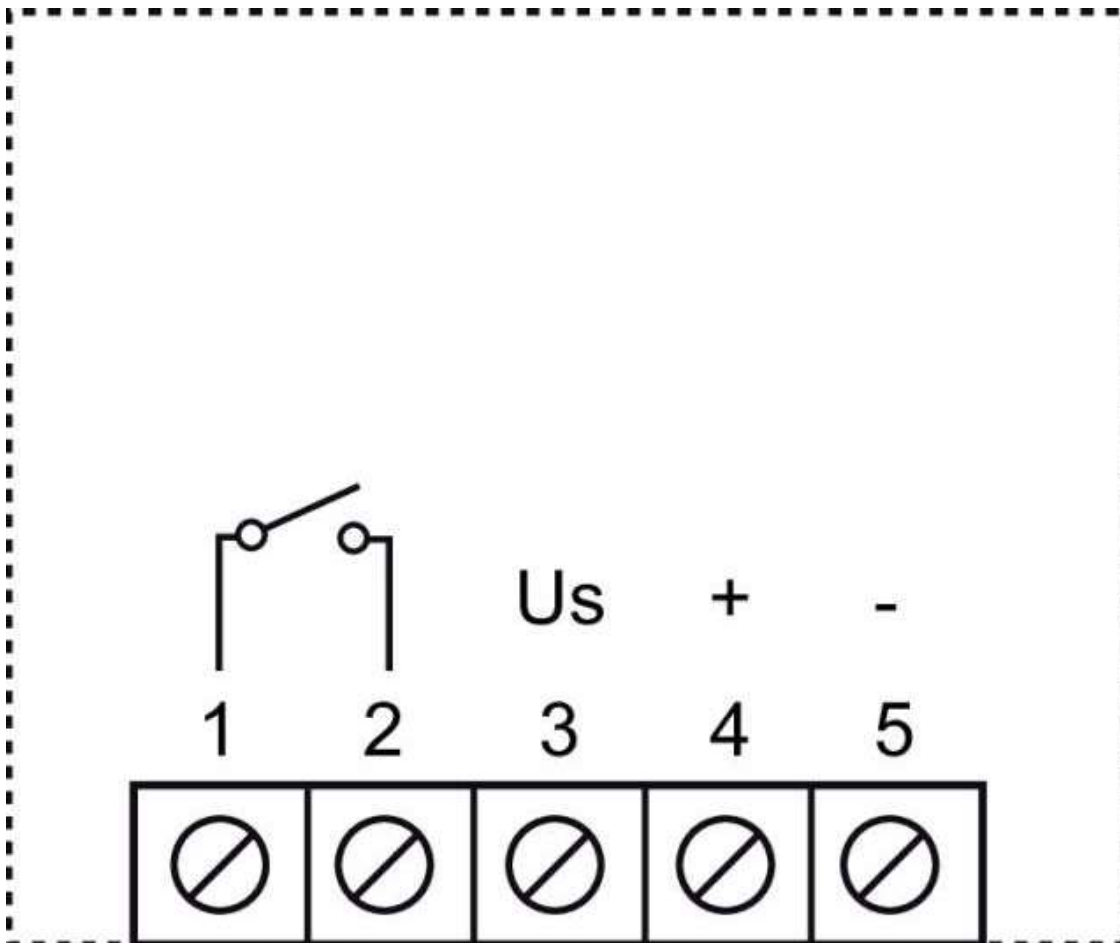


## Documentation

 MTP-Declaration of conformity.pdf (291,60kB)

 ds\_mtp010.pdf (156,06kB)

## Wiring

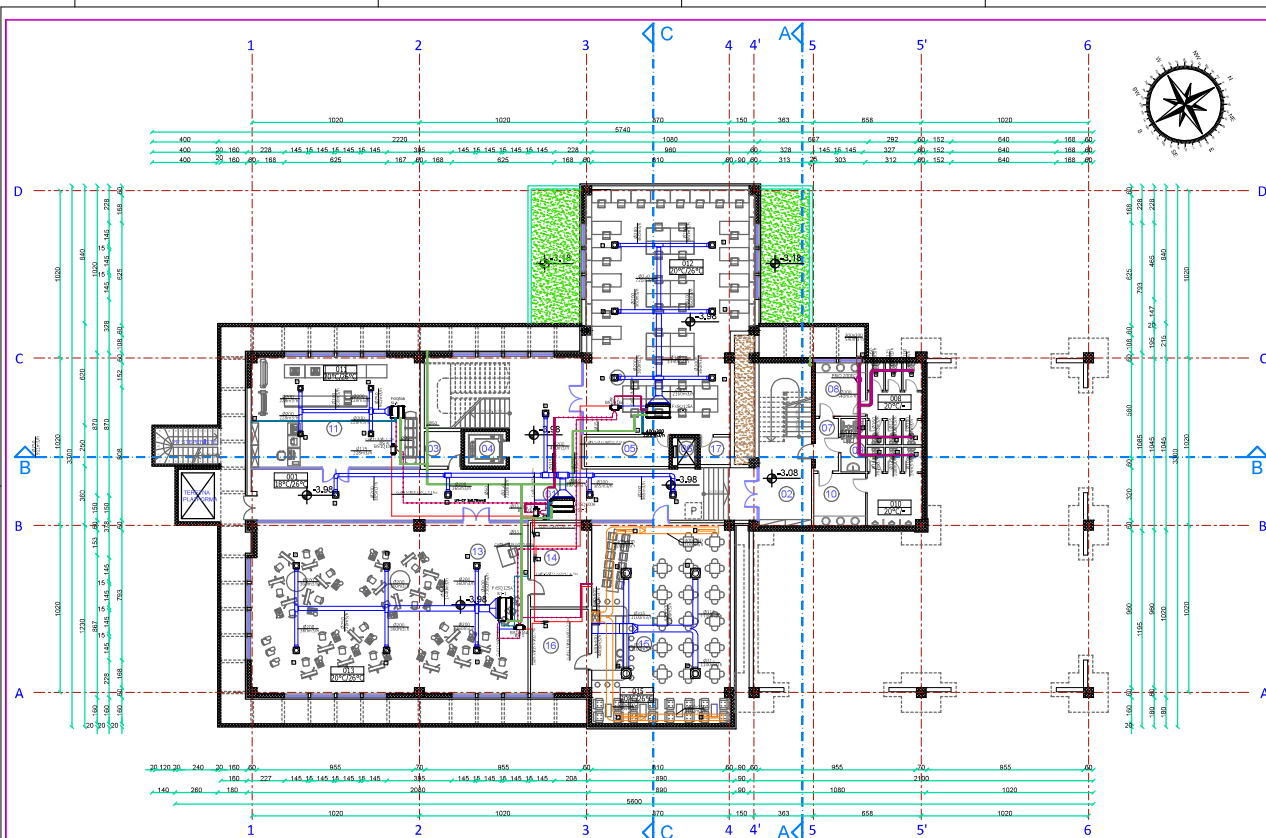


Us = 10V Supply

+ = 0-10V Output signal

- = GND

## E) GRAFIČKA DOKUMENTACIJA



PREGLED NETO I BRUTO PLOŠTINA SUTERENA									
01. HOL SA STEPENOSTEM	146,11m <sup>2</sup>	01. TOALET ZENSKI KLUB	25,25m <sup>2</sup>	103. ZAKUPNO NETO P. SUTERENA	735,42m <sup>2</sup>	UKUPNO BRUTO P. POSTOJEĆEG SUTERENA	105,40m <sup>2</sup>		
02. HODNIK SA STEPENOSTEM	3,14m <sup>2</sup>	02. TOALET ZA MUŠKARCE	4,05m <sup>2</sup>	16. OSTAVA - KAFERA	17,02m <sup>2</sup>				
03. OŠTARA SA POSTELJAKOM	4,72m <sup>2</sup>	03. TOALET ZA MUŠKARCE	4,05m <sup>2</sup>	17. RECK OŠTARA	3,08m <sup>2</sup>				
04. PLET ZA STUDENTE	9,25m <sup>2</sup>	11. STAMPAIONA I KOPIRIONA	61,76m <sup>2</sup>			UKUPNO NETO P. OBJEKTA	3705,27m <sup>2</sup>		
05. OSTAVA	9,37m <sup>2</sup>	12. MODERNA KLUBA	143,78m <sup>2</sup>			UKUPNO BRUTO P. POSTOJEĆEG SUTERENA	766,71m <sup>2</sup>		
06. PLET ZA OSOBE	2,65m <sup>2</sup>	13. VEŠERANJENSKA GALA	174,15m <sup>2</sup>			UKUPNO BRUTO P. PUNJANJAKA OBJEKTA	1024,20m <sup>2</sup>		
07. PROJEKCIOR TOAleta	4,60m <sup>2</sup>	14. OSTAVA UZ SALU	12,88m <sup>2</sup>			UKUPNO BRUTO P. PUNJANJAKA OBJEKTA	3449,50m <sup>2</sup>		

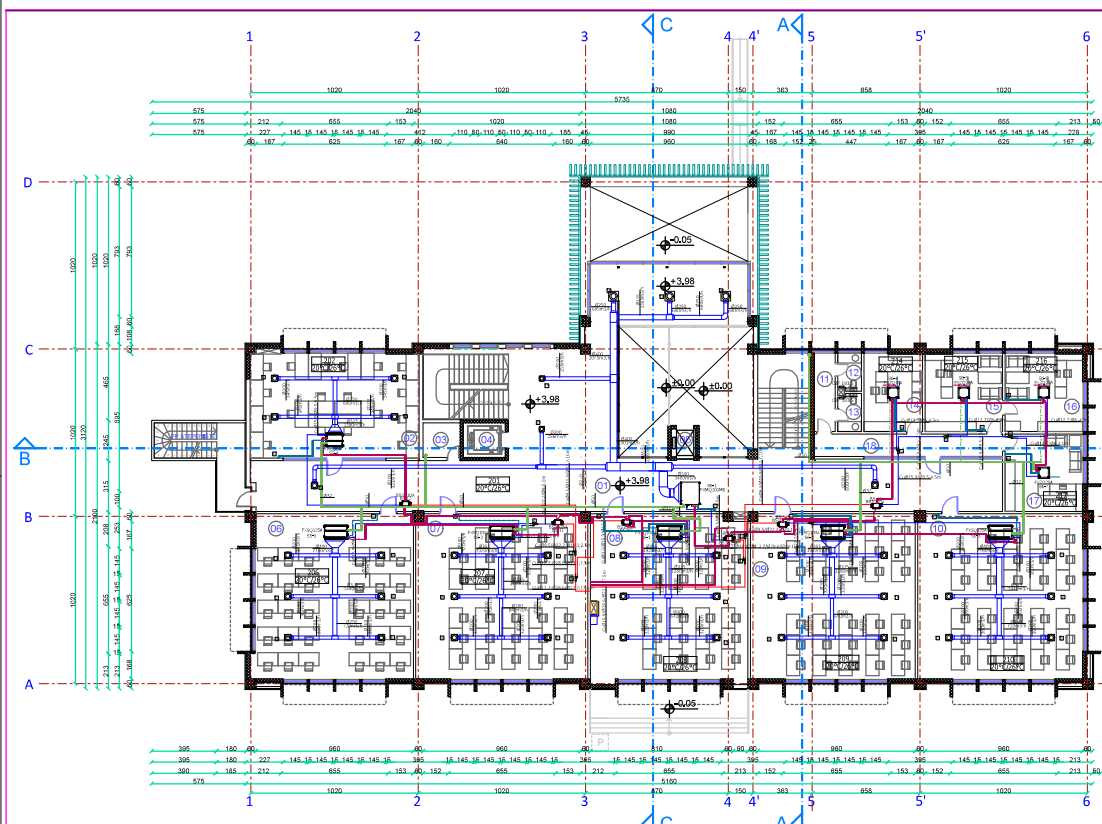
[illegible]

UNUTRAŠNJE JEDINICE VRV SISTEMA					
ODNAKA	Raširitev kapotlet UW/PN	Kapotlet g/100 g	Dimenzije HxWxD (mm)	Električne karakteristike	Priljubljeni cvipljivo
FV020SA	5,600 m	4,300 m	245x170x100	154W (230V/50Hz)	Cut536
FV025SA	11,200 m	12,500 m	245x140x100	260W (230V/50Hz)	Cut532
FV032SA	14,000 m	16,000 m	245x140x100	330W (230V/50Hz)	Cut532

[illegible][illegible]







PREGLED NETO I BRUTO POVRŠINA PRVOG SPRATA

D1, HOL, BASTEPENIŠTA	274,27m <sup>2</sup>	05, VJEZBAONICA	95,96m <sup>2</sup>	15, KABINET PRODEKANA	22,47m <sup>2</sup>	UKUPNO BRUTO P. POSTOLJESE I SPRATA	457,45m <sup>2</sup>
D2, DIPLOMISKA SALA	85,25m <sup>2</sup>	06, VJEZBAONICA	101,31m <sup>2</sup>	16, KABINET PRODEKANA	22,44m <sup>2</sup>	UKUPNO BRUTO P. SPRATA	1079,71m <sup>2</sup>
D3, TEHNIČKA PROSTORNA	4,72m <sup>2</sup>	10, VJEZBAONICA	101,31m <sup>2</sup>	17, PRAVNA SLUŽBA	15,78m <sup>2</sup>		
D4, LIFT ZA STUDENTE	5,38m <sup>2</sup>	11, PREDPROSTOR TOALETA	6,20m <sup>2</sup>	18, HODNIK			
D5, LIFT ZA OSOBLJE	3,55m <sup>2</sup>	12, TOALET	3,24m <sup>2</sup>				
01, VJEZBAONICA	97,42m <sup>2</sup>	13, TOALET	3,24m <sup>2</sup>				
02, VJEZBAONICA	105,39m <sup>2</sup>	14, RAČUNOVODSTVO	16,97m <sup>2</sup>				

VENTILATORI	Model	Prevel	Prevel	Prevel	Prevel	Prevel
CINAKA	prevel	prevel	prevel	prevel	prevel	prevel
OW100	100m <sup>3</sup> /h	100m <sup>3</sup> /h	100m <sup>3</sup> /h	100m <sup>3</sup> /h	100m <sup>3</sup> /h	100m <sup>3</sup> /h

U ovom dokumentu prikazane su sve potrebne informacije za izradu projekta. Svi podaci su izdani u skladu sa tehničkim specifikacijama i standardima. Projektant ne preuzima odgovornost za bilo kakve štete ili gubitke nastale u skladu s ovim projektom.

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VENTILATORI	Model	Prevel	Prevel	Prevel	Prevel	Prevel
CINAKA	prevel	prevel	prevel	prevel	prevel	prevel
OW100	100m <sup>3</sup> /h	100m <sup>3</sup> /h	100m <sup>3</sup> /h	100m <sup>3</sup> /h	100m <sup>3</sup> /h	100m <sup>3</sup> /h

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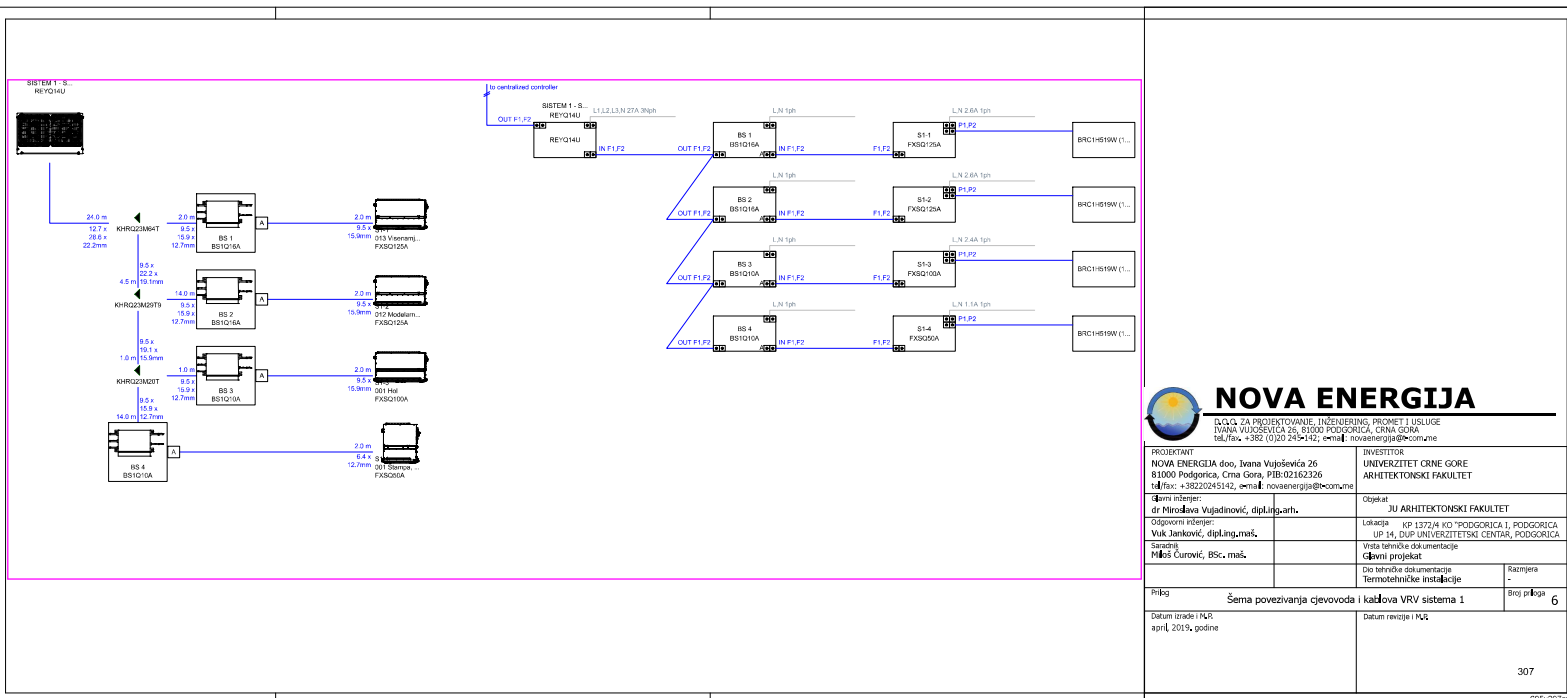
U ovom dokumentu prikazane su sve potrebne informacije za izradu projekta. Svi podaci su izdani u skladu sa tehničkim specifikacijama i standardima. Projektant ne preuzima odgovornost za bilo kakve štete ili gubitke nastale u skladu s ovim projektom.

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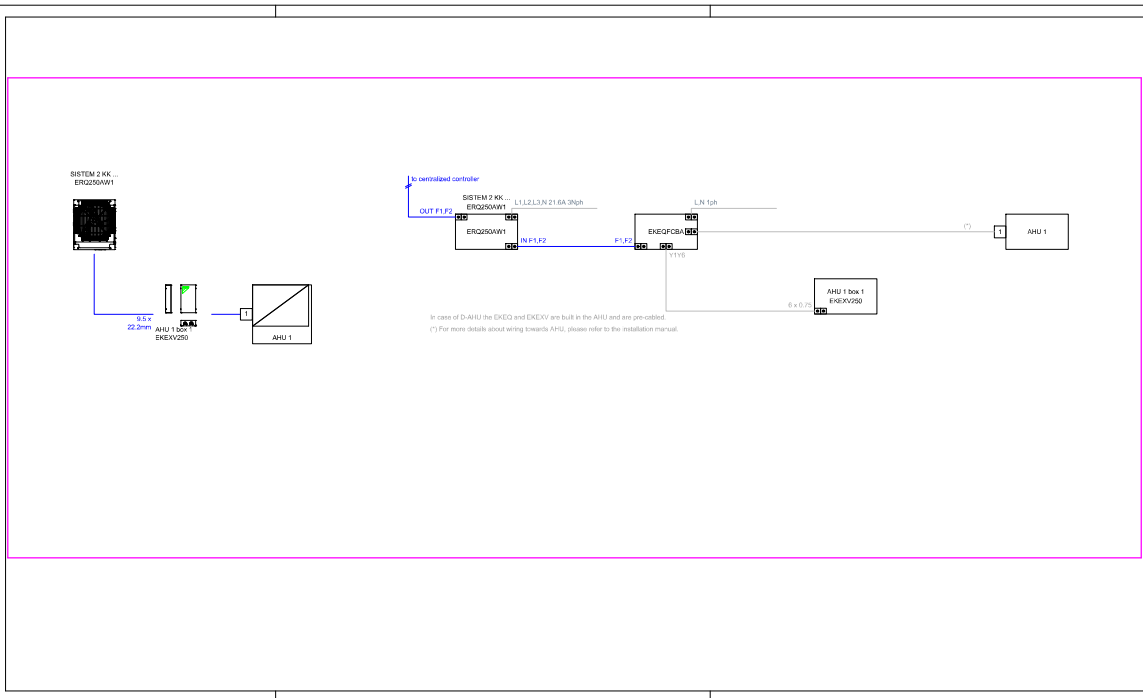



## NOVA ENERGIJA

POSREDOVANJE U PROMETU NEPOKRETNOSTI I POSREDOVANJE U PROMETU ELEKTRICNOSTI  
IVANA VUKOJEVIĆA 26, 81000 PODGORICA, CRNA GORA  
tél/fax: +382 (0)20 245142, e-mail: novaenergiya@comune

PROJEKTANT NOVA ENERGIJA doo, Ivana Vukojevića 26 81000 Podgorica, Crna Gora, PIB:02162326 tél/fax: +382(0)20245142, e-mail: novaenergiya@comune	INVESTITOR UNIVERZITET CRNE GORE ARHITEKTONSKI FAKULTET
Glavni inženjer: dr Miroslava Vujanović, dipl.ing.arh.	Objekat JU ARHITEKTONSKI FAKULTET
Odgovorni inženjer: Vuk Janković, diplomirani inženjer	Lokacija KP 1372/4 KO "PODGORICA 1, PODGORICA UP 24, DUP UNIVERZITETSKI CENTAR, PODGORICA
Saradnik: Miloš Čurović, BSc, maš.	Vrsta tehničke dokumentacije Glavni projekat
	Dio tehničke dokumentacije Termotehničke instalacije
Prilog Šema povezivanja cjevovoda i kačdova VRV sistema 1	Saopštenje Broj priloga 6

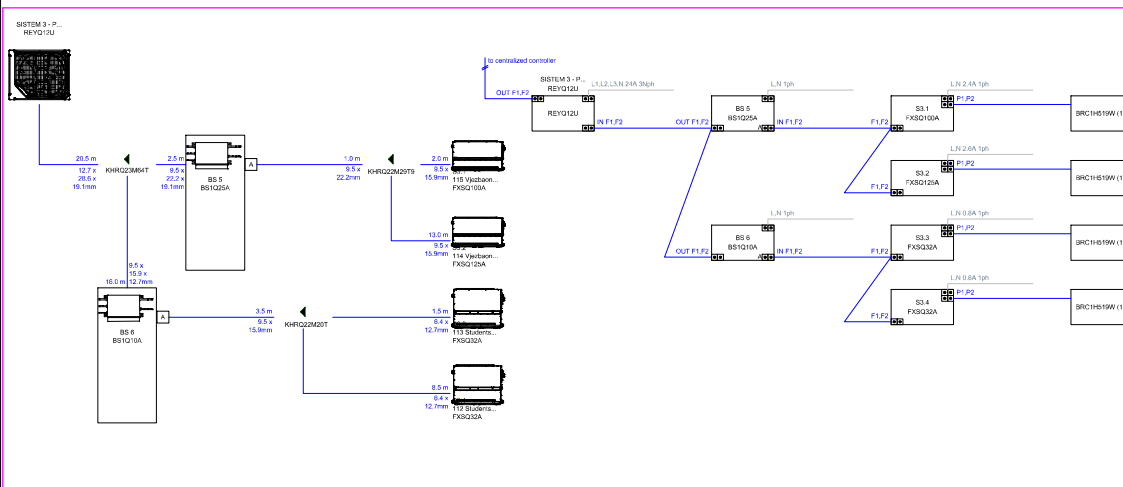
Datum izrade i PVR april, 2019. godine	Datum revizije i PVR
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# NOVA ENERGIJA

PROJEKTANT NOVA ENERGIJA d.o.o, Ivana Vukojevića 26 81000 Podgorica, Crna Gora, PIB:02162326 tel/fax: +382(0)20245142, e-mail: novaenergija@comune		INVESTITOR UNIVERZITET CRNE GORE ARHITEKTONSKI FAKULTET	
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Odgovorni inženjer: Vuk Janković, diplom.ing. meš.		Lokacija KP 1372/4 KO "PODGORICA 1, PODGORICA UP 24, DUP UNIVERZITETSKI CENTAR, PODGORICA	
Saradnja: Miloš Čurović, BSc. meš.		Vrsta tehničke dokumentacije Glavni projekat	
Prilog Šema povezivanja cjevovoda i kablova VRV sistema 2		Dio tehničke dokumentacije Termotehničke instalacije	
Datum izrade i PVR april, 2019. godine		Datum revizije i PVR	
		Saopštenje -	
		Broj priloga 7	
		308	



**NOVA ENERGIJA**

POSREDOVANJE U PROMETU NEPOKRETNOSTI I USLUGE  
IZ OBLASTI GRAĐEVINARSTVA I INŽENJERINGA

POSREDOVANJE U PROMETU NEPOKRETNOSTI I USLUGE  
IZ OBLASTI GRAĐEVINARSTVA I INŽENJERINGA

POSREDOVANJE U PROMETU NEPOKRETNOSTI I USLUGE  
IZ OBLASTI GRAĐEVINARSTVA I INŽENJERINGA

<b>PROJEKTANT</b> NOVA ENERGIJA d.o.o., Ivana Vukojevića 26 81000 Podgorica, Crna Gora, PIB:02162326 tel/fax: +382 (0)20 245142, e-mail: novaenergia@comune.me		<b>INVESTITOR</b> UNIVERZITET CRNE GORE ARHITEKTONSKI FAKULTET	
<b>Glavni inženjer:</b> dr Miroslava Vujanović, dipl.ing.arh.		<b>Objekat:</b> JU ARHITEKTONSKI FAKULTET	
<b>Odgovorni inženjer:</b> Vuk Janković, diplom.ing.		<b>Lokacija:</b> KP 1372/4 KO "PODGORICA 1, PODGORICA UP 24, DUP UNIVERZITETSKI CENTAR, PODGORICA	
<b>Saradnja:</b> Miloš Čurović, BSc. maš.		<b>Vrsta tehničke dokumentacije:</b> Glavni projekat	
<b>Prilog</b> Šema povezivanja cjevovoda i kačdova VRV sistema 3		<b>Dio tehničke dokumentacije</b> Termotehničke instalacije	
Datum izrade i PVR: april, 2019. godine		Datum revizije i PVR: -	
Broj priloga: 8		Broj priloga: 8	



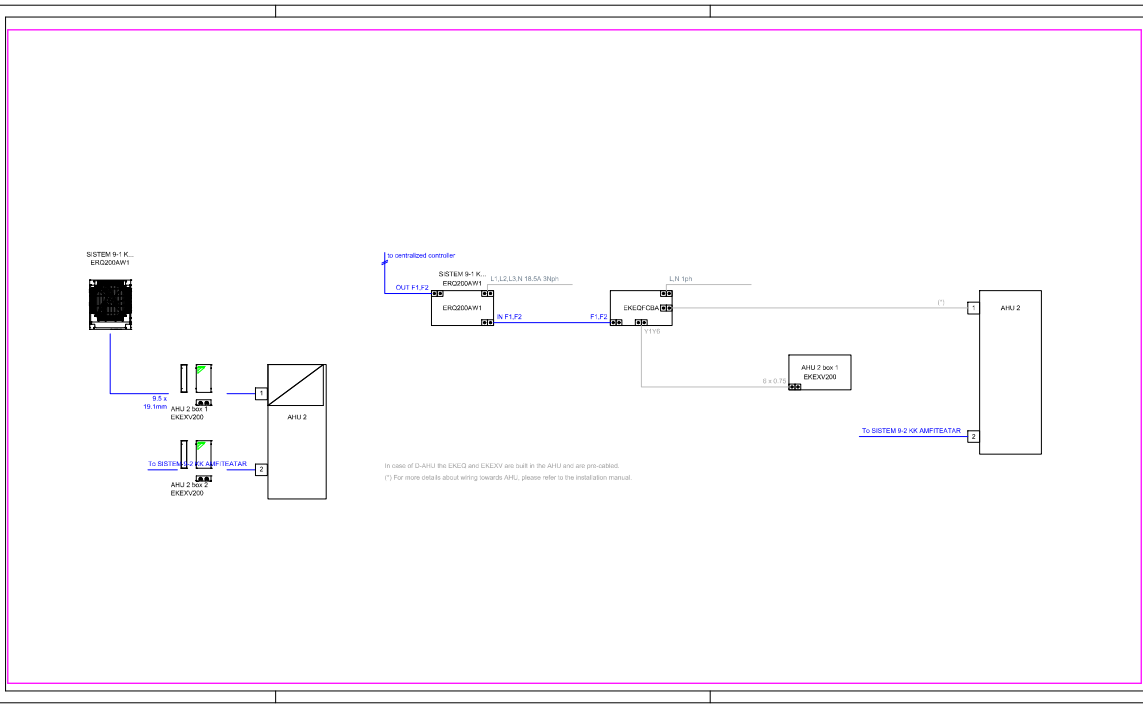













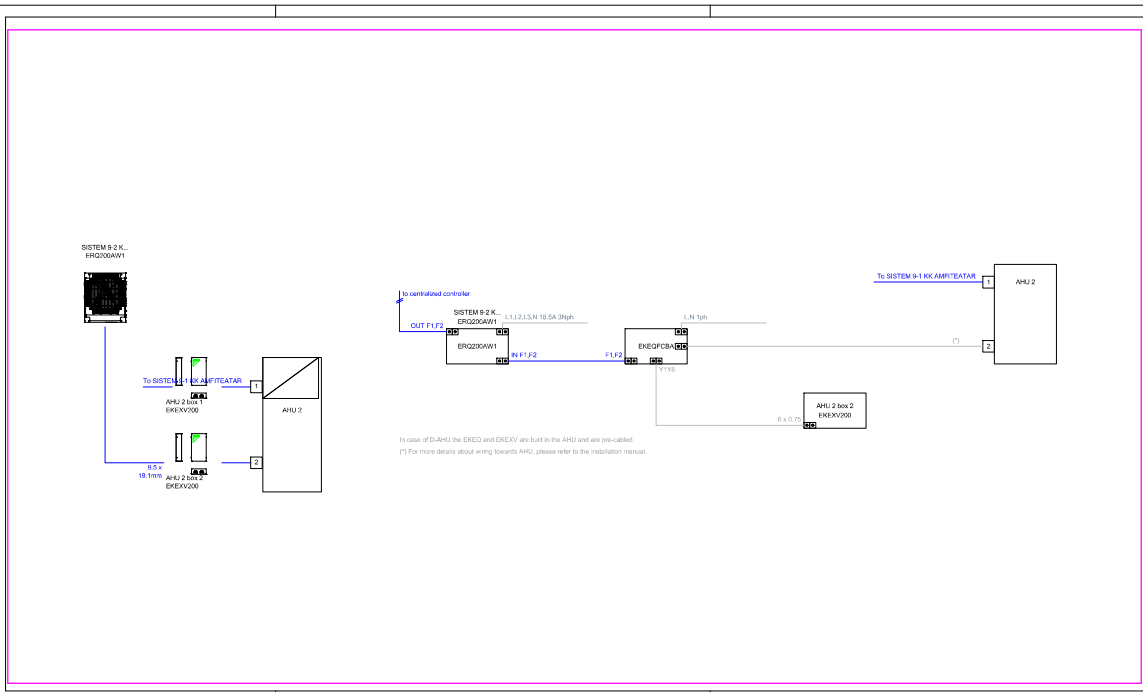



**NOVA ENERGIJA**  
POSREDOVANJE ZA PROJEKTOVANJE, INŽENJERING, PROMET I USLUGE  
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tél/fax: +382 (0)20 249142; e-mail: novaenergia@comune.me

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Odgovorni inženjer: Vuk Janković, diplom.ing.arh.		Lokacija KP 1372/4 KO "PODGORICA 1, PODGORICA UP 24, DUP UNIVERZITETSKI CENTAR, PODGORICA	
Saradnik: Miloš Čurović, BSc. maš.		Vrsta tehničke dokumentacije Glavni projekat	
		Dio tehničke dokumentacije Termotehničke instalacije	
Prilog Šema povezivanja cjevovoda i kačdova VRV sistema 9-1		Saopštenje Broj priloga 14	
Datum izrade i RJE april, 2019. godine		Datum revizije i RJE	

315

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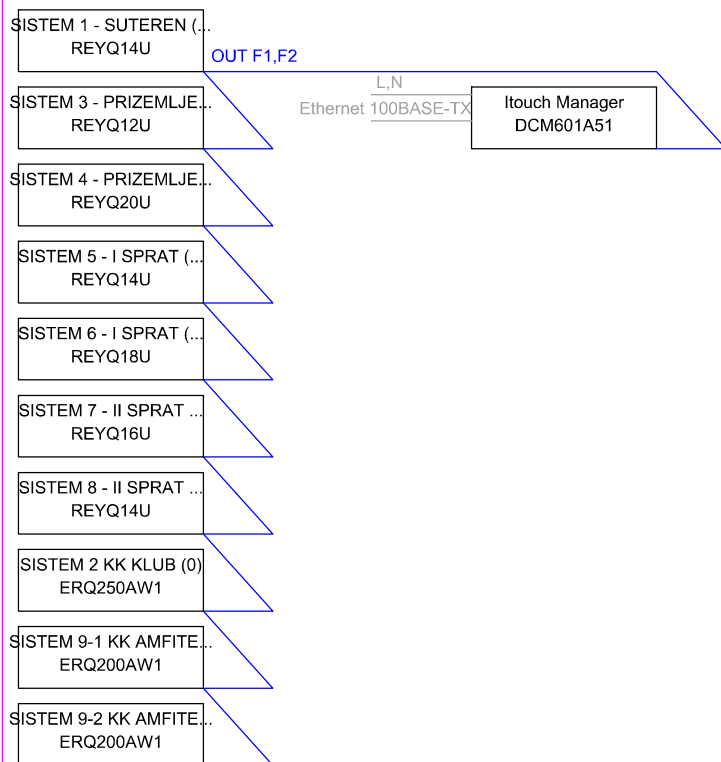


**NOVA ENERGIJA**

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<b>Glavni inženjer:</b> dr Miroslava Vujanović, dipl.ing.arh.		<b>Objekat:</b> JU ARHITEKTONSKI FAKULTET	
<b>Odgovorni inženjer:</b> Vuk Janković, diplom.ing.		<b>Lokacija:</b> KP 1372/4 KO "PODGORICA 1, PODGORICA UP 24, DUP UNIVERZITETSKI CENTAR, PODGORICA	
<b>Saradnja:</b> Miloš Čurović, BSc. maš.		<b>Vrsta tehničke dokumentacije:</b> Glavni projekat	
		<b>Dio tehničke dokumentacije:</b> Termotehničke instalacije	<b>Saopštenje:</b> -
<b>Prilog</b> Šema povezivanja cjevovoda i kablova VRV sistema 9-2		<b>Broj priloga:</b> 15	
<b>Datum izrade i PUN:</b> april, 2019. godine		<b>Datum revizije i PUN:</b> -	

316

695x287mm



# NOVA ENERGIJA

D.O.O. ZA PROJEKTOVANJE, INŽENJERING, PROMET I USLUGE  
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Glavni inženjer:	dr Miroslava Vujadinović, dipl.ing.arh.	Objekat JU ARHITEKTONSKI FAKULTET	
Odgovorni inženjer:	Vuk Janković, dipl.ing.maš.	Lokacija KP 1372/4 KO "PODGORICA I, PODGORICA UP 14, DUP UNIVERZITETSKI CENTAR, PODGORICA	
Saradnik:	Miloš Čurović, BSc. maš.	Vrsta tehničke dokumentacije Glavni projekat	
		Dio tehničke dokumentacije Termotehničke instalacije	Razmjera -
Prilog		Šema povezivanja kablova centralnog kontrolera	
Datum izrade i M.P. april, 2019. godine		Datum revizije i M.P.	
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